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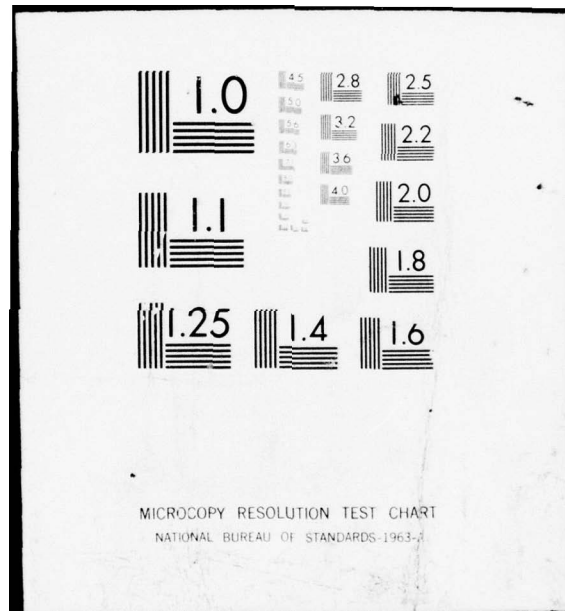
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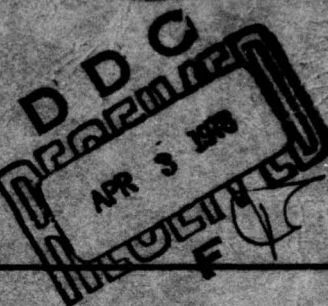


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Woods Hole Oceanographic Institution



W.H.O.I./BROWN CONDUCTIVITY,  
TEMPERATURE, AND DEPTH MICROPROFILER

by

N. L. Brown  
and  
G. K. Morrison

February 1978

TECHNICAL REPORT

*Prepared for the Office of Naval Research  
under Contract N00014-68-C-0241; NR 083-004.*

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# ABSTRACT

A Conductivity, Temperature and Depth (CTD) profiler has been designed to make precise fine scale measurements of these physical parameters in the ocean. This CTD system consists of a shipboard Data Terminal deck unit and an underwater unit which provides continuous sampling of the three variables as it is lowered into the water. Additional sensors can be added to measure other variables; the most common is dissolved oxygen.

This report is a detailed description of the CTD System and includes the necessary documentation to operate and maintain the equipment.

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## INTRODUCTION

The Conductivity, Temperature and Depth (CTD) profiler described here has been designed to make precise fine scale measurements of these physical parameters in the ocean. The CTD system consists of a shipboard Data Terminal deck unit and an underwater unit which provides continuous sampling of the three variables as it is lowered into the water. Additional sensors can be added to measure other variables; the most common is dissolved oxygen.

This report is a detailed description of the CTD System and includes the necessary documentation to operate and maintain the equipment.

Salinity can be derived from the pressure, temperature and electrical conductivity of a sample of sea water. With the CTD conductivity is measured with a miniature four electrode ceramic cell. Temperature is sensed by electronically combining the outputs of a high speed (30 millisecond) thermistor and a platinum resistance thermometer. This composite output has the excellent long term stability and linearity of the platinum probe with the rapid thermal response of the thermistor, independent of pressure effects and drifts in thermistor characteristics. Pressure is sensed by a strain gauge pressure transducer.

Data from the underwater unit is transmitted in real time to the shipboard data terminal through a single electrical conductor which is the core of the steel cable used to support the instrument in the

water. The data are in TELETYPE format using frequency shift key (FSK) modulation of a 5 and 10 kilohertz ac signal superimposed on the dc power supplied to the underwater unit through the same cable. This "audio" signal may be recorded directly on a good quality audio recorder for later processing.

The deck unit decodes the signal, provides digital data in both parallel and serial format for on-line computer processing and digital recording, and displays the variables in engineering units (decibars, degrees Celsius, and millimhos. There is also a digital to analog converter for real time plots using a two axis analog plotter.

The CTD is unique in that it provides the means for observing finestructure phenomena in both the temperature and salinity fields in the ocean at vertical scales of order centimeters. At the standard rate of 30 samples per second, an instrument lowered at about 75 meters per minute, for example, will give C, T, and D data averaged over about 1.5cm for each 5 centimeters of water providing a high resolution profile to full ocean depths (6000m) in about one and one-half hours.

## SYSTEM DESCRIPTION

Underwater Unit

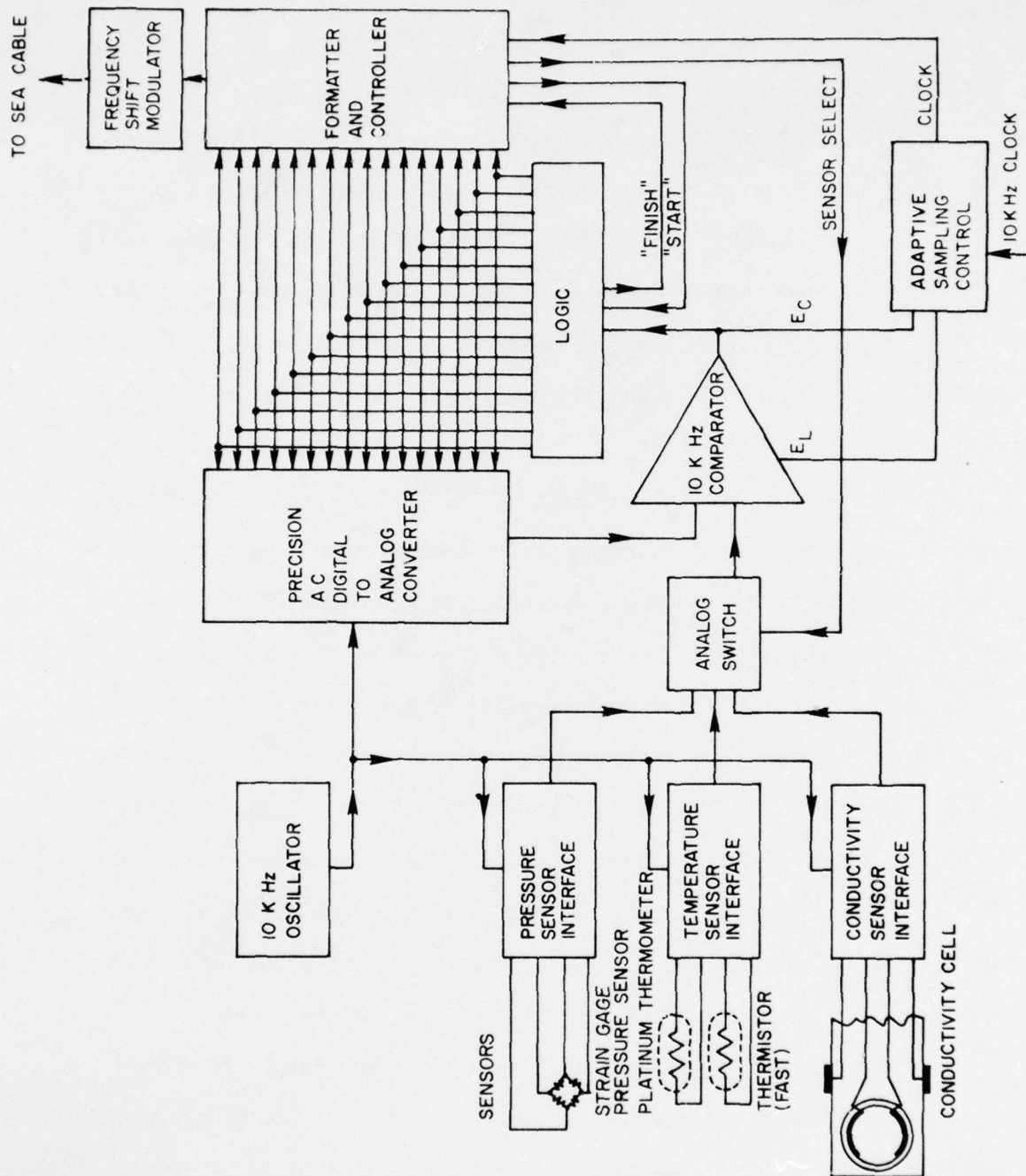
The CTD has two major assemblies, each subdivided into functional sections made up of modular circuit boards and mechanical assemblies. In the underwater unit these are the analog and digitizer sections plus some additional ancillary circuits including the Signal Generator and Power Supply voltage regulator. Figure 1.3 is a block diagram of the underwater unit showing these sections in relation to one another.

The analog section consists of the conductivity, temperature and pressure sensors and their associated interface or conditioning circuits. Consider each sensor and interface to be a four terminal device. If the two input terminals are excited with a 10 kilohertz reference voltage the amplitude of the output signal is a linear function of the variable as sensed by the corresponding transducer. The interface card for each sensor scales and linearizes the signals from zero to full scale in a special stable tuned feedback amplifier with the gain adjusted during calibration, and provides 500 millivolts RMS full scale output for each variable. These three conditioned signals then appear at the input of the analog switch for multiplexing and digitizing.

In the next section, each sensor interface output is electronically switched in sequence to the digitizer; a 16 bit binary ratio transformer which uses a successive approximation method to precisely determine the ratio of the output signal amplitude to the reference sig-



Fig. 1.3



nal voltage.

The AC Comparator, Digitizer Logic and D/A Converter form a loop which compares the output of the D/A with the sensor interface output bit by bit. Starting with the most significant, each bit is set high in turn, then reset or not depending on whether the D/A output is larger or smaller than the sensor output. The sequence continues until all 16 bits are tested. The Adaptive Sampling circuit controls the timing of the digitization and allows the comparator an appropriate recovery time after each test.

After all 16 switches have been sampled the digitizer sends a signal to indicate to the control circuitry that digitization is complete. In a standard system there are three digitization cycles in a data frame, one each for pressure, temperature and conductivity.

The Memory and Multiplexer circuit sequentially connects the interfaces to the digitizer and stores digitized words into buffer memory. The memory is required since the data from the previous frame is being clocked through the telemetry registers during digitization of the current frame. At the end of a frame the system waits for the next 31.25 hz clock pulse, after which the telemetry circuit is delayed for a few hundred microseconds while the buffer memory is dumped into the telemetry registers.

In the TTY formatting and FSK modulating card the serial data stream generated on the memory multiplexer board is serially shifted by the TTY gated clock. The data moves 8 bits at a time, then pauses while 2 "stop" bits and a "start" bit are mixed into the data stream. The

number of data bytes are counted and a continuous "high" or "one" state follows the data to complete the 32 ms. cycle or frame.

The data are shifted out of the TTY formatting circuit at 5000 bits/second into the FSK circuit where logic "ones" become two cycles of a 10 kilohertz sinewave and logic "zeros" become one cycle of a 5 kilohertz sinewave to be transmitted to the deck unit.

The signal generator board provides 10 kilohertz reference sine and square waves in phase, 10 kilohertz sine and square waves in quadrature ( $\pm 90^\circ$ ) to the reference signals, and 20, 40 and 80 kilohertz signals used in some special systems as high frequency clocks; this board also generates the 31.25 hz timing clock.

The power supply regulates the dc from the deck unit via the cable and provides the +12 and + 6 volts dc necessary to power the Underwater Unit circuitry.

#### Deck Unit

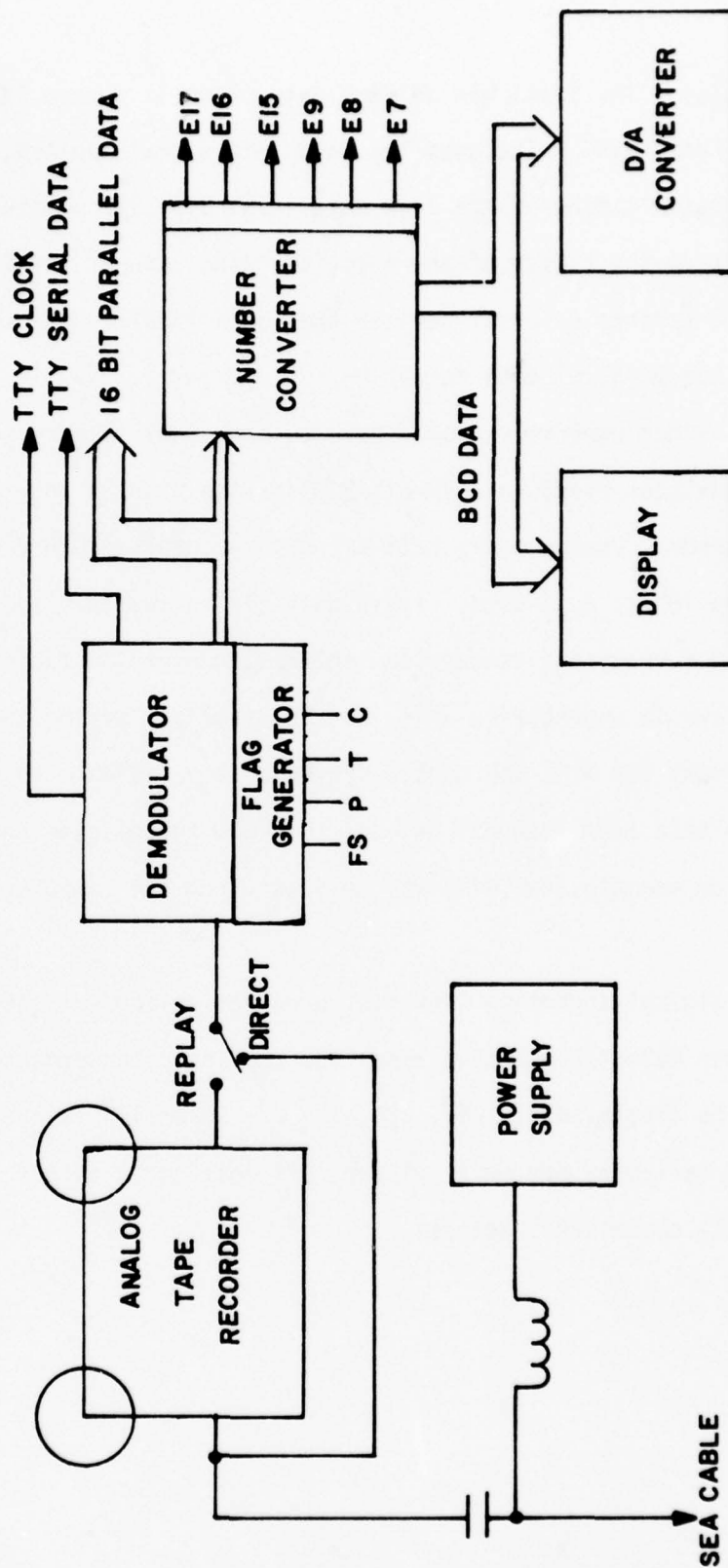
The deck unit decodes the signal from the Underwater Unit and provides analog and digital CTD data in a variety of formats.

The deck unit block diagram is given in figure 1.3(3).

The Demodulator is a phase locked loop decoder which converts the frequency shift keyed data signal from the Underwater Unit into a normal high or low state data stream. These data are available both as 16 bit parallel and serial data in TTY format. The demodulator card includes a circuit which detects a continuous stream of eleven or more logic "ones" which occur at the end of each scan and from this generates the

Fig. 1.3(3)

DECK UNIT





FRAME SYNC pulse. The first bit in each data frame is a zero "start" bit, and the FRAME SYNC pulse goes low when this signal appears, controlling the basic timing of the deck unit. The BIT TIME counter counts clock pulses from the finish of the negative going edge of the FRAME SYNC pulse and strobes external devices when a particular data word is available at the parallel data output.

The number converter board converts the 16 bit binary output from the demodulator board into 20 bit BCD for the display and the analog output boards. During every half BIT TIME a complete BCD conversion is done on the 16 bit data word. It is possible to multiply and divide by powers of 2 during this process to implement conversion factors so the data appears in engineering units on the display. During the second half of every BIT TIME the Number Converter is available to convert 16 bit binary data from external devices into BCD for display on the deck unit. For example, salinity may be input from the computer and displayed.

The digital to analog converter provides analog outputs controlled by user selectable enable lines for scaling. Temperature, for example, may be displayed at  $.25^0$ ,  $.5^0$ ,  $1^0$ ,  $2^0$ ,  $5^0$  or  $10^0$  full scale. As many as 12 variables may be displayed, originating in either the underwater unit or external devices.

## SPECIFICATIONS

MEASURED VARIABLES

<u>Variable</u>	<u>Range</u>	<u>Accuracy</u>	<u>Resolution</u>	<u>Stability*</u>
Pressure	0-320db	+0.5db	0.005db	0.1%/month
	0-650db	+1.0db	0.01 db	
	0-1600db	+1.6db	0.025db	
	0-3200db	+3.2db	0.05 db	
	0-6500db	+6.5db	0.1 db	
Temperature	-32 to +32°C	+0.005°C (-3 to +32°C)	.0005°C	.001°C/mo
Conductivity	1 to ∞ mmho	+0.005 mmho	0.001 mmho	.003mmho/mo
Dissolved Oxygen Current (Option 01)	0 to 2 µA	+ 2nA	0.5 nA	

\*For detailed description of performance in the field, see Fofonoff, Hayes and Millard, 1974.

POWER REQUIREMENTSDeck Unit

105 to 125 VAC      50 to 400Hz      200 watts  
Fuses, Back panel 2 Amp, Acopian Supply (power down cable) 200mA

Underwater Unit

100mA constant current from a 50 volt supply in the data terminal.  
Voltage at underwater unit connector is 24 V ± 10% at 100ma.

DATA FORMATData telemetry

Frequency shift key logic '1' is telemetred as two cycles of 10 kHz  
logic '0' is telemetred as one cycle of 5 kHz, 2 volts peak to peak  
max. (See Figure 3.1.12(2) )

Pressure, Temperature and Conductivity are generated as sixteen bit binary numbers; for telemetry these are broken into 2 eight bit bytes each of which is telemetred in TTY format with a logic zero start bit and two logic one stop bits making an 11 bit word. They are telemetred least significant byte and least significant bit first in the following order.

```

FRAME SYNC
PRESSURE
PRESSURE
TEMPERATURE
TEMPERATURE
CONDUCTIVITY
CONDUCTIVITY
SIGNS
DISSOLVED OXYGEN CURRENT (Optional)
DISSOLVED OXYGEN CURRENT (Optional)
DISSOLVED OXYGEN TEMPERATURE (Optional)

```

#### SENSORS

##### 1. Pressure

Standard Controls Model 211-35-440; 350 $\Omega$  strain gauge bridge, tube type.

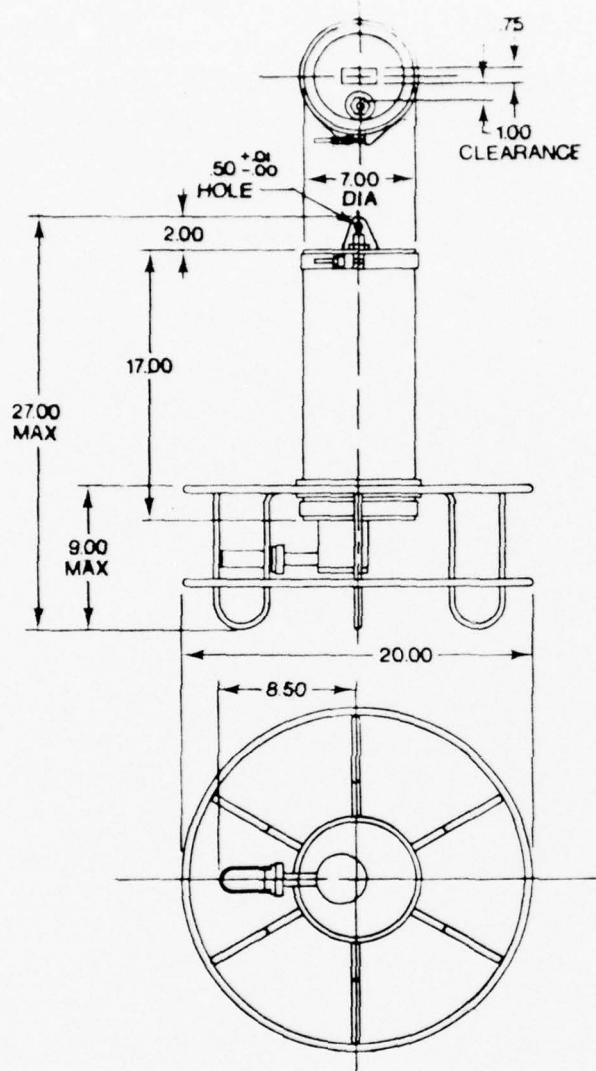
##### 2. Temperature

Platinum Thermometer Rosemount Model 171 BJ 200 $\Omega$  @ 20 $^{\circ}$ C  
(185.3 $\Omega$  @ 0 $^{\circ}$ C)

Thermistor: Fenwal #GC32SM2 2000 $\Omega$  @ 25 $^{\circ}$ C nominal.

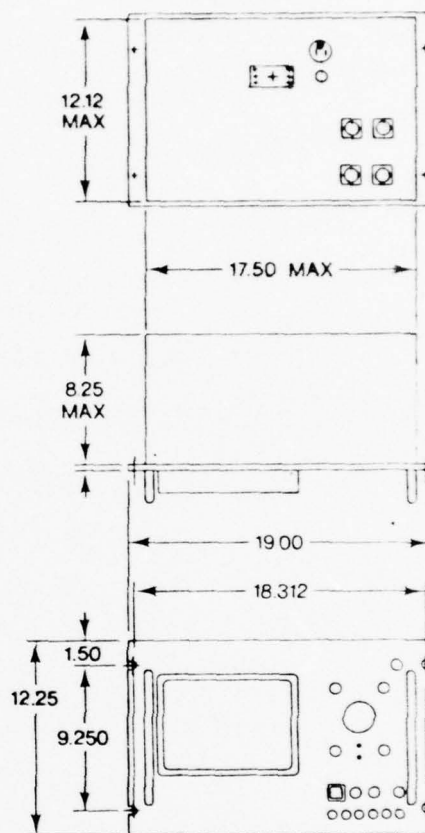
##### 3. Conductivity

Neil Brown Instruments #B10086 4 electrode cell .4cm x .4cm.  
x 3cm long. (see Section 3.1.4)



#### UNDERWATER UNIT:

Weight in air: 95 pounds  
 Weight in water: 72 pounds  
 Material: 17-4 PH stainless steel  
 Maximum safe working pressure: 7500 decibars  
 Shock protection: rugged impact absorbing  
 stainless steel guard frame



Dimensions in inches

#### DECK UNIT:

Weight: 25 pounds  
 Material: anodized  
 aluminum

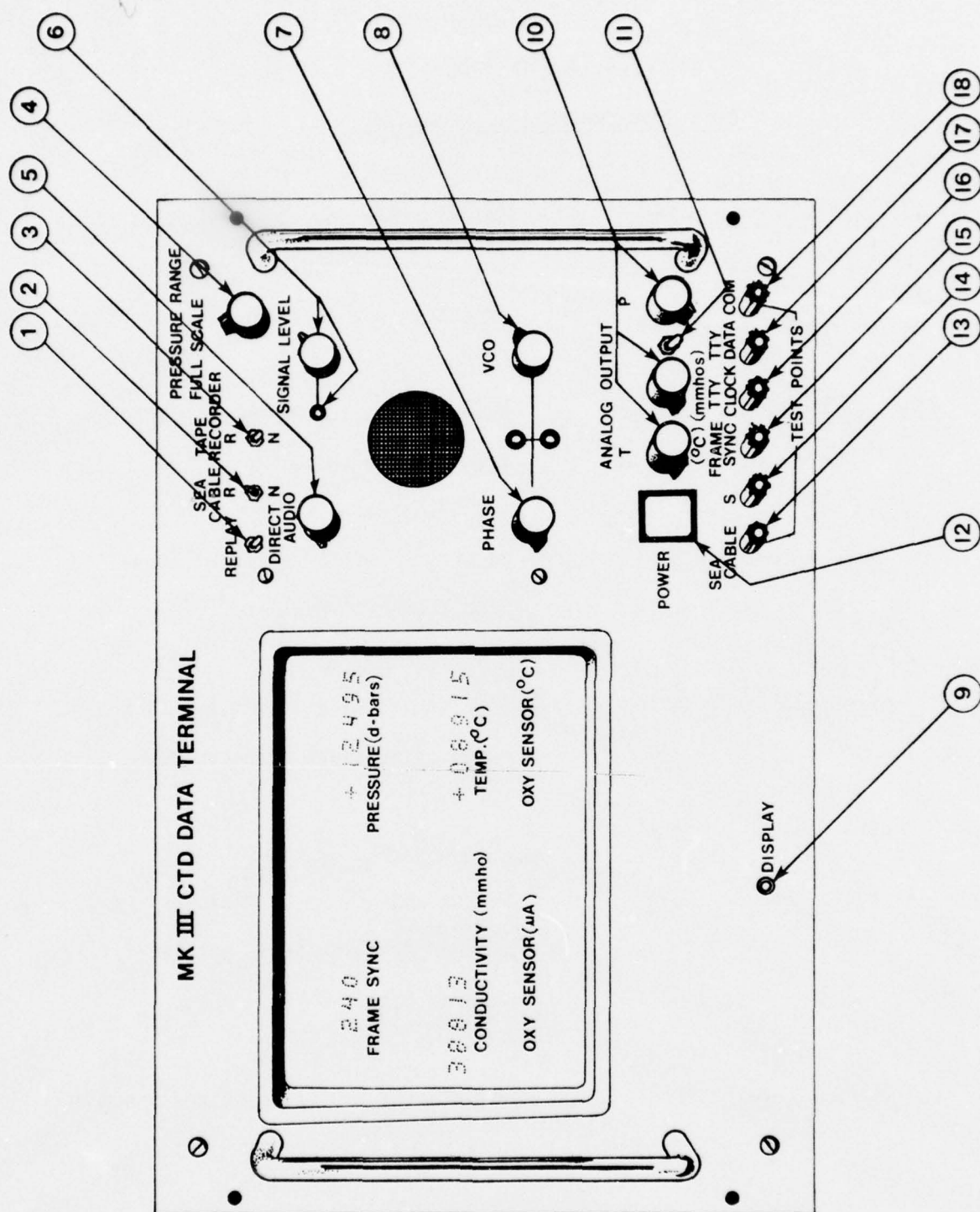
## CTD OPERATING INSTRUCTIONS

Deck Unit Controls - See Fig. 2.1

- |                                     |   |
|-------------------------------------|---|
| (1) <u>Replay/Direct</u> switch     | Selects data source - <u>Direct</u> is from the sea cable connector, <u>Replay</u> is from the tape recorder connector. |
| (2) <u>Sea Cable R/N</u> switch     | Reversing switch to invert signal from the sea cable.   |
| (3) <u>Tape Recorder R/N</u> switch | Reversing switch to invert signal from tape recorder input.   |
| (4) <u>Pressure Range</u> switch    | Sets the display to match Full Scale range of pressure transducer.  |
| (5) <u>Audio</u> control            | Switch and volume control for the speaker allowing audio output of telemetered data.                                    |
| (6) <u>Signal Level</u> control     | Adjusts the amplitude of the incoming data signal.  |
| (7) <u>Phase</u> switch             | Compensates for the cable phase shift.  |



Fig. 2.1



- (8) V.C.O. control Adjusts the frequency of the phase locked loop (PPL) in the demodulator.
- (9) Display S/H switch Freezes display (Hold) or allows it to change (Sample) at full data rate.
- (10) Analog Output switches  
    T C & P Selects Full Scale Temperature, Conductivity and Pressure corresponding to the 0 to 10V dc analog signal at connector J17 on the back of the Deck Unit. T and C ranges are given on the front panel; refer to Fig. 2.1(2) for pressure ranges corresponding to the switch positions.
- (11) S/H Sample/Hold switch holds the analog output or enables sampling at full data rate.
- (12) Power switch Actuates ac and dc power to all circuits.

#### Test Points

- (1 ) Sea Cable Frequency Shift Keyed data stream at the input to the deck unit. Audio

Pressures corresponding to full scale analog output

Pressure transducer Range	0 - 13,000	0 - 6,500	0 - 3,200	0 - 1,600
Switch position				
1	100	50	25	12.5
2	200	100	50	25
3	400	200	100	50
4	800	400	200	100
5	1,000	500	250	125
6	2,000	1,000	500	250
7	4,000	2,000	1,000	500
8	8,000	4,000	2,000	1,000

N. B. All analog outputs are self paging, i.e. after full scale is reached origin is incremented to full scale on previous scan.



signal, 2 V p-p maximum.

- (14) S Digital Data stream in F.S.K. format after level adjustment.
- (15) Frame Sync Sync pulse, negative going edge is synchronized with start of a data frame for oscilloscope triggering, etc.
- (16) TTY Clock Clock running at 8 times the data rate; External input for teleprinter interface.
- (17) TTY Data Data stream in teletype format: open collector output (pull down resistor required if the TTY interface is not connected).
- (18) Com. Signal and DC common connection.

CTD Operation

1. Connect underwater unit to sea cable termination. (See section 2.2.1)
2. Connect end of sea cable from center of cable drum to slip ring rotor.
3. Connect slip ring stator to deck unit cable. (See Section 2.2.1)
4. Connect audio tape recorder output from deck unit to tape recorder if required.
5. Connect line cord to 105-125 V alternating current supply 47-400 Hz.
6. Set pressure range switch to range of sensor in use in underwater unit.
7. Set Direct/Replay switch to Direct.
8. Set Display switch to S.
9. Turn Phase & VCO control knobs fully counter-clockwise.
10. Actuate Power switch.
11. Vary Signal Level control until associated LED is dimly lighted.
12. Turn VCO control until two associated LEDS are on with equal light intensity.
13. Select the Phase switch position until the intensity of the LEDS is minimized.
14. When properly synchronized, the Frame Sync digital display word will be either "240" or "015" when Display switch is in the H mode. If not, 1) check for other positions of the VCO control that produce equal light level on the 2 LEDS, and check Frame Sync word.

- 2) If not synchronized, reverse Sea Cable R/N switch and repeat the procedure.
15. The digital display of Temperature and Pressure will now be reading ambient temperature and pressure and the CTD is ready to be lowered into the water. To record data on an audio recorder, adjust the signal level on the recorder and commence.
16. The audio recorder can be used as a back-up in case of malfunction of a digital data logger or computer processing system, or as a convenient way to store raw data for later processing. To replay from the Audio Recorder, switch Replay/Direct switch to Replay and proceed to set up Deck Unit starting at instruction Number 8.

## ELECTRICAL CONNECTORS/CABLES

Underwater UnitXSG-2-BCL connector.

Small pin     Signal and +DC

Large pin     Common

Mating Connector RMG-2-FS

Deck UnitSea Cable

A     Signal and +DC

B     Sea ground

Serial Data Out

A     12V TTY data (open collector)

B     TTL Level TTY clock

C     TTL level TTY data

D     Common

Audio Tape Recorder

A }     Output to tape recorder

B }     Auxiliary input (high level)

C     N.C.

D     Common

E }     Input from tape recorder

F }

G     N. C.

H     N. C.

Analog Outputs (0 to 10 volt)

- A    Temperature
- B    Pressure
- C    Pressure common
- D    N.C.
- E    Conductivity common
- F    Conductivity
- G    Temperature common
- H    N.C.

Parallel Connections to Computer

See table in Section 5.2.7(3)

Cable Requirements

A single conductor armored cable is required such as  
Rochester type 1-H-255

## SERVICE ACCESS TO UNDERWATER UNIT

Conductivity Cell and Thermistor Replacement

The sensor head is a subassembly that may be electrically disconnected from within the pressure housing and removed for servicing. The fast response thermistor, platinum thermometer and conductivity cell are mounted in the head in addition to the other elements of the thermometer bridge, (temperature transformer, T1 and Vishay resistor  $R_F$ .) To remove Thermistor or Conductivity Cell:

- 1) Lay the CTD Underwater Unit on its side with the sensor arm vertical and the sensors at the top.
- 2) Remove the "U" shaped sensor guard.
- 3) Carefully remove the two socket head screws that retain the sensor clamping plate.
- 4) Withdraw the clamping plate along with the conductivity cell and thermistor.
- 5) Exercising great care rotate the conductivity cell and thermistor until the clamping plate may be removed by passing the cell and thermistor through the slots.
- 6) Both the thermistor assembly and the conductivity cell connect to the leads via electrical connectors to facilitate rapid replacement. It will be necessary to either install a pre-calibrated card when changing a sensor or else to recalibrate the appropriate channel.
- 7) After cleaning and lightly greasing the 'O' rings with Parker



"Super 'O' Lube" the sensor head should be assembled in the reverse order, after purging with Freon gas.

Underwater Unit

To gain access to the underwater unit:

CAUTION: V-BAND CLAMP TORQUE MUST NOT EXCEED 60 INCH-POUNDS.

- 1) Remove the top V-band clamp.
- 2) Use a 3/8" rod through the mounting lug on the top cap as a handle and stand on the guard cage; remove the top cap with an even, steady pull. Be careful of the penetrator connector wiring on the inside.
- 3) Disconnect electrical connector on the inside of the top cap.
- 4) Place instrument on its side and remove the bottom V-band clamp.
- 5) Unseat bottom end cap seal by pulling firmly while grasping sensor arm, and remove bottom end cap and electronics chassis.
- 6) Remove card retainer by removing the six screws on the card rack.

To gain access to Sensor Head:

- 1) Remove Bendix connector between wiring harness and sensor head.
- 2) Remove three screws that hold the sensor head to the bottom end cap.
- 3) With bottom cap off remove transformer through the upper end of the sensor assembly with gentle pressure on transformer from below.



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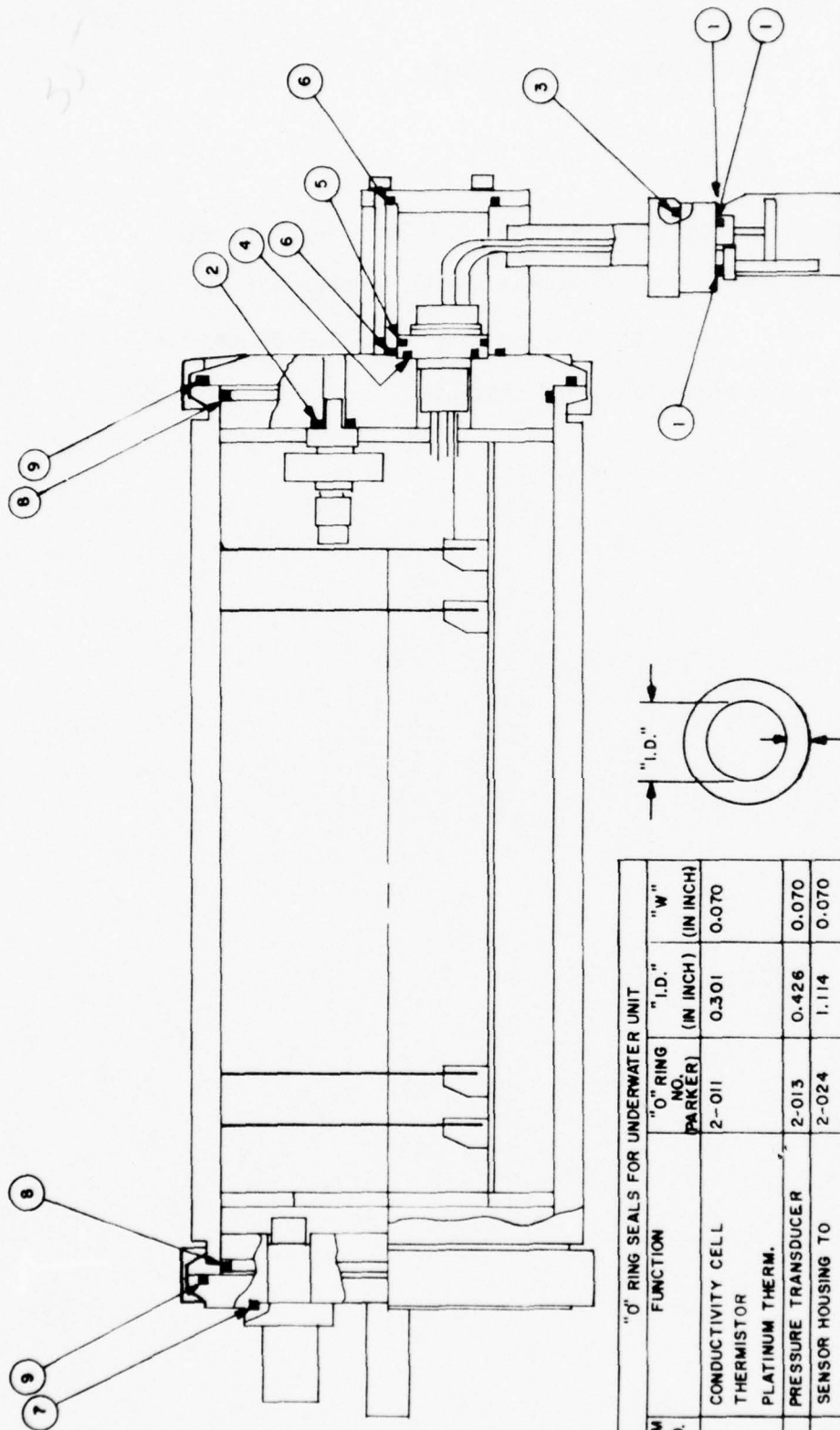
The Underwater Unit is reassembled in reverse sequence. Inspect, clean or replace and regrease 'O' rings; they should be lightly coated with Parker "Super 'O' Lube". Before installing bulkhead transformer, fill sensor head with Freon gas. Before installing top cap, purge pressure case by filling with Freon gas. Attach V-band clamps and torque to 60 inch-lbs.

## SERVICE ACCESS TO DECK UNIT

Deck Unit

To gain access to the circuit cards and 0.3 Amp down cable power fuse in the deck unit remove the six screws on top of the unit and lift off the top cover. A standard Cambion Model 714-1100-01 extender card may be used for troubleshooting and testing.

Fig. 2.2.4



"O" RING SEALS FOR UNDERWATER UNIT				
ITEM NO.	FUNCTION	"O" RING NO. (PARKER)	"I.D." (IN INCH)	"W" (IN INCH)
1	CONDUCTIVITY CELL THERMISTOR PLATINUM THERM.	2-011	0.301	0.070
2	PRESSURE TRANSDUCER	2-013	0.426	0.070
3	SENSOR HOUSING TO MOUNTING PLATE	2-024	1.114	0.070
4	BULKHEAD SEAL TO BOT. CAP	2-028	1.364	0.070
5	BULKHEAD SEAL TO SENS. HSG.	2-030	1.614	0.070
6	SENS. HSG. TO BOTTOM CAP	2-032	1.864	0.070
7	SENS. HSG. TO HOUSING CAP	2-213	0.921	0.139
8	TOP OUTPUT BULKHEAD CONN.	2-256	5.734	0.139
9	TOP END CAP & BOT. END CAP	2-260	6.484	0.139

"O" RING SEALS FOR UNDERWATER UNIT

## TESTS & CALIBRATION

This section of the manual is to outline the tests and calibration procedures necessary for users to check the calibration of their instruments. In addition to a dc voltmeter, frequency counter and an oscilloscope, it is necessary in performing the following calibrations to have a platinum standard thermometer and Mueller bridge, a supply of standard sea water, (at least 3 ampoules), magnetic stirrer, a Dewar flask large enough to accommodate the sensor housing, a precision dead weight pressure tester, and a well stirred insulated constant temperature bath. Some independent method of measuring conductivity is also desirable such as a Model CT-2 Temperature-Conductivity Transfer Standard.

### Precalibration Checkout Procedure

The following checkout must be performed before pre-cruise calibration.

1. Remove the CTD Underwater Unit pressure housing.(2.2.2(3) )
2. Measure the voltage levels on the power supply; J6, pins 30-35 should be 12V  $\pm 10\%$ . Adjust the 6V line, Pin 20-29, with the trim pot R6 on the power supply board to one half of the measured 12V value within  $\pm .01$  Volts.
3. Check the frequency on pin 8 of the signal generator J13; it should measure 10,000 Hz  $\pm 20$  Hz.
4. Check that the sine and square wave 10 kilohertz references

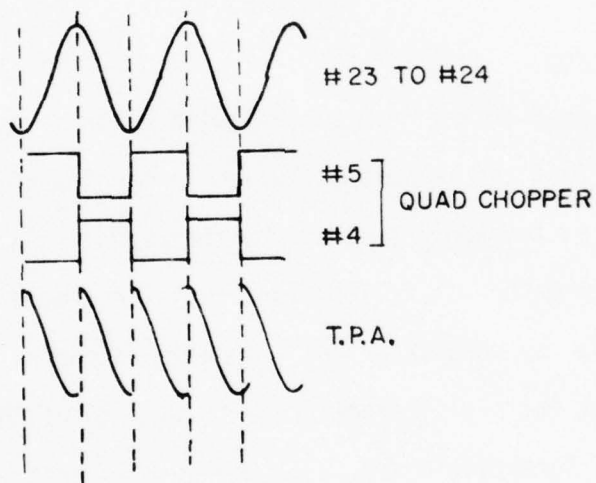
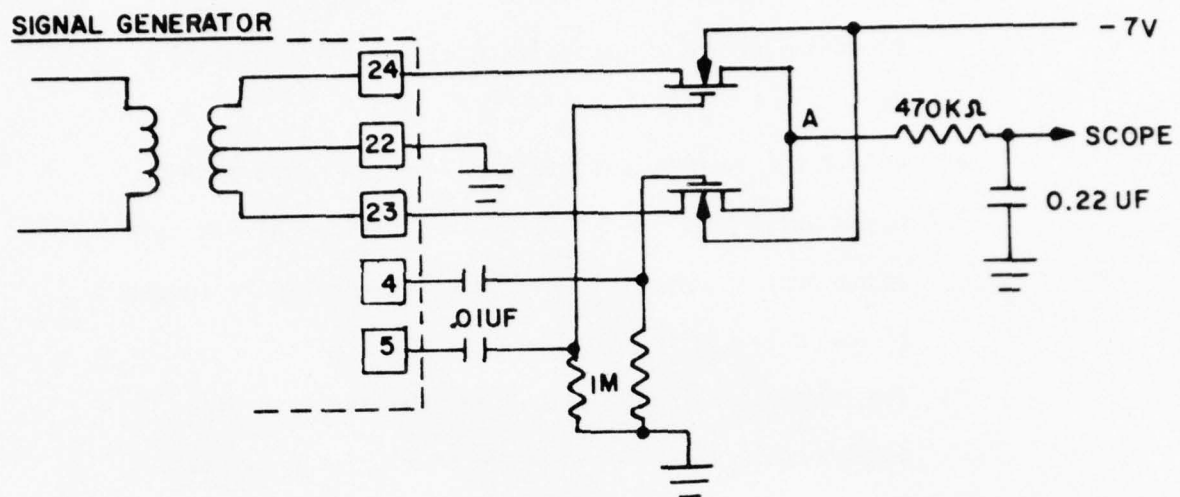
sources are exactly in phase. The test circuit illustrated is required. (Figure 2.3(2) )

5. With the signal generator still in the underwater unit connect the test fixture to connector J13 as shown. The dc output should be less than  $\pm 5\text{mV}$ ; if not, adjust the series-parallel tuned circuit on the signal generator board as follows:
  - a) Remove jumper labeled J7 on schematic and component layout. ( Figure 5.1.13; 5.1.13(1) )
  - b) Tune slug in transformer T1-J13 to give zero output  $\pm 5\text{mV}$  at output point on test fixture.
  - c) Replace jumper.
  - d) Tune slug in L1 on J13 to give zero  $\pm 5\text{mV}$  output on test fixture.
  - e) Reseal tuning slugs in T1 and L1 with R.T.V.

The signal generator board is now aligned.
6. Procedure for adjusting the zero and bias controls on the AC comparator, J7.
  - a) Remove all four sensor interface boards, (J1-J4).
  - b) Jumper pin 12 to #15 on the conductivity interface back plane connector J4.
  - c) With an oscilloscope triggered from pin 31 on the memory and multiplexer board, observe pin 5 on the adaptive sampling board (time base 1ms/cm, sensitivity 10 Volt/cm, dc coupled. The correct waveform is the



Fig. 2.3(2)



lower signal in figure 2.3(3).

- d) Adjust the bias potentiometer, P1 on the comparator to minimize the sinusoidal signal in region marked "A".
- e) Adjust the zero potentiometer P3 on the comparator board until the region 'A' becomes horizontal (as this adjustment is made this region will increase in length to about 1 ms).
- f) The comparator is now set up and the zero and bias potentiometers may be locked with R.T.V. or glyptal.

#### Temperature Calibration

The first step in the temperature calibration is to ensure that the quadrature from the sensors is nulled in the interface circuits at  $15^{\circ}\text{C}$ . To do this, the sensors should be immersed in a well stirred  $15^{\circ}\text{C} \pm 1^{\circ}\text{C}$  temperature bath. It is important that the temperature of the bath should not change by more than  $.001^{\circ}\text{C}$  in a few seconds.

1. Connect the oscilloscope probe to pin 26 of the fast response interface board, J3. The 10 kilohertz sine wave at this point should be nulled using the quadrature adjustment potentiometer, P1, on the fast response board, J3.
2. Move the oscilloscope probe to test point 6 on the AC comparator board, J7 with the oscilloscope triggered from pin 31 on the memory and multiplexer board, J10. Set the time base of the oscilloscope to 5 milli-seconds per divi-

COMPARATOR TEST POINTS

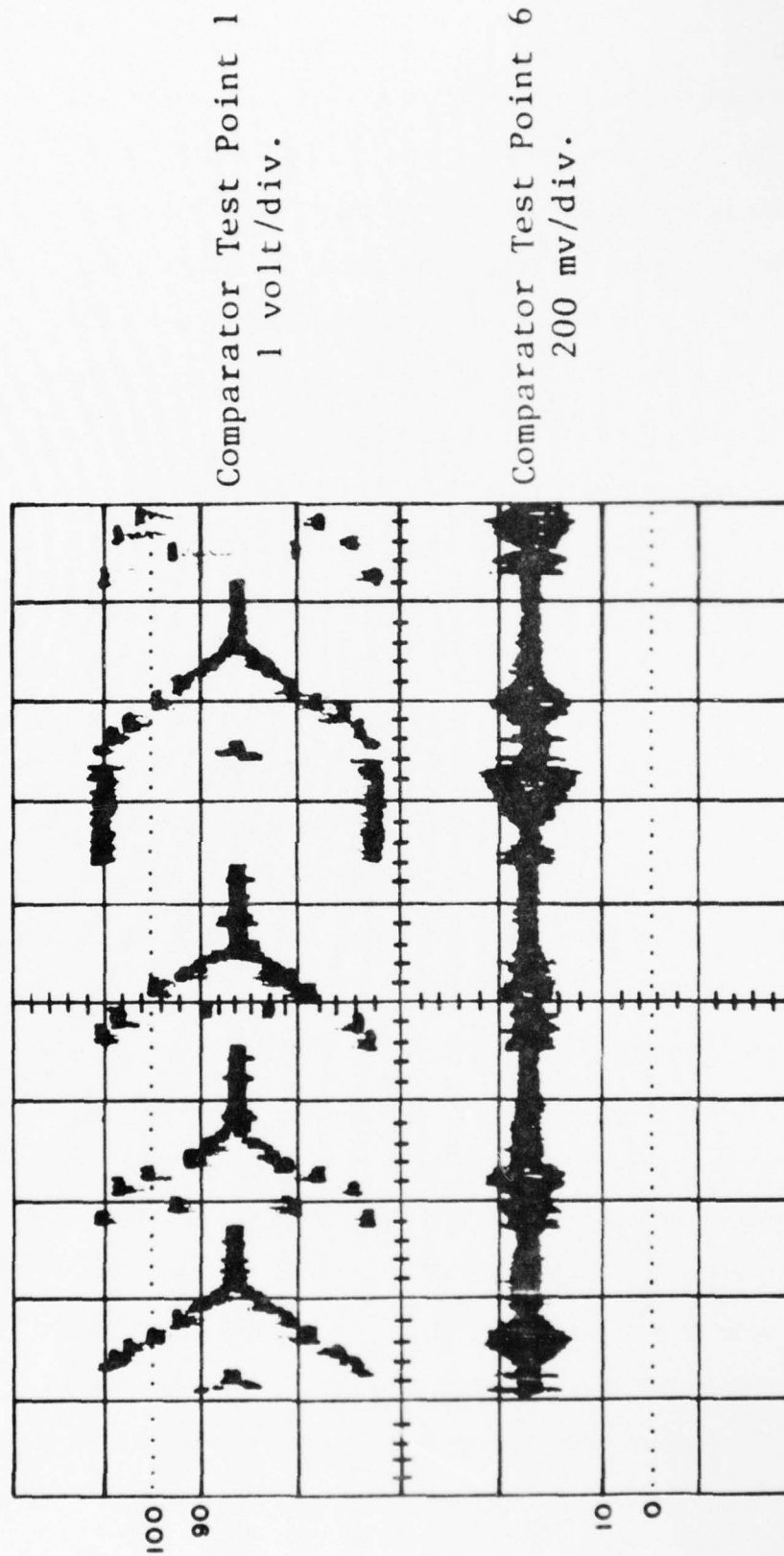


Fig. 2.3(3)

sion, and the vertical sensitivity to .200 volts per division. The signal during the second 10 milliseconds of the trace should be nulled with the quadrature adjustment potentiometer, P1, on the temperature interface board, J4. The adjusting screw on the quadrature potentiometer on the fast response board (P1 on J3) should now be secured with R.T.V. or glyptal. (See figure 2.3 (4) )

3. When the temperature bath is stable, note the temperature on the deck unit display. Adjust the quadrature potentiometer, P1, on the temperature interface board to give a two-thirds maximum output during the temperature period, observing the quadrature signal on the oscilloscope at TP6, J7 as before. The quadrature potentiometer, P2 on comparator J7 should now be adjusted to restore the temperature value displayed on the deck unit as noted when the temperature quadrature was nulled. The quadrature potentiometer, P1, on the Temperature interface board should now be turned back through zero until it is at two-thirds saturation on the other side of zero. The indicated temperature display should not have changed by more than a few millidegrees from the value at zero quadrature and two-thirds quadrature in the opposite direction. It may be necessary to trim the quadrature potentiometer, P2, on the comparator to obtain minimum variation in the displayed temperature when the temperature interface quadra-

# COMPARATOR TEST POINTS

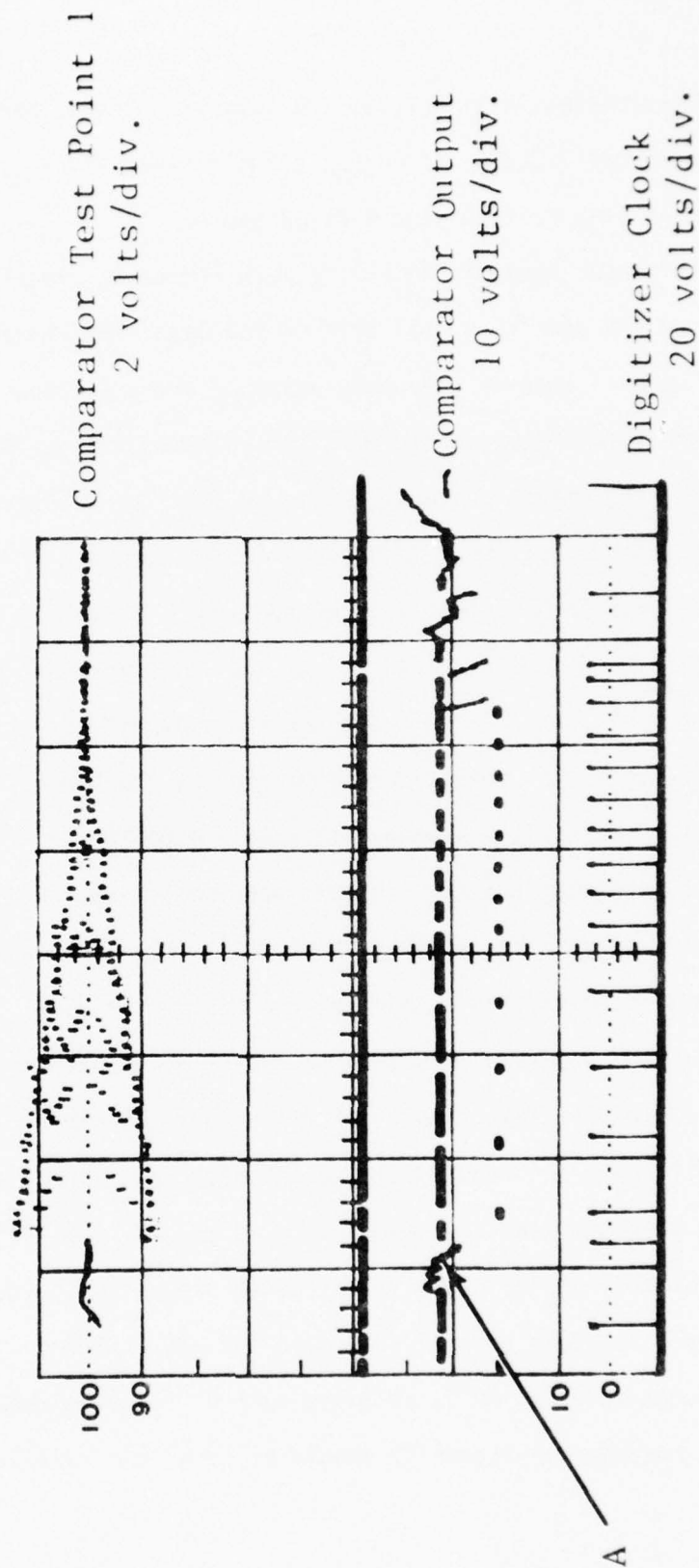


Fig. 2.3(4)

Oscilloscope triggered externally from pin 31 on Memory and Multiplexor jack, time base 1 ms/div.



ture potentiometer is adjusted  $\pm 2/3$  saturation; max. permissible error  $\pm 0.002^{\circ}\text{C}$ . Readjust potentiometer P1,J7 by criteria of step 2, then secure P1,J2 and P2, J7.

4. Cover the sensor assembly with fine mesh screen to protect the sensor and develop a well stirred ice bath with shaved ice and water. Immerse the probe assembly and a platinum resistance thermometer connected with a Mueller bridge in the bath. The entire assembly should be left to stabilize for at least one half hour before continuing the test. When the ice bath has stabilized as confirmed by several consecutive identical readings of the Mueller bridge, adjust the zero pot, P2, on the temperature interface board, J7, until the temperature indicated by the CTD agrees with the Mueller standard to within  $\pm 0.001^{\circ}\text{C}$ .
5. Remove the sensors from the ice bath and immerse them in a well-stirred bath of water at about  $30^{\circ}\text{C}$ . When the bath has been allowed time to stabilize, the Mueller bridge should be read several times and the sensitivity potentiometer, P3, on the temperature interface board should be adjusted to make the reading on the CTD deck unit agree with the platinum standard temperature to within  $\pm 0.001^{\circ}\text{C}$ . To check the linearity of the temperature circuitry it is necessary to measure several points in the well-stirred bath between zero and  $30^{\circ}\text{C}$ , at least each  $5^{\circ}$  is recommended. The maximum non-linearity should be less than  $.002^{\circ}\text{C}$ .

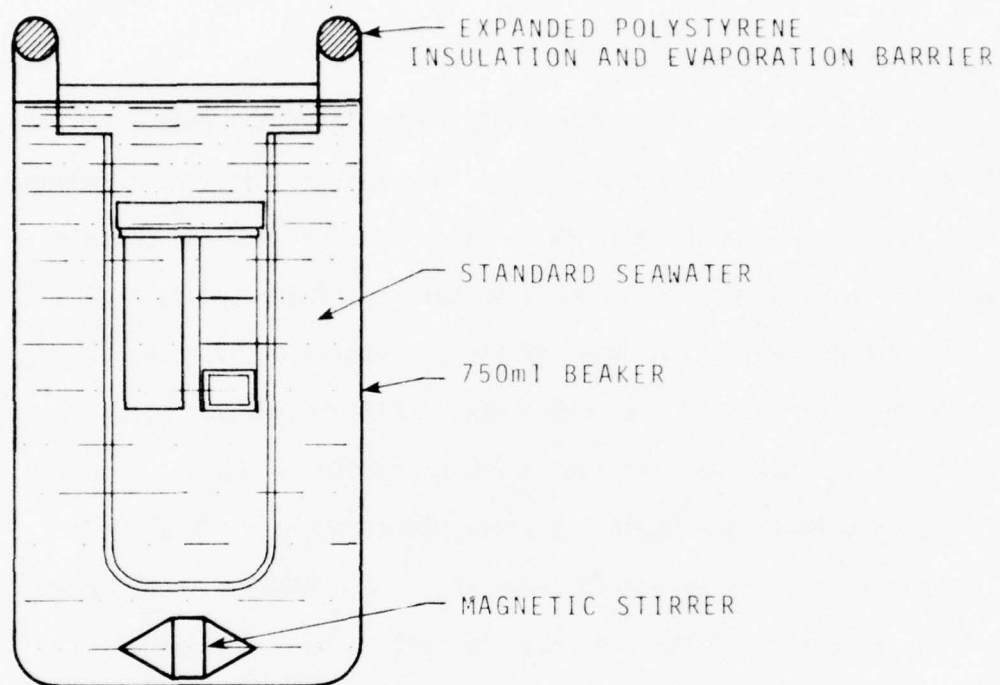
After the calibration is completed, check that all the potentiometers which have been adjusted are secured with R.T.V. or glyptal.

#### Field Conductivity Calibration

Before starting the conductivity calibration the cell should be cleaned by soaking for several minutes in a solution of 1 part saline dissolvent (General Chemical MT6) to 25 parts of water. After cleaning immerse the sensor assembly in a small beaker as illustrated in Figure 2.3(6) taking care to ensure that the ends of the conductivity cell tube do not come within 3/4 inch of the beaker wall. Fill the beaker with standard sea water of known salinity until the conductivity sensor is completely immersed up to the stainless steel mounting block. Start the magnetic stirrer, making sure that there are no air bubbles in or around the tube at the bottom of the conductivity cell. The beaker should be as well sealed as possible to minimize evaporation and the standard sea water should be warmed before opening and allowed to cool slowly during the conductivity calibration so that air is going into solution rather than coming out and forming bubbles which cause problems during the calibration. The first filling of standard sea water will almost certainly be wasted by the time the air bubbles have been removed and the bath is stable since evaporation will probably have been sufficient to cause a significant change in the salinity resulting in a faulty calibration.

Observing test point 6 on the comparator board, J7 and triggering the scope from pin 31 of the memory and multiplexer board, J10.

Fig. 2.3(6)



the quadrature signal during the 3rd 10ms period of the trace should be nulled by means of the quadrature potentiometer, P1, on the conductivity interface board, J4. (See Figure 2.3(4) )

Without disturbing the arrangement illustrated in the figure, stop the magnetic stirrer, remove the standard sea water from the beaker by means of a small siphon tube, and refill the beaker with fresh warm standard sea water. Several readings of conductivity and temperature should be noted and the salinity computed with the equation given in Appendix 7.4. The conductivity sensitivity adjustment P2 on J4 should be trimmed until the indicated conductivity agrees with the expected conductivity for standard sea water at the measured temperature. After this value has been correctly set, the measurement should be repeated with at least one more filling of standard sea water to confirm that the adjustments are correct. This conductivity calibration is a single point calibration: it is intended as a performance check when sophisticated calibration equipment is not available. It should be emphasized that a temperature error of  $.001^{\circ}\text{C}$  will introduce a conductivity error of about  $.001 \text{ mmho/cm.}$ ; it is important to note temperature values closely during the conductivity calibrations.

Note:  $\text{Salinity} = 1.80655 \times \text{Chlorinity}$  quoted on Std. Sea Water Ampoule  
Laboratory Conductivity Calibration

Clean the cell and adjust the quadrature of the Conductivity Interface according to the steps outlined in the Field Conductivity Calibration procedure .

Zero offset adjustment procedure:

1. Set zero potentiometer, P3, J4, to mid-range by observing wiper with an oscilloscope and adjusting for null output with respect to ground.
2. Measure two known conductivities at extremes of the range (i.e. 10 mmho,  $G_L$ , and 60 mmhos,  $G_H$ , and correct measured conductivity for thermal effects on the cell using:

$$G_{\text{Corrected}} = G_{\text{Indicated}} (1 - \alpha (T - 15^{\circ}\text{C}))$$

where  $\alpha = 6.5 \times 10^{-6} \text{ }^{\circ}\text{C}^{-1}$  = coeff. of expansion of alumina ceramic

$\Delta G_L$  is the error at Cond.,  $G_L$

$\Delta G_H$  is the error at Cond.,  $G_H$

Find  $\Delta G_H$ , and  $\Delta G_L$  where  $\Delta G = \text{Actual Cond.} - G_{\text{Corrected}}$

Linearly extrapolate these two values to zero and find intercept. (error at conductivity zero)

$$\text{Zero offset, } A = \Delta G_H - G_H \left( \frac{\Delta G_H - \Delta G_L}{G_H - G_L} \right)$$

For example:

$$\Delta G_H = .012 \text{ mmho } \Delta G_L = .004 \text{ mmho.}$$

$$\text{if } G_H = 60 \text{ mmho and } G_L = 10 \text{ mmho.}$$

$$A = .012 - \frac{.008 (60)}{50} = .0024.$$



3. Using high known conductivity adjust zero potentiometer, P3, J4, to make intercept zero (i.e. decrease reading by A)

Sensitivity adjustment using high known conductivity:

Adjust sensitivity potentiometer, P2, J4, to make full scale reading correct - making allowance for temperature dependance of cell using:

$$G_{Ind} (1 - \alpha (T - 15)) = G_{known}$$

#### Pressure Calibration

The following adjustments should be made in the sequence indicated. As in the previous sections, it will first be necessary to null the quadrature signal from the sensors. Test point 6 on the comparator board, J7, should be observed using an oscilloscope triggered from pin 31 on J10 on the memory and multiplexer board. The quadrature signal in the pressure region, the first 10 milliseconds after the trigger, should be nulled by the same procedure for temperature and pressure, by means of the zero quadrature nulling potentiometer, P3, on the pressure interface board, J1. With the pressure transducer at ambient pressure, the zero adjust potentiometer, P2, should be adjusted to cause a zero reading on the deck unit. The dead weight tester should be set to full scale, first the sensitivity quadrature potentiometer, P5, should be adjusted, and then the sensitivity potentiometer, P4, should be adjusted to cause the deck unit to display the correct full scale reading.

Several intermediate points should be checked to establish the linearity of the pressure transducer.

To perform the temperature coefficient adjustments, it is necessary to remove the pressure transducer from the end cap and to mount it in a special block as Figure 2.13(10)

CAUTION: PRESSURE TRANSDUCER TORQUE MUST NOT EXCEED 60 INCH-POUNDS.

Pack this block and transducer in ice and allow the temperature to stabilize. After approximately one half hour, adjust the zero temperature coefficient potentiometer, P1 on J1, to bring the pressure reading back to zero with zero pressure applied. The pressure transducer should now be exercised to full scale using a dead weight tester as before and the jumper links in the scale temperature coefficient adjustment should be shifted to regain the room temperature full scale readings on the deck unit. One link shift is equivalent to either .02% or .04% change depending on the position of link  $J_s$  on board J1.

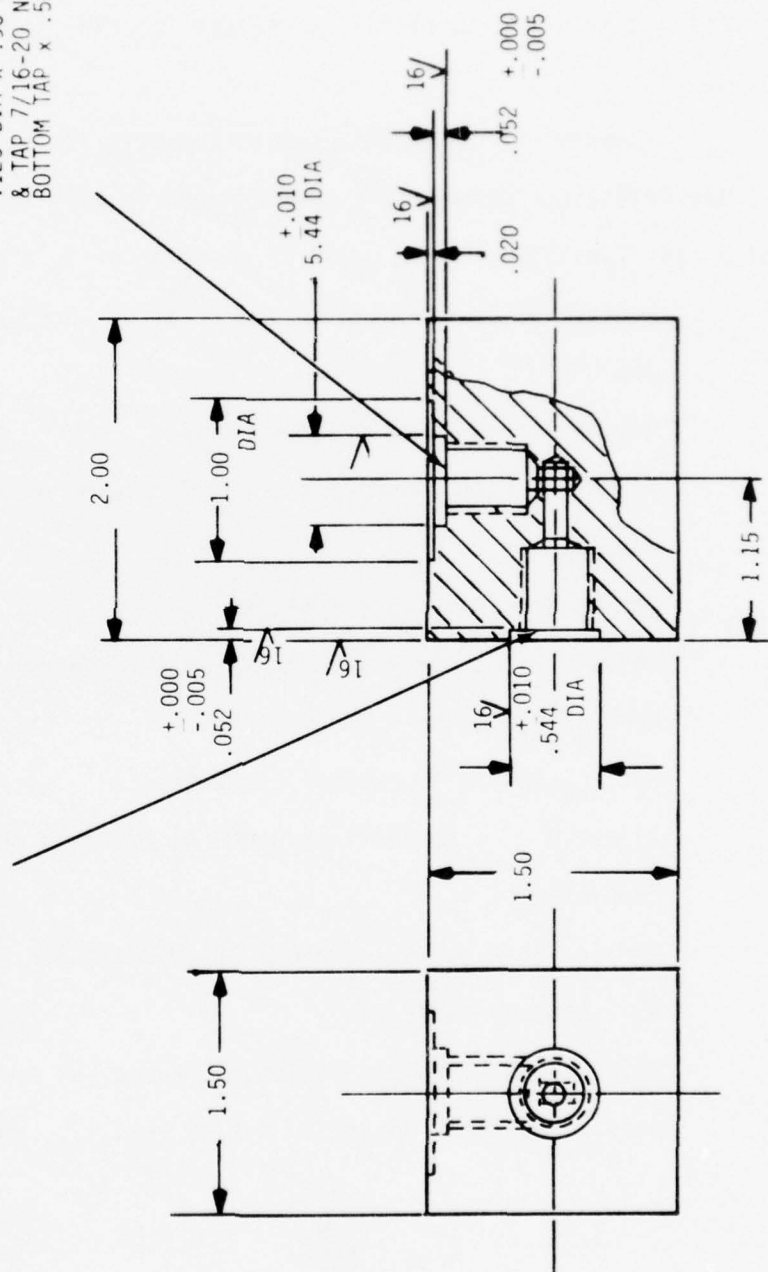
CAUTION: PRESSURE TRANSDUCER TORQUE MUST NOT EXCEED 60 INCH-POUNDS.

Replace the transducer in the end cap, and readjust zero and zero quadrature; secure potentiometer adjusting screws.

UNLESS OTHERWISE NOTED  
DIMENSIONS ARE IN INCHES

.125 DIA x 1.12 DEEP  
& TAP 7/16-20 NF-2B  
BOTTOM TAP x .50 DEEP

.125 DIA x .90 DEEP  
& TAP 7/16-20 NF-2B  
BOTTOM TAP x .50 DP.



## OXYGEN CALIBRATION PROCEDURE

Install 'O' rings in  $O_2$  receptacle housing. Screw cap on the  $O_2$  receptacle housing and install screw and 'O' ring in the side of the housing.

Immerse the sensor housing in ice bath for several hours until the resistance between the green and white wires at the receptacle housing has stabilized. Note value of resistance ( $R_t$   $0^\circ\text{C}$ ).

Connect GR box to pins 28 and 29 of  $O_2$  backplane connector, J5.

Set GR box to  $R_t$   $0^\circ\text{C}$  measured above

Adjust  $T_o$  potentiometer for +00.0 reading on oxygen temperature display

Set GR Box to  $R_t$   $25^\circ\text{C} = 41.2\text{k}\Omega$ .

Adjust  $T_s$  pot for +25.0 on oxygen temperature display

Recheck  $R_t$   $0^\circ\text{C}$  and  $R_t$   $25^\circ\text{C}$  points.

Set  $V_{os}$  pot fully counter-clockwise

Adjust  $V_{os}$  cw to just get 0.000 on D/U with no load resistor connected.

Measure voltage, E, at pin 2 of AD580 to pin 29 of connector, J5. Note value as E

Using  $800\text{k}\Omega$  0.1% load resistor between red and black wires on sensor housing. Adjust  $O_2$  pot to read  $I_{cal}$  on D/U.

$$I_{cal} = \frac{E}{800\text{k}\Omega}$$

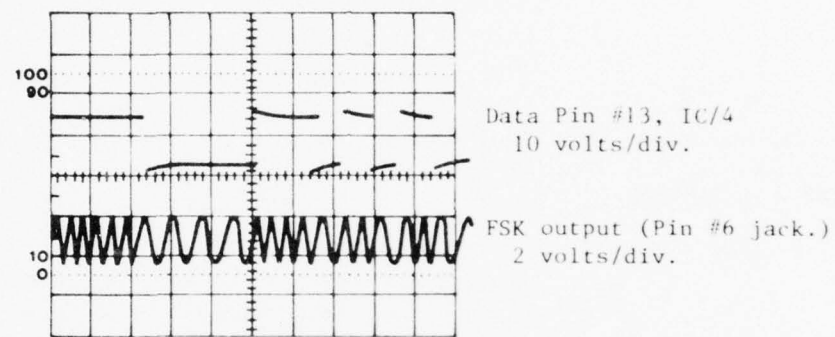
## TEST POINT WAVEFORMS AND SEQUENTIAL TIMING DIAGRAM

	Page
TTY/FSK Waveforms	2.4(2)
Comparator test points	2.4(3)
	2.4(4)
	2.4(5)
Memory and Multiplexer	2.4(6)
Demodulator test points	2.4(7)
Sequential timing diagram	2.4(9)

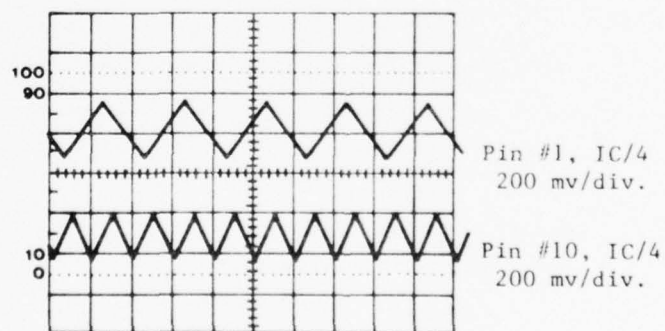


Fig. 2.4(2)

TTY/FSK WAVEFORMS



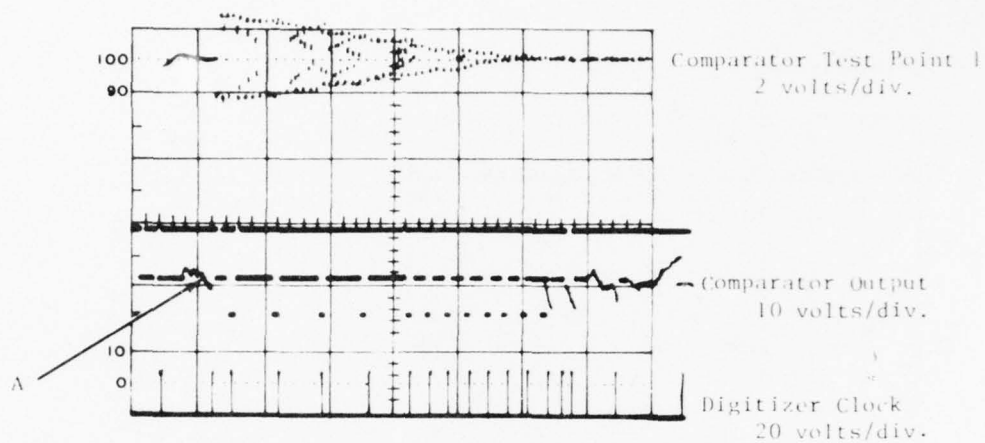
Time base uncalibrated >200 ms/div.



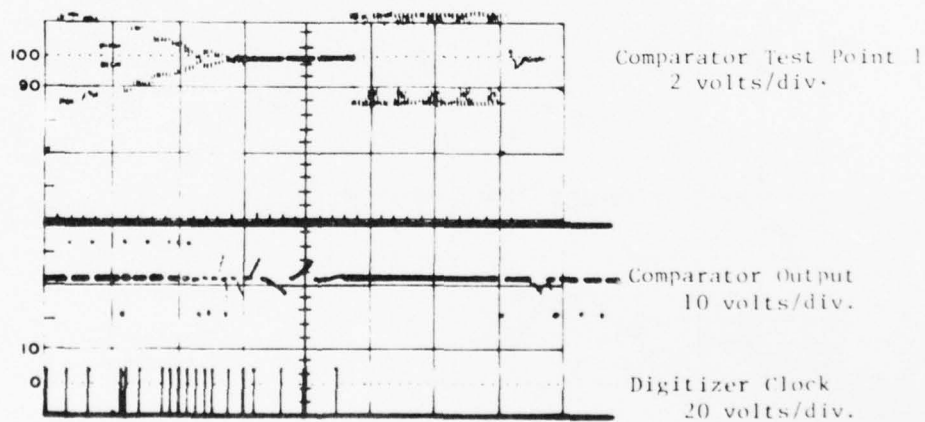
Time base 100  $\mu$ s/div.

Fig. 2.4(3)

# COMPARATOR TEST POINTS



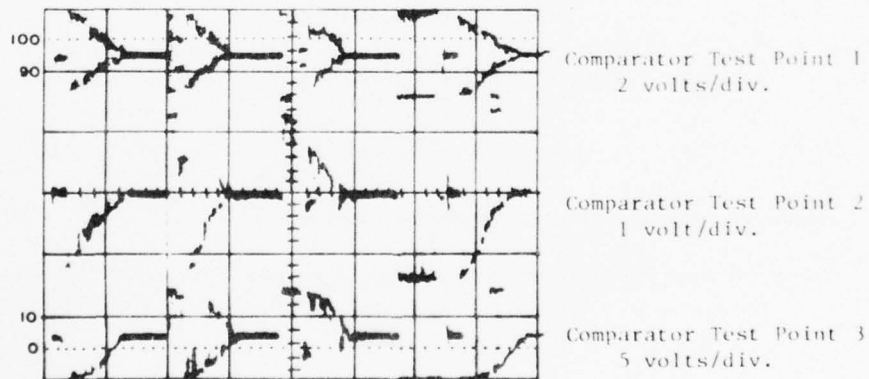
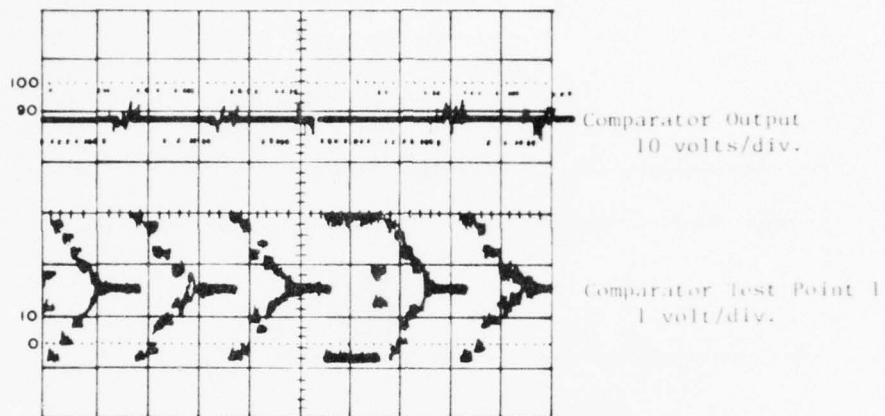
Oscilloscope triggered externally from pin 31 on Memory and Multiplexor jack, time base 1 ms/div.



Oscilloscope triggered externally from pin 31 on Adaptive Sampling jack, time base 2 mS/div.

Fig. 2.4(4)

COMPARATOR TEST POINTS

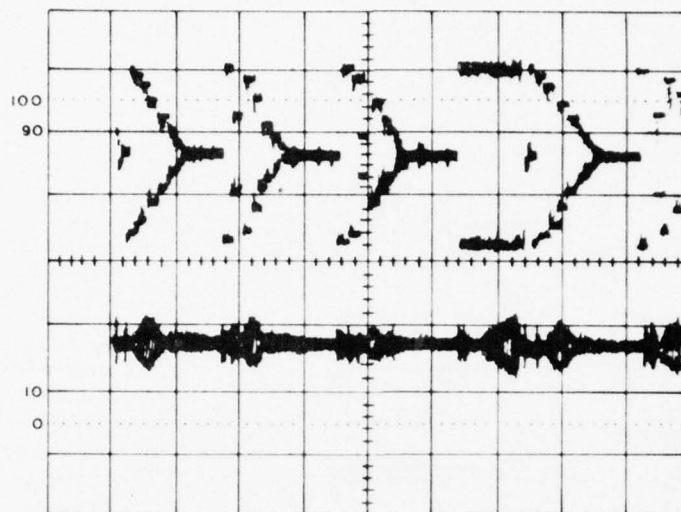


Oscilloscope externally triggered from pin 31  
on the Memory and Multiplexor jack, time base  
5mS/div.

Fig. 2.4(5)

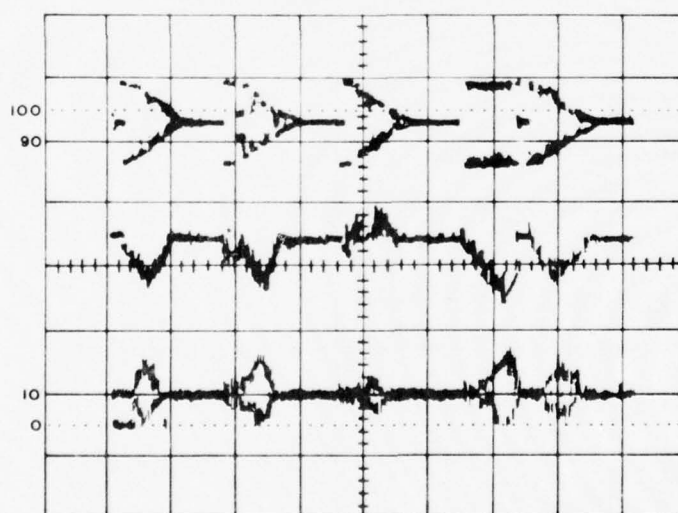
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# COMPARATOR TEST POINTS



Comparator Test Point 1  
1 volt/div.

Comparator Test Point 6  
200 mv/div.



Comparator Test Point 4  
2 volts/div.

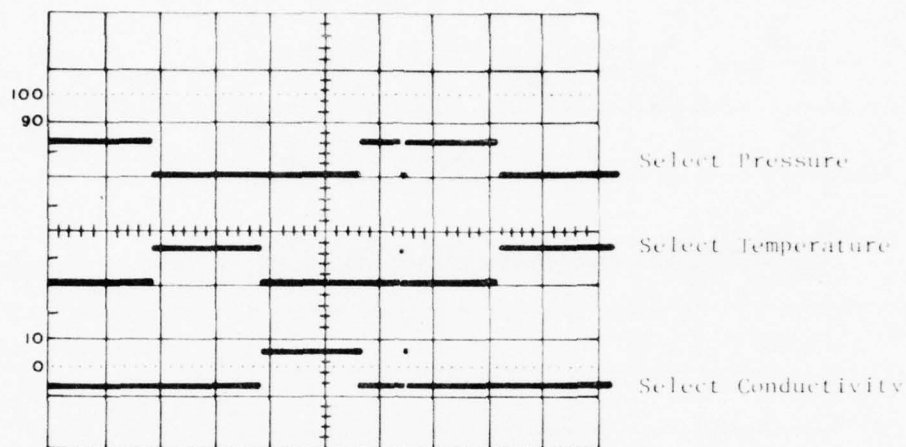
Comparator Test Point 5  
1 volt/div.

Comparator Test Point 6  
200 mv/div.

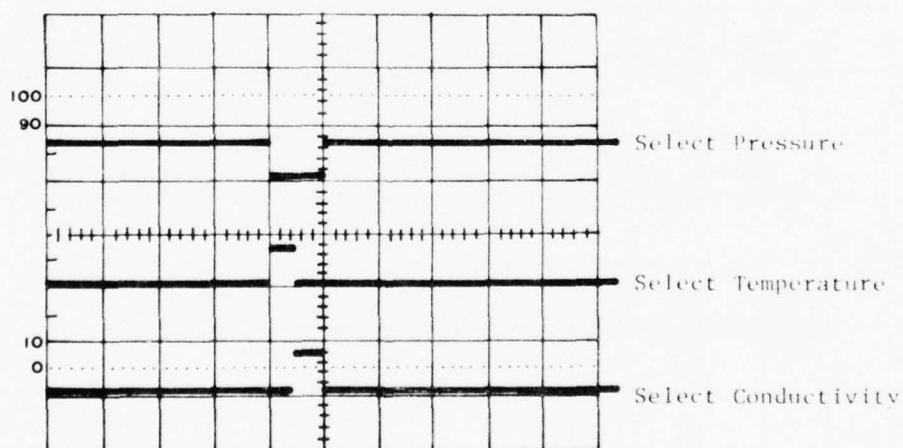
Oscilloscope externally triggered from pin 31 on the memory and multiplexor jack, time base 5 ms/div.

Fig. 2.4(6)

# MEMORY AND MULTIPLEXOR



Oscilloscope externally triggered from pin 31 on Memory and Multiplexor jack all traces 20 volts/div., time base 5 mS/div.

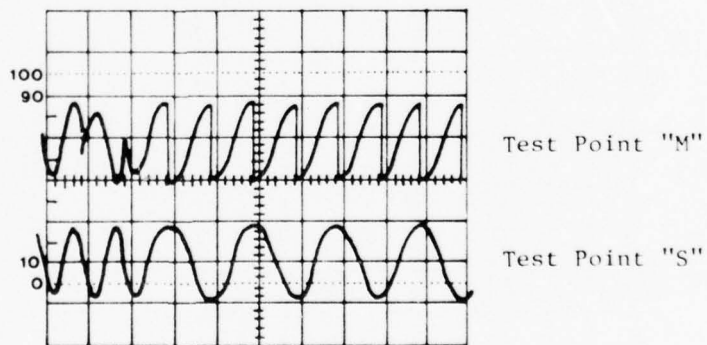
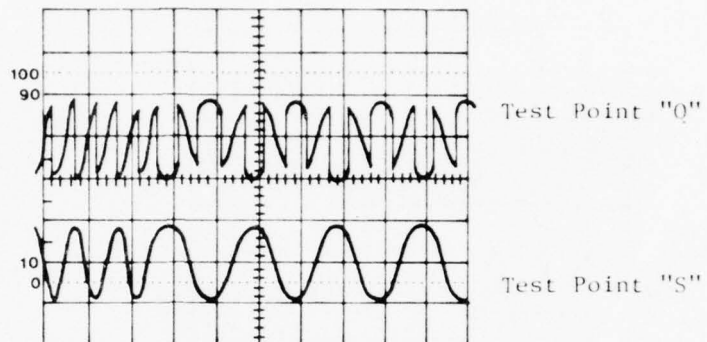


Expansion of "read cycle" approximately 32 mS after start of above trace, time base 200  $\mu$ S/div., sens 20 volts/div.



Fig. 2.4(7)

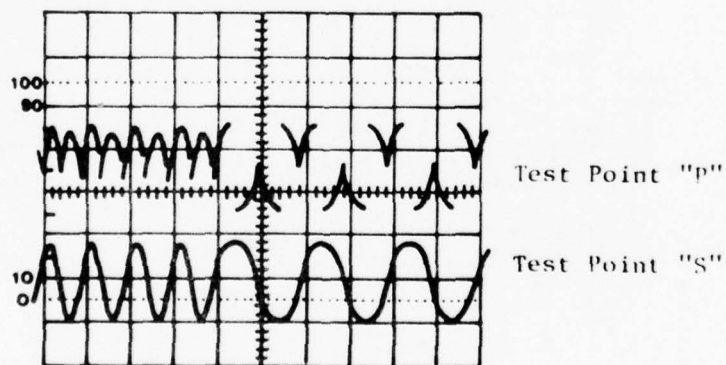
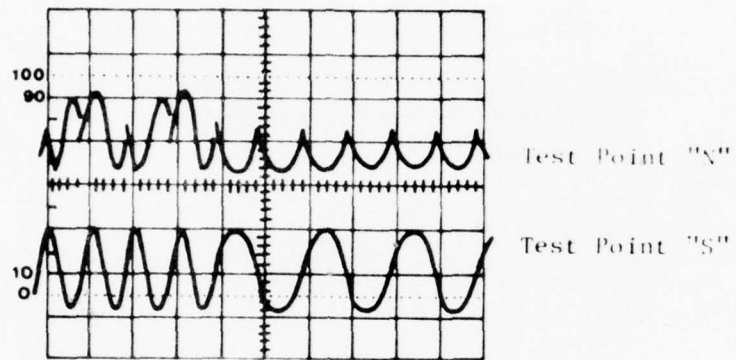
DEMODULATOR TEST POINTS



Oscilloscope sensitivity 2 volts/div.,  
time base 100  $\mu$ s/div.

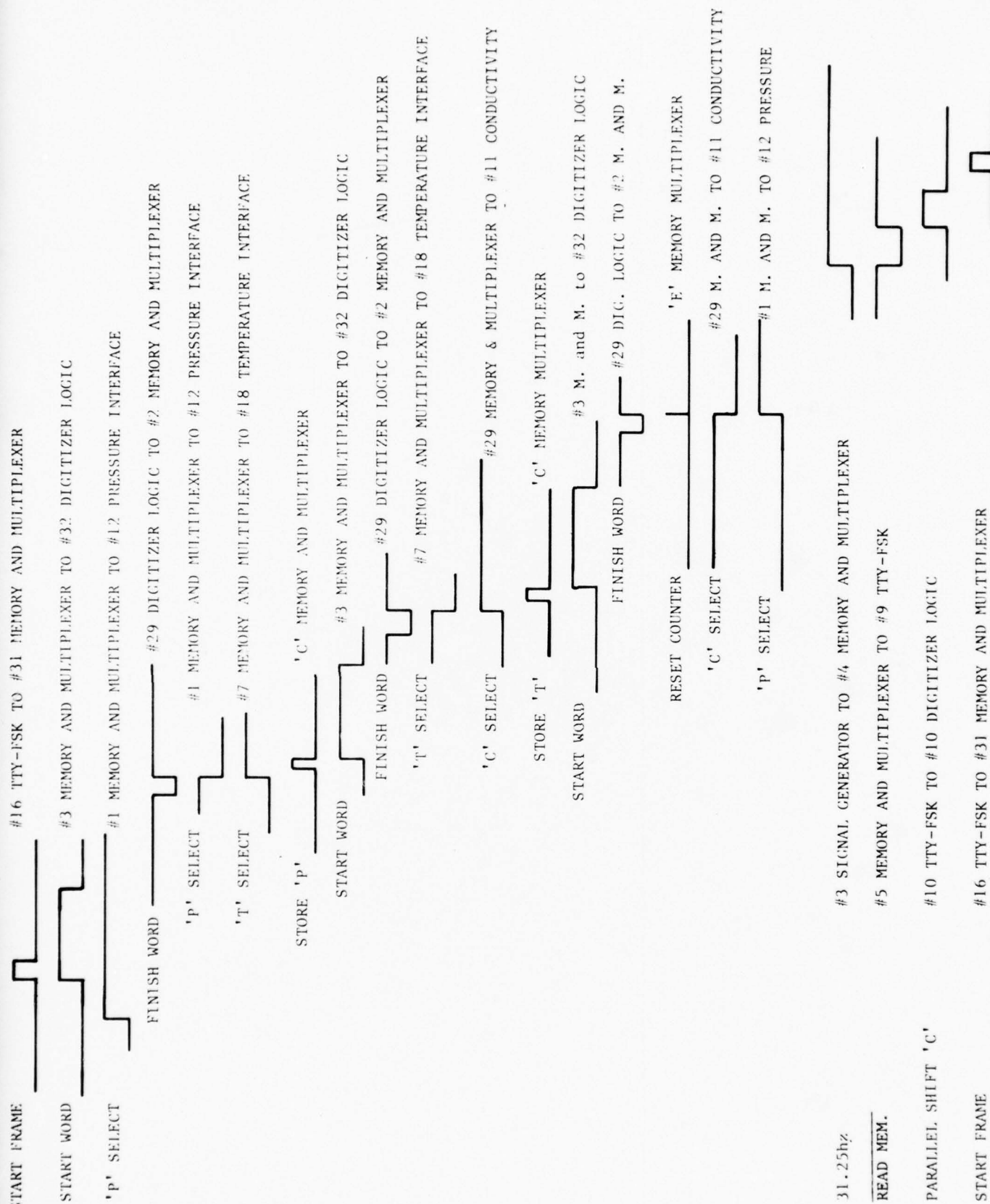
Fig. 2.4(8)

DEMODULATOR TEST POINTS



Oscilloscope sensitivity 2 volts/div.,  
time base 100  $\mu$ s/div.





## CIRCUIT DESCRIPTIONS

<u>Circuit Jack #</u>	<u>Underwater Unit</u>	<u>Part Number</u>	<u>Page</u>
J1	Pressure Interface	001-PC-01-2	3.1.1
J2	Temperature Interface	002-PC-01-2	3.1.2
J3	Fast Response Temp. Interface	003-PC-01-1	3.1.3
J4	Conductivity Interface	004-PC-01-2	3.1.4
J5	Oxygen Interface (Optional)	020-PC-01-0	3.1.5
J6	Power Supply (U.W.U)	008-PC-01-0	3.1.6
J7	Comparator	005-PC-01-1	3.1.7
J8	D/A Converter	006-PC-01-1	3.1.8
J9	Digitizer Logic	007-PC-01-1	3.1.9
J10	Memory & Multiplexer	010-PC-01-1	3.1.10
J11	Adaptive Sampling	C10009-	3.1.11
J12	TTY Formatter & FSK Modulator	014-PC-01-1	3.1.12
J13	Signal Generator	C10066-	3.1.13
<u>Circuit Jack #</u>	<u>Deck Unit</u>	<u>Part Number</u>	<u>Page</u>
J1-J2(D)	Display Card	016-PC-02-1	3.2.1
J3-J4(D)	Number Converter	015-PC-02-0	3.2.2
J5-J6(D)	D/A Converter	017-PC-02-1	3.2.3
J7-J8(D)	Demodulator	014-PC-02-1	3.2.4
J9-J10(D)	Option Card		3.2.5
	Power Supply (D.U.)	018-PC-02-0	3.2.6
	Chassis Mounted Circuits		3.2.7



## PRESSURE INTERFACE

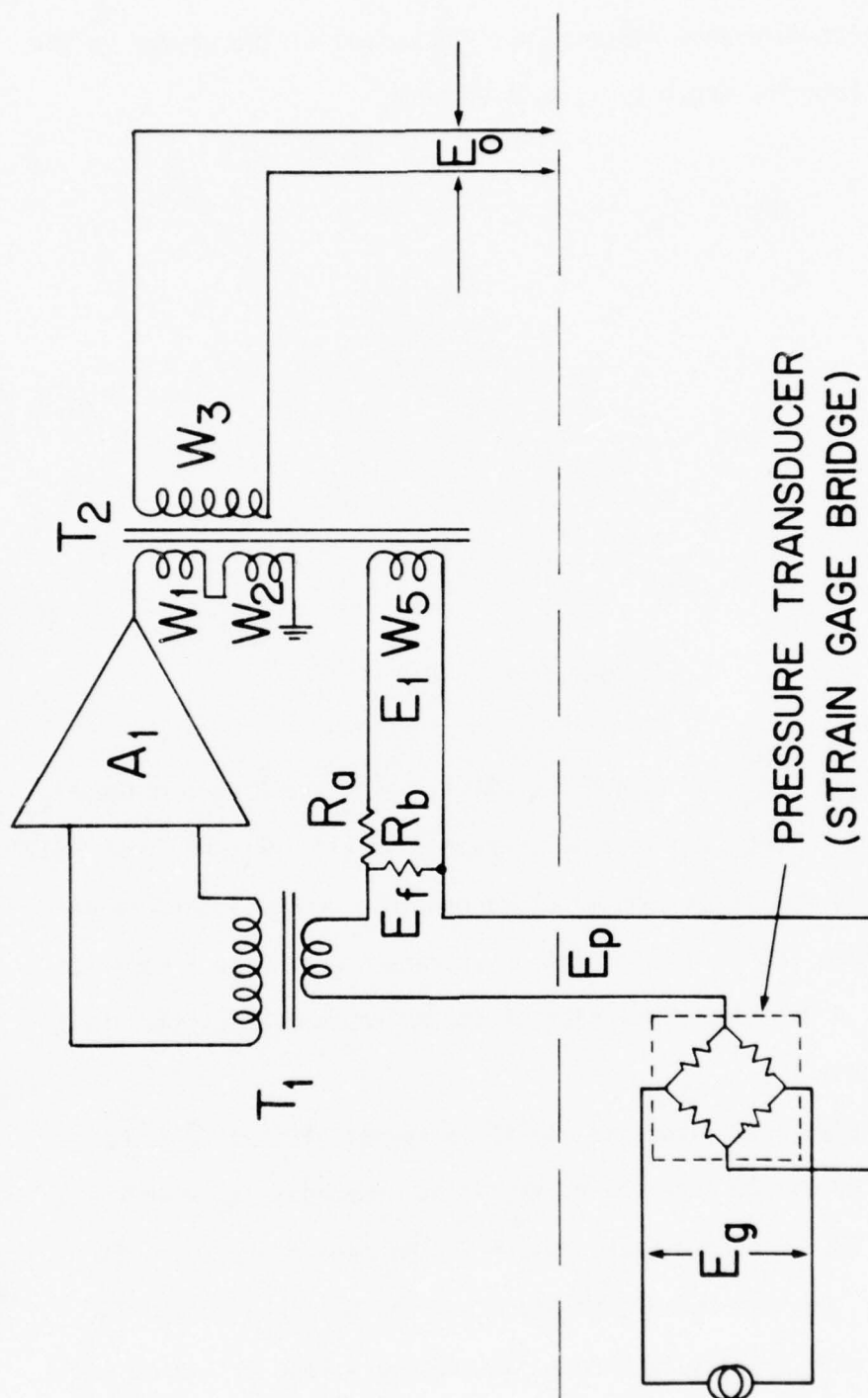
Pressure Interface: The pressure transducer is a 350 ohm bonded wire strain gauge bridge (Standard Control Inc. Model #211-35-440). Field and laboratory experience with this transducer has shown overall accuracy consistently better than  $\pm 0.1\%$  of full scale (Typical full scale is 6500 decibars).

Pressure Transducer Interface Circuit: The purpose of the interface circuit is to match the characteristics of the sensor to the requirements of the digitizer. The pressure transducer output is 2.5 millivolts full scale per volt of excitation, and the transducer is rated at 10 volts. To conserve power, the 10 kilohertz excitation is limited to 2 volts R.M.S. for an output range of 0 to 5 millivolts.

The digitizer measures the ratio of the sensor interface output voltage to the reference voltage, and full scale output (all "ones") from the digitizer occurs when the sensor interface output (digitizer input) is 500 millivolts. Consequently, the transducer output of 5 millivolts must be amplified by 100.

For overall accuracy and stability, it is critical that the gain and phase characteristics of the ac amplifier be extremely stable. Referring to the simplified schematic, Figure 3.1.1 assume the open loop gain ( $A_0$ ) of the feed-back amplifier consisting of  $T_1$ ,  $A_1$  and  $T_2$  is infinite, and the feed-back from winding  $W_5$  is negative; it can be shown by operational amplifier theory that the input to  $T_1$  is zero. The pressure transducer is shown as the Wheatstone bridge excited by

Fig. 3.1.1



the 10 kilohertz reference voltage  $E_g$ . The output of the bridge is the signal  $E_p$ . Since the input to  $T_1$  must be zero,

$$\begin{aligned} \text{then } E_p &= -E_f \\ &= E_1 \frac{R_b}{R_a + R_b} \end{aligned}$$

$$E_1 = E_0 \frac{W_5}{W_3}$$

$$\text{so } \frac{E_0}{E_p} = \frac{W_3}{W_5} \frac{R_a + R_b}{R_b}$$

= closed loop gain.

Since the ratio of  $\frac{W_3}{W_5}$  on  $T_2$  and the values of  $R_a$  and  $R_b$  are extremely stable the closed loop gain is also extremely stable.  $R_a$  and  $R_b$  are S102 Precision Vishay resistors mounted close together on the interface card, and  $W_3$  and  $W_5$  are the fixed windings on a transformer, also a very stable quantity. A detailed discussion of the ac feedback amplifier is given in Appendix 7.1.

The stable 10 kilohertz amplifier represented as  $A_1$  is made up of Q1, Q2, Q3 and Q5 with their associated components between transformer T1 and T2. The feed-back network is composed of the resistor network P4, R7, R8, R20 and a quadrature nulling network, P5 and C4. Both in-phase and quadrature zero adjustments are made by adding small fractions of the bridge excitation signal  $E_g$  into the input of  $A_1$

through networks P2, R6, R21, R22 and P3, C3 respectively to cancel fixed offsets.

To compensate for possible nonlinearity in the pressure transducer, winding W4 and resistors R4 and R5 are provided. By means of the link J1 it is possible to connect the linearize feed-back winding in such a manner as to increase or decrease the output corresponding to the maximum pressure. In normal use R5 is left open-circuit and R4 is a short-circuit. Unfortunately, the strain gauge pressure transducer is sensitive to large changes in temperature which the instrument will experience as it is lowered through the ocean from the surface to the cold deep water at the bottom. To compensate for this apparent pressure reading caused by temperature, a temperature compensation circuit is provided. The temperature of the pressure transducer is monitored by a thermistor connected across pins 25 and 26 of the interface card. The thermistor is the variable in a bridge which includes the primary of transformer, T3, and resistor, R1. This network is excited by the reference voltage  $E_g$  or half of the reference voltage,  $E_g/2$ , depending upon the position of jumper, JS. The voltage appearing across the primary of T3, therefore, is a function of the out-of-balance or difference in resistance of the thermistor and resistor R1.

Temperature compensation is made as an offset correction at zero pressure, and a sensitivity correction at full scale pressure. The offset is adjusted at  $0^{\circ}\text{C}$  and zero pressure with "TC" potentiometer, P1; the sensitivity is corrected automatically by slightly increasing or decreasing the transducer excitation as a function of temperature. The

sense and magnitude of the correction is determined by jumpers JR and JT on T3. Adjustment of the temperature compensation is described in the test and calibration section, 2.3; these tests require a pressure standard and an ice bath.

The bipolar outputs of the pressure interface appear on windings 6 and 3 on transformer T2. By means of Q4 and Q6 in conjunction with IC1 and resistors R18, R19 and diodes CR1, CR4, CR5 and CR6 the appropriate output is selected and connected to the digitizer at the appropriate time during the digitization cycle. The output transformer T2 has a center tapped winding W3 - W6. The center tap is connected to the analog common and output signals  $+E_s$  and  $-E_s$  are connected to switches Q4 and Q6 respectively. IC1 examines the pressure select and sign lines and presents the appropriate signals to the digitizer under the control of the digitizer logic and memory and multiplexer circuits.



## TEMPERATURE INTERFACE

Sensor: The temperature sensor is dual 100 ohm element platinum resistance thermometer manufactured by Rosemount Engineering Co., their model 171-BJ.

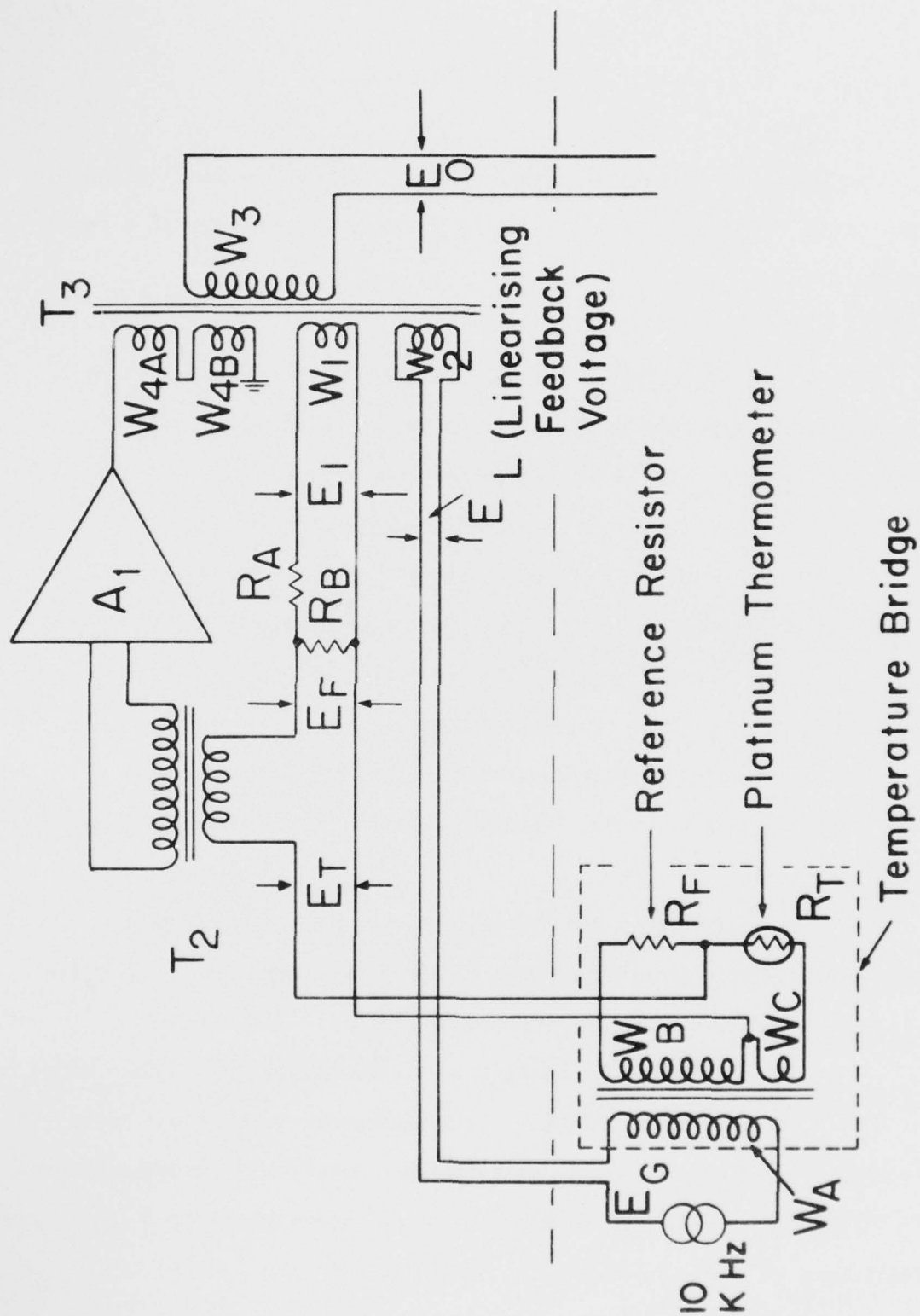
Temperature Interface: The platinum thermometer interface circuit is essentially the same as for pressure and is shown in simplified schematic, Figure 3.1.2. The differences are the form of the sensor bridge and the addition of a "linearizing" feed-back signal.

The sensor bridge is made up of the platinum thermometer,  $R_T$ , a precision reference resistor,  $R_F$  and the two windings,  $W_B$  and  $W_C$  of the bridge transformer. The transformer bridge offers several advantages over a conventional four resistor bridge.

- 1) It provides efficient matching to the signal source.
- 2) It has lower output impedance, leading to a lower signal to noise ratio.
- 3) It requires only one precision resistor instead of three.
- 4) The ratio transformer arms  $W_B$  and  $W_C$  have essentially no ratio error or drift with temperature or time.

The platinum thermometer resistance is 200 ohms at 20° (185.3 ohms at 0°C), and self-heating effects limit the maximum permissible current to 1mA. In the platinum thermometer bridge, sensitivity is greatest when  $R_F$  is infinite; since the actual value of  $R_F$  is ten times the 0°C resistance of the thermometer, the sensitivity is about 90% of the

Fig. 3.1.2



theoretical maximum.

The resistance-temperature characteristic of platinum resistance thermometers is not perfectly linear, and since  $R_F$  is a finite value, the current through  $R_F$  and  $R_T$  decreases with increasing temperature and results in increasing values of  $P_T$ , reducing the incremental sensitivity. The temperature interface adds a linearizing voltage,  $E_L$ , to the 10 kHz reference voltage,  $E_G$ .

The addition of  $E_L$  to the generator voltage  $E_G$  increases the excitation voltage to the bridge as the temperature increases, negating the decrease in incremental sensitivity.

Combination of the platinum thermometer and interface circuit above result in a 10 kHz output of 0 to 500 millivolts between  $0^\circ\text{C}$  and  $32.767^\circ\text{C}$  to  $\pm 0.0015^\circ\text{C}$  with long term stability within  $0.005^\circ\text{C}$  per year. The response time of the thermometer is typically 250 milliseconds while the response time of the conductivity cell when moving through the water at 1 meter per second is typically 25 milliseconds. Salinity computed from the output of these two sensors alone results in "salinity spikes" when a sharp temperature gradient is encountered. These "spikes" can be reduced by computing a temperature lag correction from a running average of the two sensor readings, resulting in "smoothed" salinity data.

To more nearly match the thermal characteristics of the temperature and conductivity sensors, a technique is used to combine the high frequency response of a thermistor with the low frequency response of the platinum probe. These fast response thermistor circuits are described in Section 3.1.3.

Circuit: Amplifier  $A_1$  is the discrete component amplifier with input

transformer T2 and output transformer T3. (A theoretical discussion of this amplifier is found in appendix 7.1). Feedback resistors  $R_A$  and  $R_B$  are formed by the resistive network R12, R13, R14 and P3. Resistors R1, R2, R3 and P2 permit zero adjustment, and the quadrature is nulled using P1 and C1.

The platinum thermometer, transformer, T1, and reference resistor,  $R_F$ , are mounted in the sensor head. Turns ratio  $W_B/W_C$  and the resistive ratio  $R_F:(R_{t1} + R_{t2})$  at  $0^\circ\text{C}$  is designed so that the bridge output will be zero at  $0^\circ\text{C}$ . To linearize the bridge output, the "linearize" winding W2 is connected to increase the drive to the sensor bridge with increasing temperature. The modulated 10 kHz signal is output to the digitizer by switch Q4 or Q6 as controlled by gate IC1. The center tap of the output transformer is connected to signal common.

## FAST RESPONSE TEMPERATURE INTERFACE

Sensor: The fast response temperature measurement is done with a miniature thermistor probe, with a 25 ms time constant, Fenwal No. GC32SM2 mounted on a ceramic paddle. This sensor is used with an electronic servo balanced bridge excited at 10kHz; the output from the bridge is precisely zero for steady state conditions. However, whenever temperature changes rapidly, the presence of an integrator in the control loop results in an exponentially decaying "error" signal.

With proper adjustment of an integrator time constant the response time of the servo is made equal to the response time of the platinum thermometer, and the bridge amplitude response is adjusted so the "error" signal is equal to the lag error in the reading of the platinum thermometer. The sum of these two signals results in a 10kHz output signal with the excellent linearity and stability of the platinum thermometer and the fast thermal response of the thermistor. An electrical analogy of this scheme is illustrated in Fig. 3.1.3.

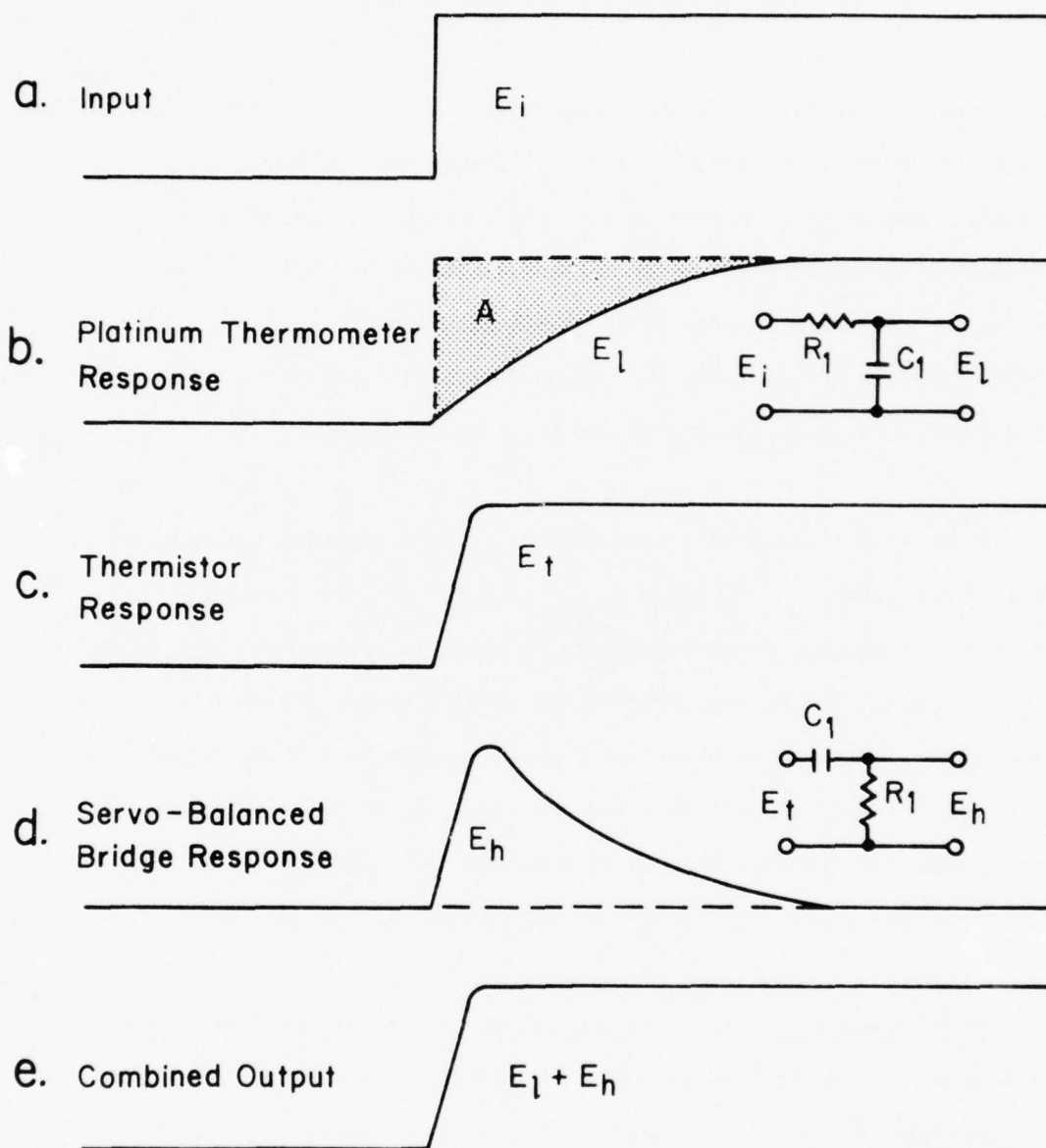
Fast Response Circuit: The equivalent circuit of the fast response interface is shown in Fig. 3.1.3(2). Windings  $W_2$  and  $W_3$  of transformer  $T_1$ , resistor  $R_F$  and thermistor  $R_T$  form a bridge circuit which is excited by a 10 kHz signal  $E_g$  across winding  $W_1$  of transformer  $T_1$ .

.. Under steady state conditions  $E_1 = E_t - E_m = 0$  volts.

A step change in temperature causes a step change in the resistance



Fig. 3.1.3



of  $R_T$  which causes  $E_1$  to become non-zero.  $E_1$  amplified by  $A_1$  produces  $E_o$  which is synchronously detected by  $M_2$ . The resultant dc output from  $M_2$ ,  $E_d$ , is applied to an integrator  $A_2$  and the output  $E_c$  drives one input of multiplier  $M_1$ ; the other input of  $M_1$  is  $E_g$  from winding  $W_4$  of transformer,  $T_1$ . The 10 kHz output of  $M_1$ ,  $E_m$ , will change so as to reduce  $E_1$  to zero at a rate determined by the gain of the servo loop and the integrator time constant. The rate at which  $E_1$  is returned to zero is carefully adjusted to match the response time of the platinum thermometer.

A detailed theoretical description is given in Appendix 7.2.

Fast Response Circuit Description: Compare Fig. 3.1.3(2) with schematic Fig. 5.1.3

$A_1$  - is op amp IC2/1 and its associated components

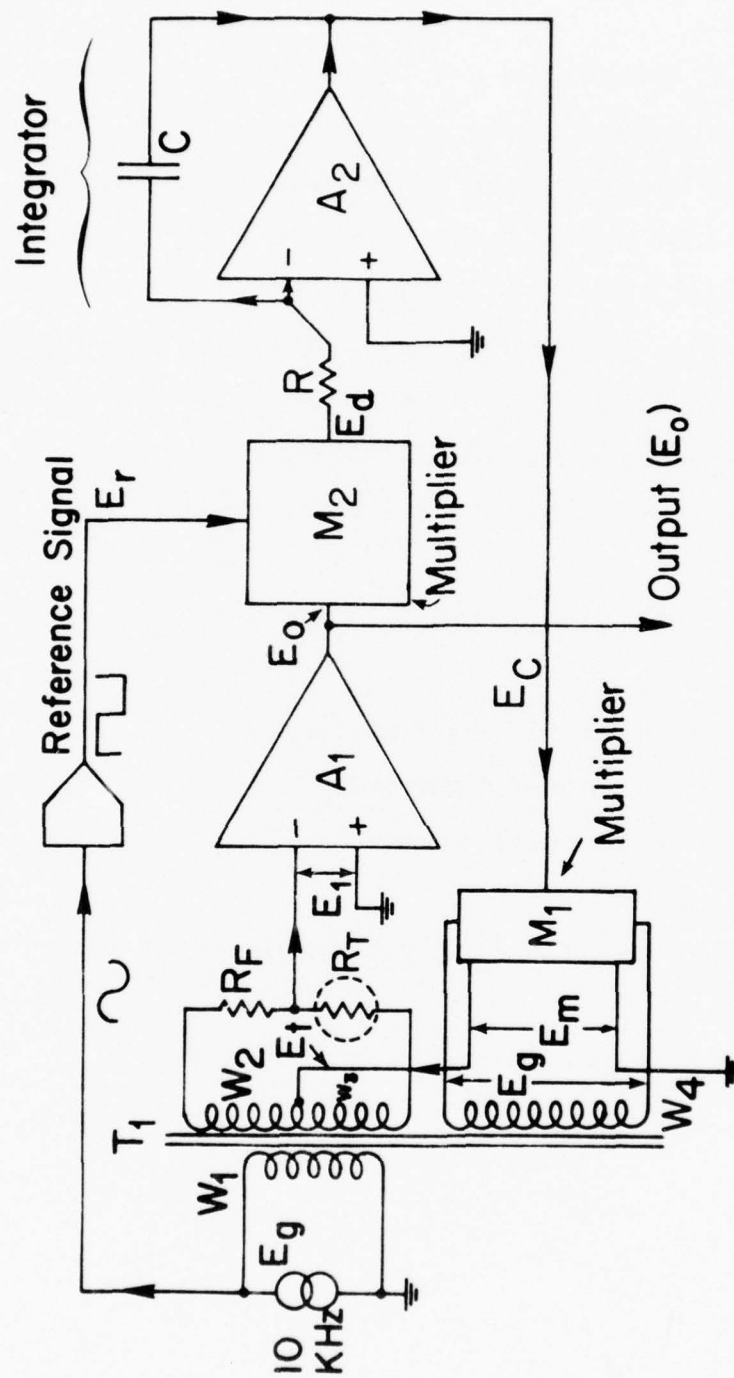
$M_2$  - is IC3, and its associated components

$A_2$  - is IC4 and its associated components,

R - is R9 and C is C12

IC2/13 inverts the output of  $A_2$ , R, C to provide complementary outputs to drive  $M_1$ .

Set up instructions for this circuit are given in Section 2.3.



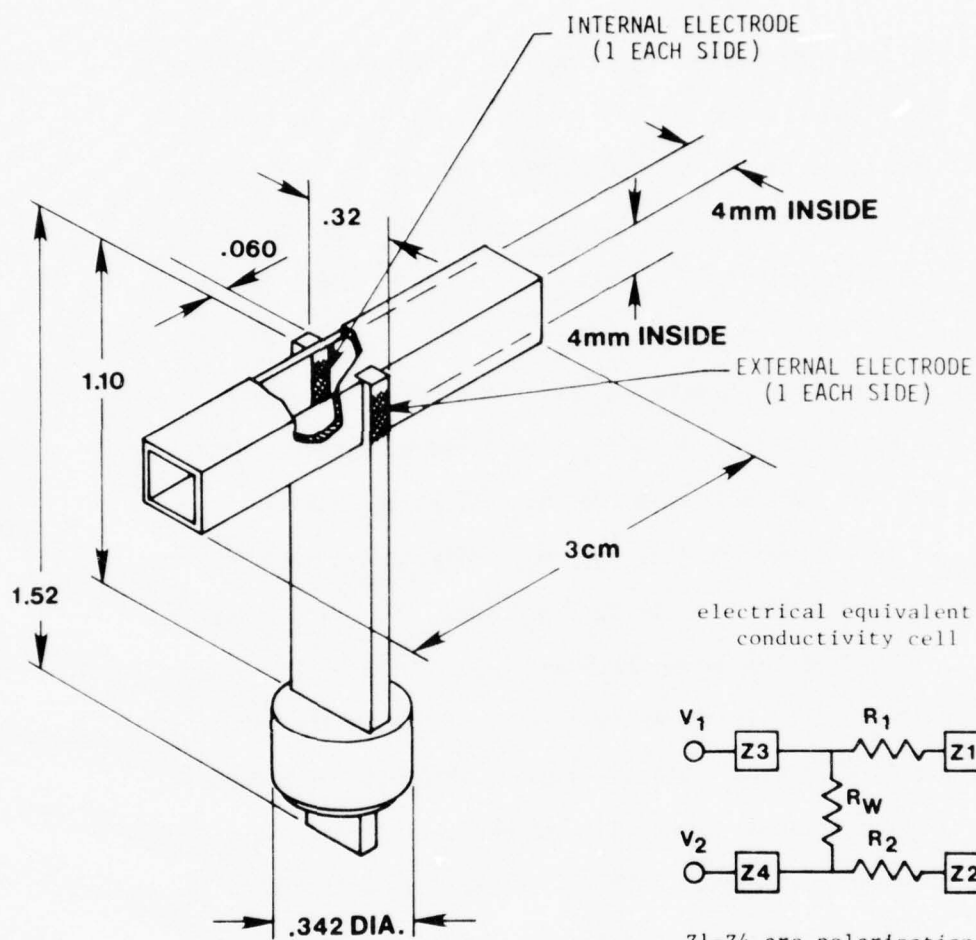
## Rt=Fast Response Thermistor

## CONDUCTIVITY SENSOR INTERFACE

The CTD has a miniature four electrode conductivity cell for measuring sea water conductivity. This type of sensor has the particular advantage that conductance (defined as the ratio of current through the "current electrodes" to the open circuit voltage at the "potential electrodes") is independent of polarization impedance effects. These effects are due to electro-chemical reactions at the electrode-electrolyte interface and are very dependent on surface cleanliness of the electrodes and other factors which make a simple two electrode cell too unpredictable for high accuracy measurements. Unlike an inductively-coupled cell, the four electrode cell can be readily scaled down in size without loss of accuracy due to electrical problems. However, since conductivity is a function of conductance and cell geometry, it should be noted that a small cell is inherently more sensitive to the effect of deposits on the cell wall simply because a given thickness of a deposit represents a larger fractional change in apparent cell dimensions.

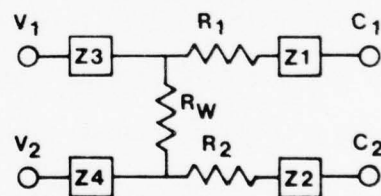
The original cylindrical cell was observed to drift at an increasing rate, with the initial rate typically equivalent to .0001 to .0005 parts per thousand salinity per hour of immersion (Fofonoff, Hayes and Millard, 1974). This drift is believed to be due to calcium and/or magnesium carbonate deposits on the inside surfaces of the ceramic structure. A 0.00002 millimeter deposit on the 2 millimeters inside diameter of the microstructure cell causes an apparent change in salinity of approximately .0008 parts per thousand (for  $S = 35$  ppt) due entirely

Fig. 3.1.4



GENERAL PURPOSE  
CONDUCTIVITY CELL  
(3cm HEAD)

electrical equivalent of  
conductivity cell



$Z_1$ - $Z_4$  are polarization impedance  
at each electrode surface

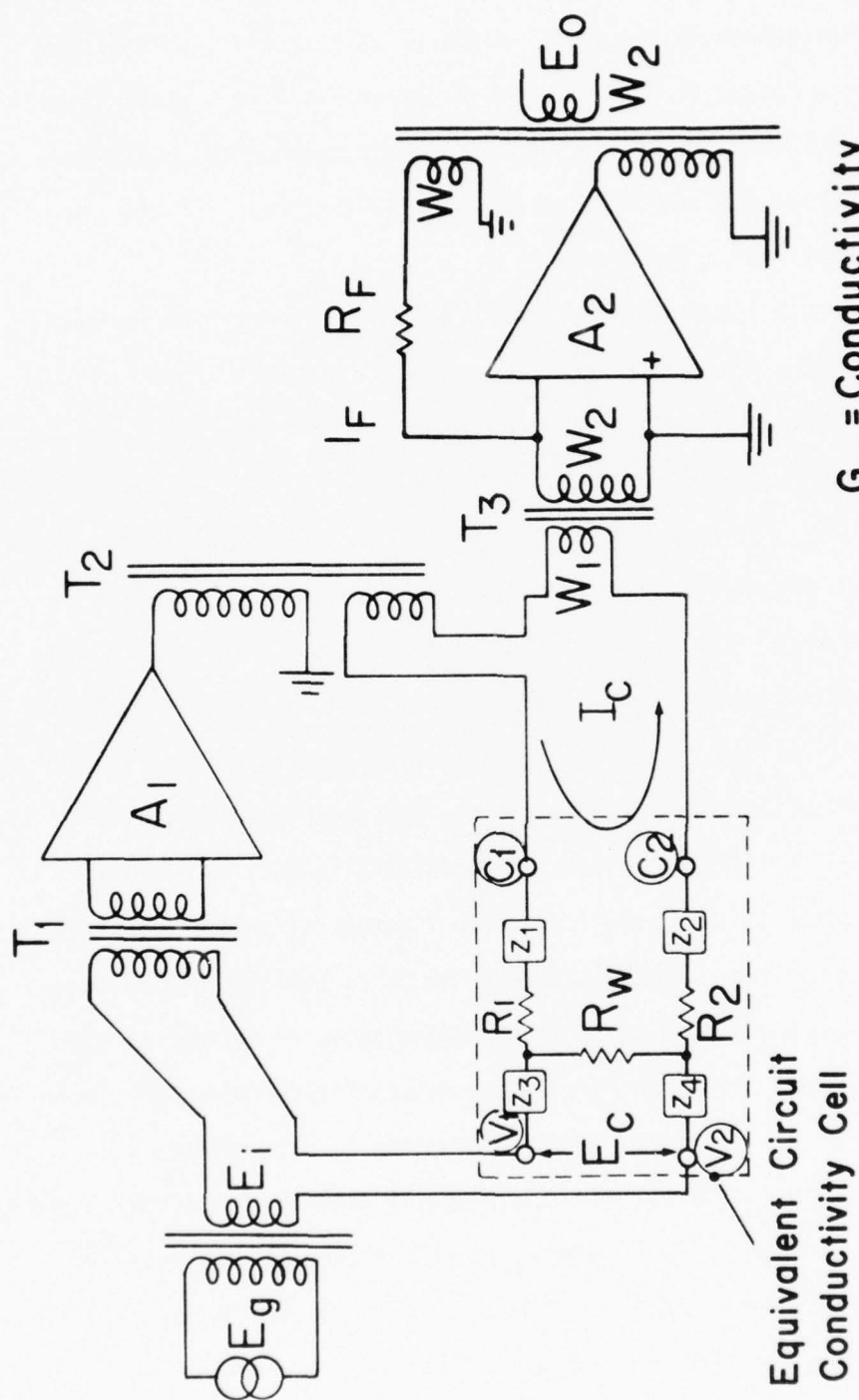


to the apparent change in the inside diameter of the cell. This effect is reduced by a factor of 4 in the general purpose cell now standard on the Mark IIb CTD and calibration is restored by soaking the cell in a solution of 1 part General Chemical Co. Saline Dissolvent diluted with 25 parts of water, for a few minutes.

Figure 3.1.4 shows a cut-away view of the four electrode conductivity sensor and an equivalent electrical circuit of the cell. Two of the four electrodes are opposite each other on the inner wall of a .4cm square ceramic tube 3 cm long. The other two electrodes are mounted externally on the stem; four electrodes are in the same plane normal to the axis of the sensor. This geometry has the advantage of being relatively insensitive to apparent changes in position of the electrodes due to non-uniform contamination. This can be seen from Figure 3.1.4(2) which shows the current flow lines and the resulting equipotential lines in the tubular section of the sensor head. Equipotential lines in the vicinity of the "voltage" electrodes are essentially parallel to the "voltage" electrodes, i.e., the longitudinal potential gradient is very small. This means that a small apparent change in position due to non-uniform contamination would cause negligible changes in voltage at the "voltage" electrode. The symmetry of the external electrodes and their wider separation result in even greater immunity to this effect.

Referring to the equivalent electrical circuit of the cell, Figure 3.1.4, impedances  $Z_1$  through  $Z_4$  are the polarization impedances at each electrode-electrolyte interface.  $R_1$  and  $R_2$  are the sea water path resistances from the "current" electrodes to the points in the

Fig. 3.1.4(2)



$G_w$  = Conductivity

$K$  = Cell Constant

electrolyte sea water, paths having the same potential as the "voltage" electrodes.  $R_w$  represents the remaining sea water path and is measured by observing the ratio of the open circuit voltage across the "voltage" electrodes  $V_1$  and  $V_2$  to the current through the "current" electrodes  $C_1$  and  $C_2$ .

$$R_w = \frac{E_c}{I_c}$$

$$\text{so } G_w = \frac{1}{R_w} = \frac{I_c}{E_c} = \text{conductance.}$$

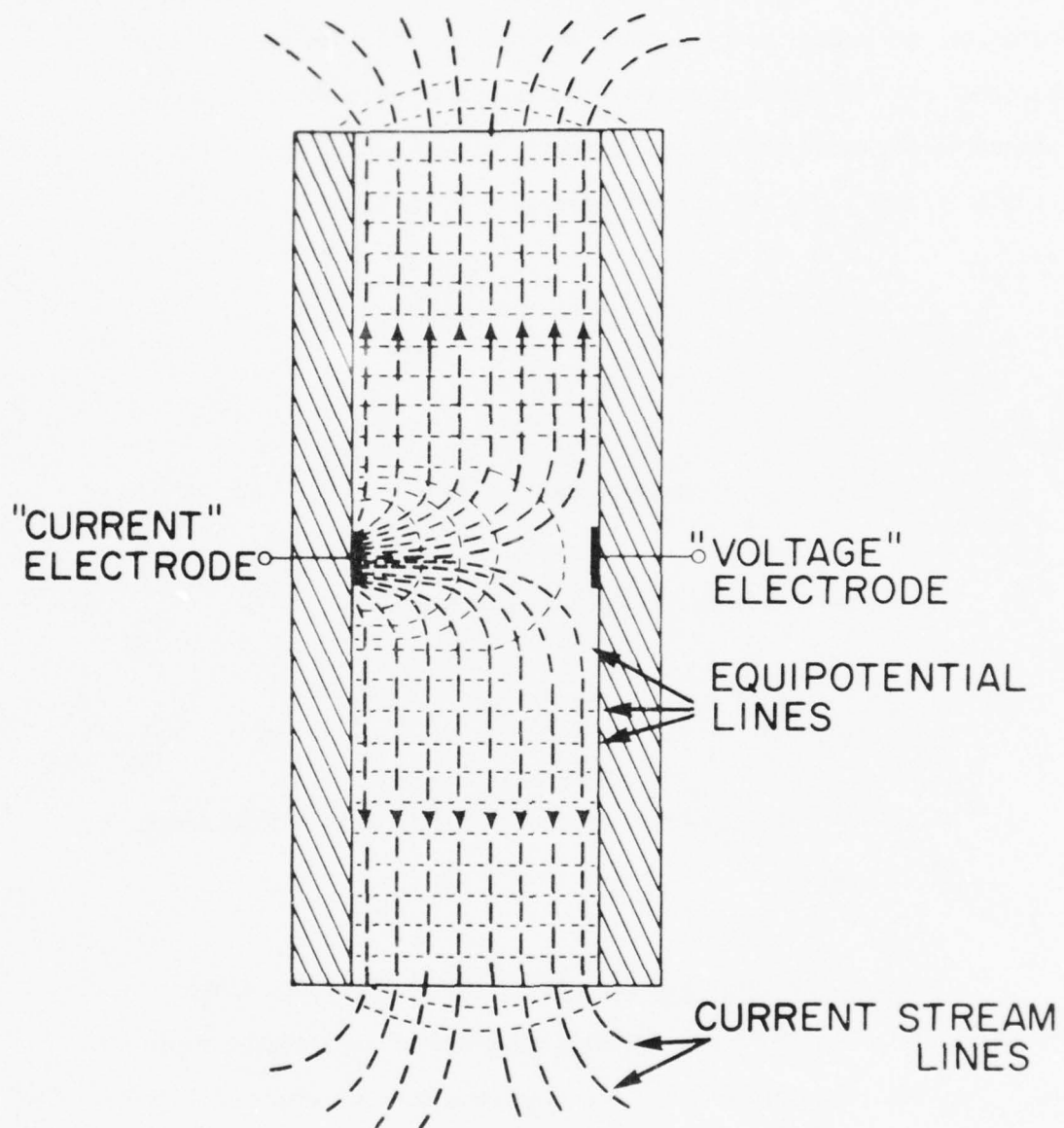
Therefore the conductivity  $G$  is given by

$$G = K \frac{I_c}{E_c} = KG_w$$

where  $K$  = cell constant, dependent on the physical dimensions of the cell.

Conductivity Interface Circuits: The conductivity sensor interface circuit shown in Figure 3.1.4(3) consists of two feed-back circuits. The first consists of the four electrode conductivity cell, transformers  $T_1$  and  $T_2$ , and high gain feed-back amplifier  $A_1$ . The input signal to  $A_1$  through  $T_1$  is the difference between the 10 kilohertz input reference voltage  $E_i$  and the voltage across the voltage electrodes  $V_1$  and  $V_2$  of the conductivity cell. Assuming  $A_1$  has infinite gain and the feed-back is negative, then the voltage  $E_c$  will be exactly equal to input

Fig. 3.1.4(3)



reference  $E_i$ , since

$$E_c = I_c R_w = E_i$$

$$I_c = \frac{E_i}{R_w}$$

$$= E_i G_w$$

where  $G_w$  = conductance of sea water path.

The cell current  $I_c$  is applied to the input transformer  $T_3$  of the second feed-back circuit which consists of  $T_3$ ,  $A_2$ , output transformer  $T_4$  and feed-back resistor  $R_f$ . Negative feed-back through  $A_2$  and  $T_4$  will result in a feed back current  $I_f$  through winding  $w_2$  on  $T_3$  such that

$$I_f w_2 = I_c w_1 \quad (w_1, w_2 \text{ on } T_3) \text{ and } I_f = I_c \left( \frac{w_1}{w_2} \right)$$

$$\text{now } E_o = I_f R_f$$

$$= I_c R_f \left( \frac{w_1}{w_2} \right) \text{ but } I_c = \frac{E_i}{R_w} = E_i G_w$$

$$= E_i G_w R_f \left( \frac{w_1}{w_2} \right) \text{ if } G_w = gK, \text{ then}$$

$$E_o = gK E_i R_f \left( \frac{w_1}{w_2} \right) \quad \frac{E_o}{E_i} = gK R_f \left( \frac{w_1}{w_2} \right)$$

$$\text{therefore } \frac{E_o}{E_i} = gK_1$$



$$\text{therefore } \frac{E_o}{E_i} = gK_1$$

where  $K_1 = KR_f \left( \frac{W_1}{W_2} \right)$ , a circuit constant.

The ratio of the conductivity interface circuit output voltage to input reference voltage,  $\frac{E_o}{E_i}$ , is proportional to the conductivity,  $g$ , of the sea water inside and immediately around the conductivity cell.

The current source  $A_1$  which drives a current through the conductivity cell in order to generate a voltage  $E_c$  equal and opposite to  $E_i$  is made up of the components labeled "Conductivity to Current Converter" between transformers T1 and T2 on the Conductivity interface schematic. The current that is driven through the cell also excites the primary winding of T3. A second amplifier  $A_2$  labeled "current to voltage Amp." is made up from the components between transformers T3 and T4. The plug-in feedback circuit  $R_f$  is a very stable resistor network made up of components P2, R10, R11, and R17, and determines the thermal stability of this interface. Zero offset and quadrature errors are nulled using potentiometers P1 and P3.

Unlike the Pressure and Temperature circuits the output of the conductivity circuit is unipolar, and the analog gate is selected by the select conductivity signal independent of  $S_o$  and  $\bar{S}_o$ , the sign signals.

## OXYGEN INTERFACE (OPTIONAL)

Optionally, the MarkIIIb CTD/O provides an electrical interface to the Beckman polarographic dissolved oxygen sensor (Beckman p/n 147737 sensor, p/n 148184 sensor receptacle assembly). By means of this the electrode membrane current and sensor thermistor outputs are digitized and added to the CTD serial data stream. Sensor membrane current is presented at full scale value of  $2.047 \mu\text{A}$  and 12-bit resolution, while the thermistor output is linearized and offset to allow resolution of approximately 0.13 degrees C. Temperature information is presented as an 8-bit signed binary word having values between -15 and +241 corresponding to temperatures between -1.9 and +30.8 degrees C. Both  $\text{O}_2$  membrane current and  $\text{O}_2$  thermistor resistance are averaged by the electronics for 1.024 seconds.

Oxygen Sensor: The Beckman oxygen sensor is polarized at  $0.81\text{v} \pm 0.02\text{v}$  by the Mark IIIb CTD interface electronics. The  $\text{O}_2$  dependent sensor current is digitized by means of a current-to-frequency converter, the output of which is counted for 1.024 seconds. The counter output is thus a binary word with a value proportional to sensor current. The zero drift and linearity of this conversion are maintained within  $\pm 1/2$  LSB. The gain accuracy, i.e., full-scale current, is maintained  $\pm 0.1\% \pm 100\text{ppm/degree C}$ . This is sufficient to hold errors in the electronics an order of magnitude below sensor uncertainties.

Other full-scale current ranges for membrane current may be chosen by making  $R5 = 2.5/I_s$  where  $I_s$  is the desired full-scale.  $R5$  should be

a type RN60C of 1% value nearest the calculated resistance.

MEMBRANE TEMPERATURE: The Beckman sensor receptacle assembly incorporates a thermistor which allows an approximate determination of the internal membrane temperature. The Mark IIIb CTD interface electronics provides an 8-bit digitization of thermistor resistance. The accuracy of this conversion is such that an absolute determination of thermistor resistance to within 1 part in  $2^8$  may be obtained by means of the following relationship:

$$R_t = \frac{1}{mx + b} - R_s \quad \text{where } R_t \text{ is thermistor resistance at } T$$

$m$  &  $b$  are calibration constants

$x$  is the binary output of the temperature channel, with sign

$R_s$  is the value of a resistor used to optimize the temperature channel resolution and linearity

The calibration constants may be determined as follows:

$$m = \frac{\frac{1}{R_T + R_s} - \frac{1}{R_{T0} + R_s}}{240}$$

$$b = \frac{1}{R_{T0} + R_s}$$

where  $R_T$  is the thermistor resistance at 30.72 degrees

$R_{T0}$  is the thermistor resistance at 0 degrees C

$R_s$  is the linearization resistor defined above

The value 240 in the equation for  $m$  represents the difference between the digitizer output at 30.72 deg. and zero. The authors generate a table of R-T values for each sensor by making three accurate measurements

of thermistor resistance ( $\pm 0.1\%$ ) at three temperatures (approximately 0, 15, and 27 degrees C, absolute value within 0.01 degrees C). These values determine coefficients for a second order exponential equation which fits the range -2 to +31 degrees C within 0.0015 degrees C. The equation generates a table of R-T values spanning the calibration range of the interface. The electronics is then calibrated with a precision ( $\pm 0.01\%$ ) resistance decade box simulation of the tabulated thermistor resistance values.

The binary output of the temperature channel is multiplied by  $2^7$  and divided by 1000 in the CTD Data Terminal number converter. This results in a displayed temperature range of -1.9 to +30.7 degrees C. The temperature channel is calibrated by adjusting the interface electronics at 0 and 30.72 degrees C.

The maximum deviation from predicted temperature is approximately 0.25 degrees C, with zero error at 0, 30.7 and half-scale.

Data Format: The  $O_2$  membrane current is represented as a 16 bit word with the 4 most significant bits unconditionally set to zero. The 8 least significant bits are available at bit time 98, while the 8 most significant bits occur at bit time 109. The temperature channel output is the 8 bit word occurring at bit time 120. The  $O_2$  temperature sign is the third least significant bit in the sign word. The sign word occurs at bit time 087.

Power supply: Transformer T1 and diodes D1 through D4 with transistor Q1 form a floating d.c. power supply permitting the oxygen sensor to be powered without forming an electrical path to the CTD

housing. All logic signals between the d.c. digitizer and the remainder of the CTD circuitry are similarly ac coupled. This power supply generates approximately 10 volts across the diode bridge.

Oxygen Interface: The oxygen interface consists of two dc digitizers, one 12 bit and one 8 bit. These digitizers operate on a charge balancing technique. A counter stores the number of pulse of a fixed frequency which are required to produce an average current through a resistive network so as to exactly balance an unknown current for a given sampling time(1.024 seconds). Controlled reference voltage is applied to the polarographic oxygen sensor and a thermistor. The resulting currents which are a function of dissolved oxygen and sensor membrane temperature are input to the digitizers. The digitizer output is a 12 bit digital number proportional to the current between the polarographic sensor electrodes when a dc reference voltage is applied to them. The interface also digitizes to 8 bit resolution the current through a thermistor in the same sensor assembly when the same dc reference voltage is applied to it. These two numbers are used to compute dissolved oxygen by an appropriate algorithm.

Operational amplifier IC2 is wired as an integrating comparator which balances the  $O_2$  sensor current and the average current through resistors,  $R_5$  and  $P_1$ . Output D of flip-flop IC5/1 is initially set low and the current source for  $R_5$  and  $P_1$  becomes the negative supply. When the average current from this source is sufficient to null the integrated input to the comparator then D of IC5/1 is set high and the current in  $R_5$  and  $P_1$  is switched off. The length of time during which the current source is the negative supply is measured by gating



a 4 kHz clock into counter IC9 with  $\bar{Q}$  of IC5/1. If the maximum sensor current is flowing then  $\bar{Q}$  of IC 5/1 will be true for the entire 1.024 seconds sensor averaging time producing a maximum output of 4096 counts which is displayed as 2.048 $\mu$ A.

The temperature digitizer (IC3, IC5/13, IC4/13, IC4/12, IC6/5 & 14, IC11/13 & 10,) behaves in the same manner, except the zero is offset by summing a steady current from R6, R7 and P2 into the integrating comparator, IC3. In this case the maximum count will be 256 and a 250 hz clock is used. To provide bipolar output capability the circuit is arranged so no current flows through the thermistor at -1.9°C. The gated counter in this case combines a presetable count-down/count-up counter and a binary counter. Initially the up-down counter is set to 15 in the count down mode; when this counter reaches zero it is set to count up and the sign bit is set positive. Overflow from the counter is counted by the binary counter. The temperature channel has a minimum count of -15 and a maximum count of 241 and is displayed using E15 enable :  $10^3$ ; the oxygen temperature is displayed on the deck unit over a range of -1.9°C to +30.7°C.

IC7, IC8, IC11/1, IC12 and IC13 control the timing of the data transfer into the telemetry register.

## POWER SUPPLY - UNDERWATER

The input to the underwater unit power supply is unregulated dc from the deck unit which a zener diode mounted on the underwater unit card rack end plate limits to 22 volts. The regulated outputs are a low impedance 12 volt  $\pm 5\%$  supply with current limiting at approximately 120 mA and a 6 volt supply which is adjusted by a potentiometer to be equal to one-half the nominal 12 volt output  $\pm .01$  volts and current limits at approximately 40 mA.

Transistor Q3, diodes CR1, CR2, CR3 and resistors R10 and R19 form a constant current circuit which turns the darlington pair Q4 and Q5 hard on. The Q5 collector current flowing through CR5 and R15 generates a voltage across R15 which turns on Q7 causing it to pass current from the constant current source and adjust the zener current of CR5 to approximately 3mA. The collector current in Q5 is limited to about 120mA by R11 and Q6. When 120 mA is flowing through R11, Q6 turns on causing Q7 to conduct more current and starve the base of Q4. The maximum available 12 volt output current will therefore be 120 mA less the 3mA zener current and equal to 117 mA.

The output voltage is the sum of the CR5 zener voltage and the voltage drop across R15 or 12.3 volts,  $\pm 10\%$ .

The 6 volt supply is generated by regulator IC1. The level is adjusted by variable resistor, R6 and fixed resistors, R5 and R7. The current limit is set at 43 mA by resistor R9.

Transistors Q1 and Q2 with their associated resistors and diode perform no function in the standard Mark IIb CTD, but are used only when the system is operated with a battery pack; Q1 is normally replaced by the jumper indicated by a dotted line.

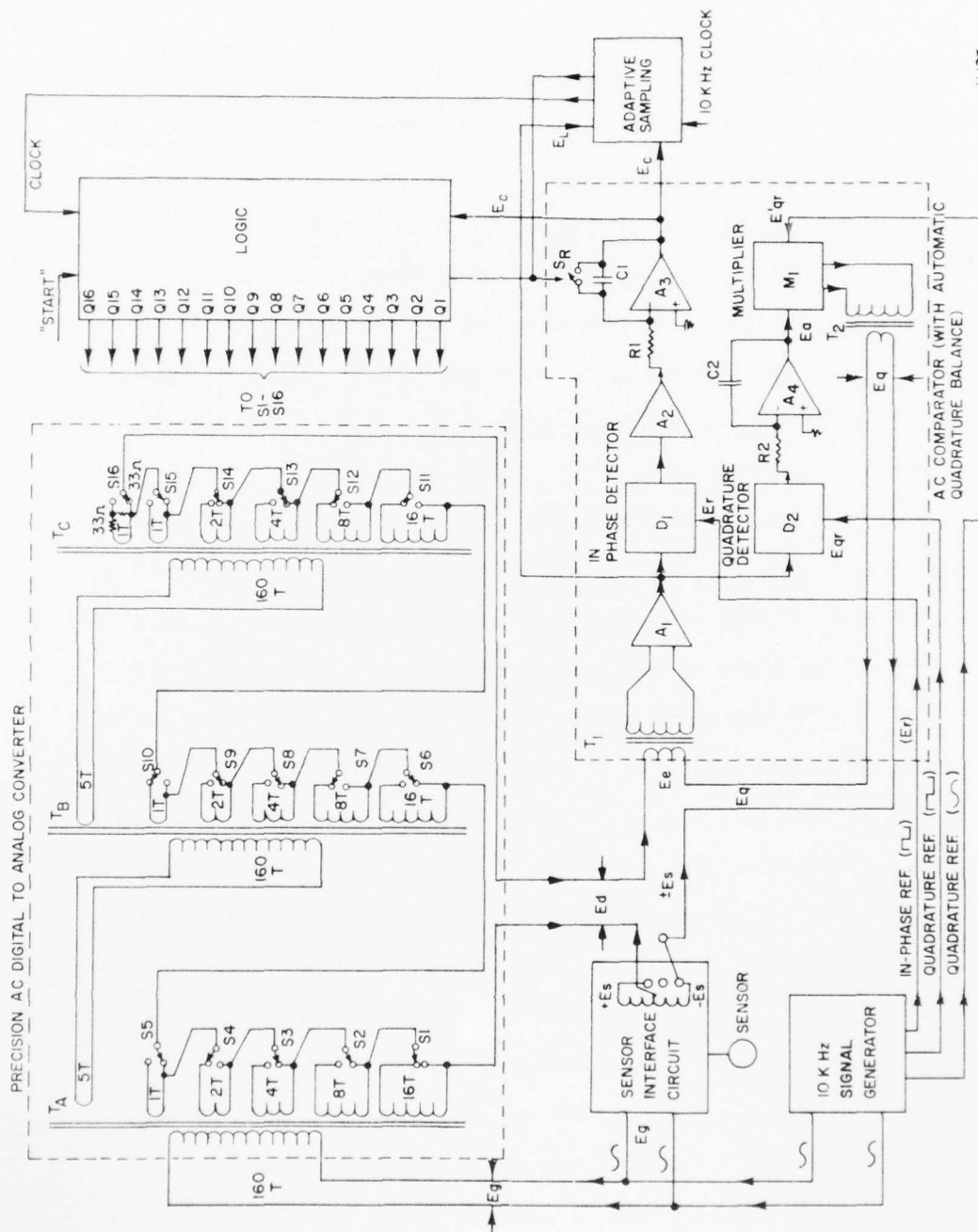
## AC COMPARATOR

The purpose of the AC comparator is to detect if the 10 kHz D/A output is greater than or less than the sensor interface signal. Referring to figure 3.1.7, assume initially that  $E_s$  and  $E_d$  are exactly in phase and that  $E_q = 0$ . The input  $E_e$  to the comparator is the difference between  $E_s$  and  $E_d$  and will be in phase or  $180^\circ$  out of phase depending on whether  $E_s$  is greater or smaller than  $E_d$ .  $E_e$  is amplified by  $T_1$  and  $A_1$ , and detected by  $D_1$ . The resulting dc signal is further amplified in  $A_2$  and then applied to the input of a "finite time" integrator consisting of  $A_3$ ,  $R_1$ ,  $C_1$  and reset switch  $S_R$ .  $S_R$  is momentarily closed, re-zeroing the integrator at the beginning of each clock pulse to the logic module. The dc error signal including random noise at the output of  $A_2$  is then integrated for the remainder of the clock period and the resulting output is then interpreted by the logic as either "high" or "low". The "finite time" integrator is thus used as an optimum filter having no "memory" of the error signal during the previous clock period so its response to a very small error signal is not impaired by having been subjected to a large error signal during the previous clock period.

Initially we assumed  $E_q$  was zero and that  $E_s$  was exactly in phase with  $E_d$ . In reality, there is usually a small phase difference between  $E_s$  and  $E_d$  due to a small quadrature component in the sensor signal  $E_s$ . The in-phase detector  $D_1$  theoretically should not be sensitive to a small quadrature component. However, if the quadrature component is large enough  $D_1$  can saturate causing non-linear operation and error.

Any quadrature component is detected by the "quadrature" detector

Fig. 3.1.7





$D_2$  which is identical to  $D_1$  except that its reference.  $E_{qr}$  is phase shifted  $90^\circ$ . The output of  $D_2$  is filtered in a second integrator consisting of  $R_2$ ,  $C_2$  and  $A_4$ . The filtered output is then applied to one input of a multiplier  $M_1$ ; a second input to  $M_1$  is a 10 kHz sine wave shifted  $90^\circ$  from the sensor input  $E_q$ . This means that the resulting output from  $M_1$  is at  $90^\circ$  or  $270^\circ$  depending on the polarity of  $E_a$ . The closed loop consisting of  $T_1$ ,  $A_1$ ,  $D_2$ ,  $A_4$ ,  $M_1$  and  $T_2$  automatically balances the quadrature component of  $E_e$  by making  $E_q$  exactly equal and opposite to it.

Compare fig. 3.1.7 with the detailed schematic fig. 5.1.7

$A_1$  is op amp IC1/1 and associated components

$D_1$  is op amp IC1/13 and associated components (see appendix 7.5)

$A_2$  is op amp IC2/1 and associated components

$A_3$ ,  $R_1$ ,  $C_1$  - finite time integrator - is op amp IC3, R19, C7  
and other associated components.

$D_2$  is op amp IC2/13 and associated components.

$A_4$ ,  $R_2$ ,  $C_2$  - finite time integrator - by op amp IC4, R32, C10 and  
other associated components

$M_1$ , - multiplier - is IC5 and associated components

$S_R$  - Comparator reset switch is implemented with IC6/10.

Examples of typical wave forms for the comparator test points are included in Section 2.4.

## DIGITAL TO ANALOG CONVERTER

The digital to analog converter is a digitally controlled ratio transformer. The precision of the input to output ratio is better than 1 part in  $10^5$ , an accuracy which is unattainable using conventional current summing converters. These devices are subject to uncertainties caused by finite switch resistance and imprecise resistors having significant temperature coefficients and long term drift.

The theory and practice of precision ratio transformers is widely documented and will not be discussed here except to note that the use of very high permeability cores (e.g., Supermalloy), proper selection of operating frequency, winding geometry, and shielding etc., result in transformers having output voltage ratios precisely proportional to the turns ratios. In special cases the precision can be as high as 1 part in  $10^8$ .

Each of the three transformers  $T_A$ ,  $T_B$  and  $T_C$  have a 16, 8, 4, 2 and 1 turn windings, i.e., five binary stages.  $T_C$  has an additional 1 turn winding with a resistive divider to provide the 16th binary stage (LSB). A 5-turn winding on  $T_A$  drives a 160-turn winding on  $T_B$  giving a 32 to 1 reduction from  $T_A$  to  $T_B$ . Similarly, a 160-turn winding on  $T_C$  is driven from a 5-turn winding on  $T_B$ .

Each switch  $S_1$  through  $S_{16}$  is single pole-double throw and is implemented by a pair of FET's. One switch of each pair is turned "ON" or "OFF" directly by one line ( $Q_1$  through  $Q_{16}$ ) from the logic module while the other is turned "OFF" or "ON" by inverting the logic output.

Experience with this type of AC D/A Converter has consistently shown very nearly ideal performance with total errors less than 1 least significant bit and no detectable drift.

The digital to Analog Converter plays a critical role in the accuracy of the digitizer section of the CTD, shown in simplified diagram Figure 3.1.7.

## DIGITIZER LOGIC

The digitizer logic circuit uses Motorola successive approximation registers and is in a loop including a D/A converter and a comparator to generate from a given input signal a binary number which precisely represents the input signal.

Digitization is initiated by a "START" command to the logic module causing  $S_0$  to be set "high" and  $S_1$  through  $S_{16}$  to be set "low". The A/C comparator compares the analog output from the D/A converter  $E_d$  with the sensor output voltage  $E_s$ . If  $E_s$  is smaller than  $E_d$ , with  $S_1$  through  $S_{16}$  low,  $E_d$  equals zero and the comparator output  $E_c$  goes "low". At the next clock pulse  $S_0$  is set "low", indicating a negative sign and reversing polarity of  $E_s$ ;  $S_1$  is set "high". If  $E_s$  is larger than  $E_d$ ,  $E_c$  goes "high" and then at the clock pulse  $S_0$  remains "high" and  $S_1$  is set "high". This sequence is repeated until switches  $S_0$  through  $S_{16}$  have been set by logic outputs  $Q_0$  through  $Q_{16}$ . At this point the analog output of the D/A converter  $E_d$  is equal to the sensor output  $E_s$ . The binary output is represented by the settings of  $Q_0$  through  $Q_{16}$ .

The Motorola successive approximation registers (S.A.R.) are IC1 and IC3 and the timing diagram for them is shown in fig. 3.1.9.

- 1) A "master reset" (M.R.) pulse will cause all outputs to go low.
- 2) A "start convert" (S.C.) pulse will arm the device so that the succeeding clock pulse will start the successive approximation.
- 3) The first clock pulse sets  $Q_0$  high and  $Q_1$  thru  $Q_{16}$  low.

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WOODS HOLE OCEANOGRAPHIC INSTITUTION MASS

F/G 8/10

W.H.O.I./BROWN CONDUCTIVITY, TEMPERATURE, AND DEPTH MICROPROFIL--ETC(U)

FEB 78 N L BROWN, & K MORRISON

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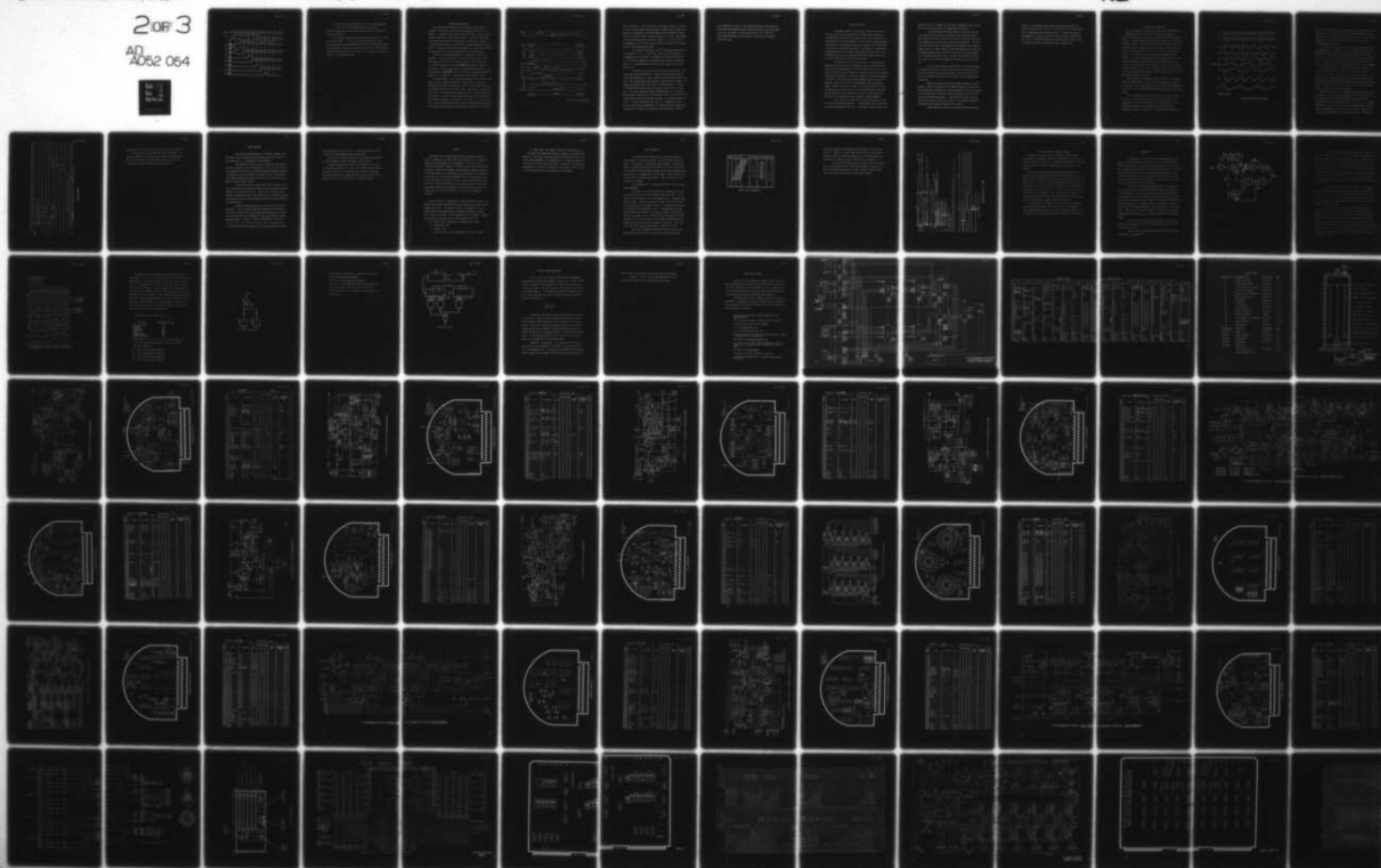
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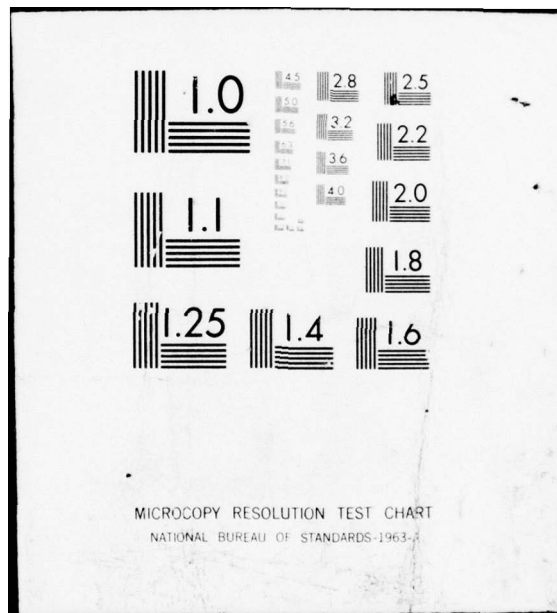
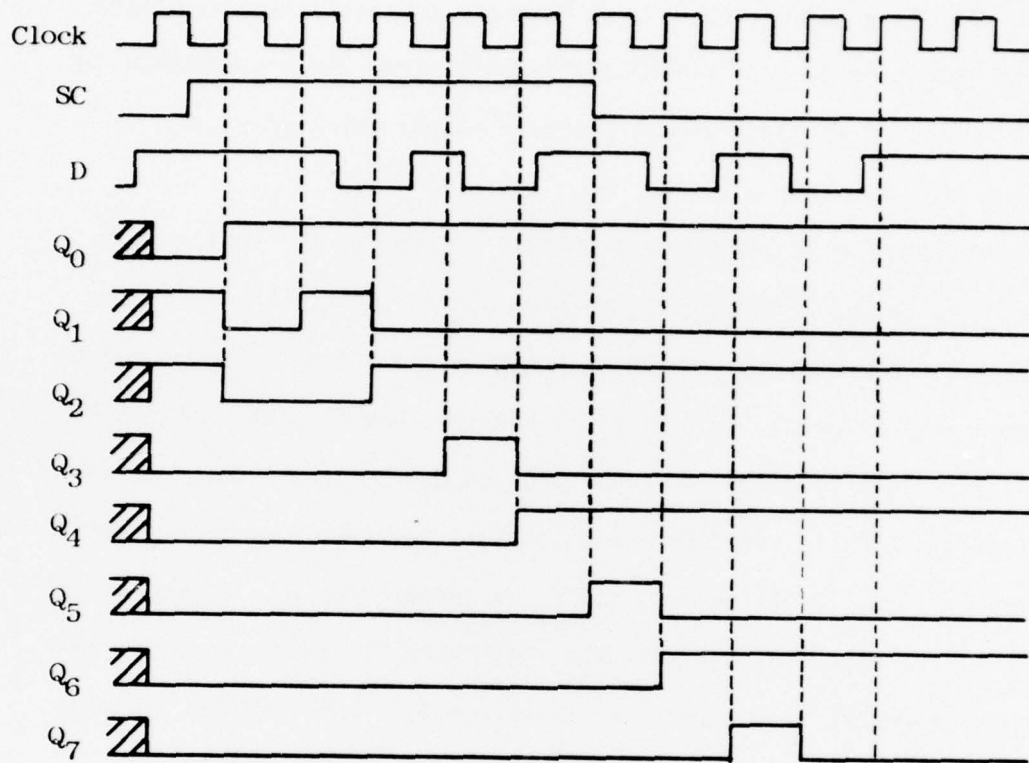


Fig. 3.1.9



- 4) The next clock pulse leaves  $Q_0$  high or not, depending upon state of D; and unconditionally sets  $Q_1$  high, etc.

In the digitizer logic circuit two of these devices are cascaded for 16 bit digitization.

An extra stage to the S.A.R. which determines the sign bit is made up of IC5 and IC6/13. Flip-flop, IC6/2 generates the  $Q_{16}$  waveform which tells the memory and multiplexer to select the next analog channel for digitization. Registers IC2 and IC4 are part of the long telemetry register; following the third digitization in any frame, the conductivity value will be strobed into them.

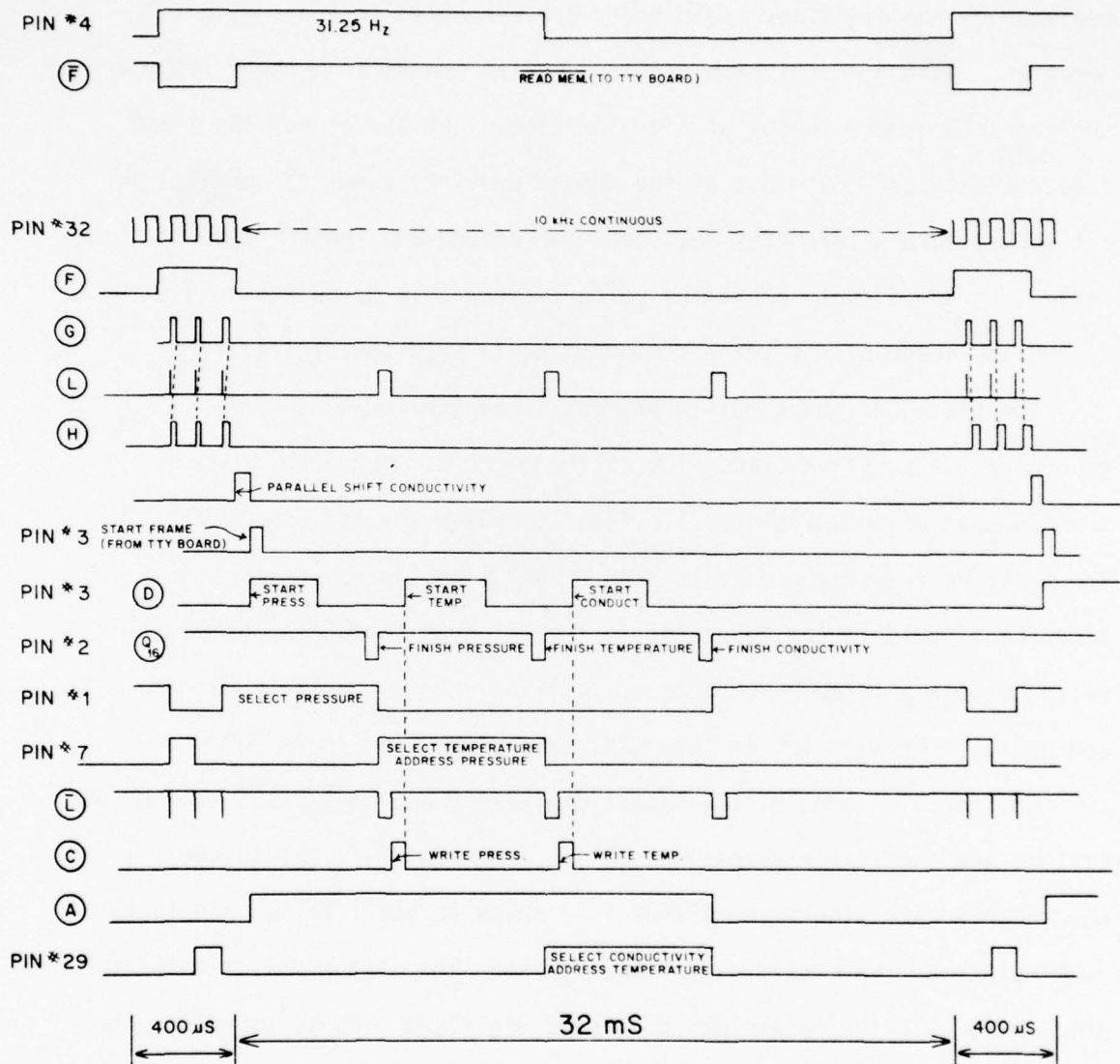
## MEMORY AND MULTIPLEXER

The sixteen parallel outputs of the successive approximation register on the digitizer logic board are connected to two 4 by 8 bit memories. At the end of each sampling period the data on these lines are shifted into memory in one of four locations. At the end of the frame time the data are moved out of the memory and into a set of parallel input serial output telemetry registers for coding and transmission up the cable. In addition to providing buffer memory this circuit also controls the multiplexing of the three analog channels into the digitizer.

The timing of the sampling process is controlled by the signal generator. A positive transition of the 31.25 Hz square wave causes the  $\bar{Q}$  output of the 'finish' flip flop to pulse low for about 300  $\mu$ s. The positive transition of this READ MEMORY line causes a 'start digitize frame' pulse to be generated in the Teletype formatting board. The delay between a 'READ MEMORY' positive transition is variable between 200 and 400  $\mu$ s; the duration of 'start digitize frame' pulse is 200  $\mu$ s.

The positive edge of the 'start digitize frame' pulse sets the reset, status, and the filter flip-flops (FF). The reset F.F. resets the word counter and clocks the status F.F. which is still being held in the 'set' state by the 'start dig. frame' pulse. The status F.F. remains set until after all the parameters have been digitized. On being reset, the word counter '0' output or pressure analog gate line goes high connecting the pressure interface to the digitizer. The filter F. F. goes high causing a 'start digitize word' pulse to be sent to the digitizer logic board. At the end of the digitization period the  $Q_{16}$  line goes low for one digi-

Fig. 3.1.10



MEMORY & MULTIPLEXER TIMING

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tizer clock period. The positive edge of this pulse causes a  $3\ \mu\text{s}$  pulse on line L, which advances the word counter to operate the next gate, temperature, simultaneously telling the memory that the digitized pressure data on its parallel input is to be called word 1. As the L line reverts to the low state the positive edge of  $\bar{L}$  causes a  $3\ \mu\text{s}$  'write' pulse to be generated on line C and the ensuing positive transition of  $\bar{C}$  generates the next 'start digitize word' pulse.

This process repeats until the  $n^{\text{th}}$  word has been digitized ( $n$  is selectable 2, 3, or 4). The  $n^{\text{th}} Q_{16}$  causes L to pulse high for  $3\ \mu\text{s}$  incrementing the 'word counter' to address the  $n^{\text{th}}$  word, operating the  $(n + 1)^{\text{th}}$  gate and immediately resetting the word counter and setting status F.F. low preventing any further writing to memory by disabling the write F.F.

On the arrival of the next 31.25 Hz positive transition, line F goes high enabling the Read F.F. Positive transitions of the 10 kHz clock signal generate  $10\ \mu\text{s}$  pulses on the G line which appear directly on the L line incrementing the word counter to address memory locations. To address the pressure word, the rise of  $\bar{L}$  clocks the write F.F. but the C line does not get pulsed since the D input of the write F.F. is now low.  $10\ \mu\text{s}$  after G goes high  $\bar{G}$  goes high generating a  $2\ \mu\text{s}$  pulse on H which parallel shifts data from the addressed memory location into the addressed parallel-in serial-out shift registers. This process repeats until  $(n - 1)$  words have been shifted into  $(n - 1)$  telemetry registers. The final word, always conductivity, will remain on the D/A output until  $\bar{F}$  goes high at the end of the frame time, thus generating a 'parallel

shift conductivity' signal in the Teletype formatting circuit which parallel-shifts the conductivity data from the D/A input to the shift register on the logic board. The logic board sends a start frame back to the memory multiplexer board and both digitization and telemetry cycles start over.

## ADAPTIVE SAMPLING

The adaptive sampling circuit varies the clock rate to the digitizer logic and the reset time of the 'finite time' integrator in the comparator in such a way as to obtain a minimum digitization time consistent with error free operation. The reset time is 600 microseconds if the previous error signal was equal to or greater than the sixth most significant bit, and 200 microseconds if it was smaller. The 600 microseconds period allows an automatic quadrature balancing circuit in the AC Comparator more time to recover from saturation effects which occur when large signals exist at the comparator input.

The adaptive sampling circuit contains a threshold detector which goes 'high' as soon as the comparator output, a finite time integrator, falls to approximately +2.5 volts or rises to +9.5 volts. This causes a D type flip-flop to generate a digitizer clock pulse at the next 10 kHz master clock pulse. Large error signals will cause the comparator to arrive at a decision rapidly and the adaptive sampling circuit will generate a clock within 100  $\mu$ s of the comparator reset line being released. However, if the error signal is sufficiently small or zero and the comparator has not arrived at a decision after one millisecond the adaptive sampling circuit generates a clock pulse without waiting for the finite time integrator to reach the upper or lower threshold.

This circuit also contains the Pressure and Temperature sign bit latches and telemetry register, strobe signals used to latch these two signs are generated on this card. They appear on pins 29 and 31 and

they are useful for triggering an oscilloscope immediately after the completion of either the Pressure or Temperature digitizations.

At the beginning of the digitization of a new word the adaptive sampling circuit receives an A/S reset signal from the digitizer logic, which sets IC2/13 and arms IC5/13 causing a digitizer clock pulse to be generated at the next 10 kHz clock positive transition. The digitizer clock causes IC2/1 to be clocked and the comparator to be unconditionally reset. For every digitizer clock pulse except the one initiated by adaptive sampling reset, IC2/1 will latch the signal from comparator T.P.1 during the previous bit time. For small error signals during the last step, IC2/1 Q will be set high but for large errors it will be set low.

As this first clock pulse resets IC2/1 it will disable IC8/11 so that the reset time for the first bit time will be forced to 600  $\mu$ s. For the first step then we have to wait 600  $\mu$ s for IC9 to count up to 5 since it was held in reset for the first 100  $\mu$ s during the digitizer clock pulse.

When the digitizer reset has been removed counter IC1 starts counting. Either IC1 counting to 9 or threshold detector (Q4, Q12, Q3 and Q4) detecting a threshold will cause the arming of IC3/13 so the next positive transition of the 10 kHz clock will generate a clock pulse and the following transition remove it. The digitizing time for each bit then may be as short as 300  $\mu$ s or as long as 1.6 ms depending upon the magnitudes of the present and previous error signals.

Normal operation of this circuit may be ascertained by exam-

ination of the comparator output signal (see waveforms section 2.4) - reset times should always be 600  $\mu$ s for the first step in a digitization but will subsequently be either 200 or 600  $\mu$ s. The time required for the comparator to arrive at a decision after the reset is removed will vary in 100  $\mu$ s increments between 100  $\mu$ s when the error signal is large to 1ms when the error is less than one least significant bit.



## TTY FORMATTER &amp; FSK MODULATOR

This card provides the telemetry circuitry for the underwater unit.

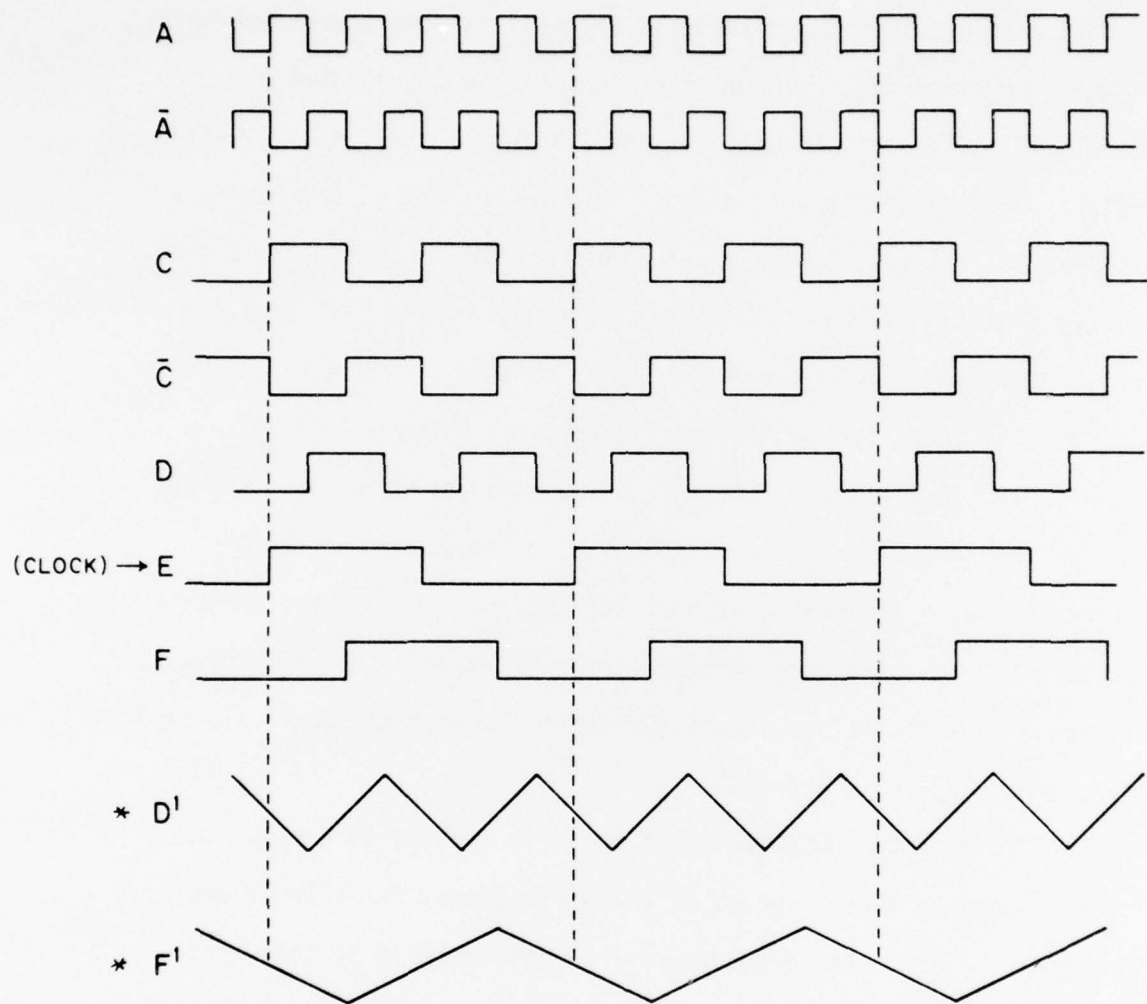
When the "read mem." signal goes high this card generates a parallel shift signal that completes the loading of the long telemetry register. Other sections are loaded under the control of the Memory and Multiplexer circuit. Internally this parallel shift signal starts the telemetry process; a zero "start" bit is output by the TTY formatter which is then followed by the first 8 bits of data in the telemetry register. The frame sync word always alternates between 00001111 (decimal, 015) and 1111 0000 (decimal, 240) on adjacent scans. The TTY formatter then outputs two "one" stop bits followed another "zero" start bit and then the next 8 bits of data etc. until a preset number of eight-bit bytes have been sent as eleven-bit words. The TTY formatter will then send a continuous stream of "ones" (logic high) until the next data telemetry cycle is started.

The TTY formatted data generated above is applied to a modulator which will cause either 2 cycles of a high frequency for a logic one or one cycle of half that frequency for a logic zero to be telemetred up the cable. In a standard system these two frequencies are 5 kHz and 10 kHz.

IC's 1 and 6 produce a 40 kHz clock which is further divided by ICs 2 and 3 to produce two 5 kHz square waves phase-shifted by 90° designated F and in-phase data clock K. A third output is a 10 kHz square wave designated 2F, phased such that zero crossings of F correspond with zero crossings of 2F. The data clock is gated, with



Fig. 3.1.12



\* NOT TO SCALE

FSK MODULATOR TIMING DIAGRAM

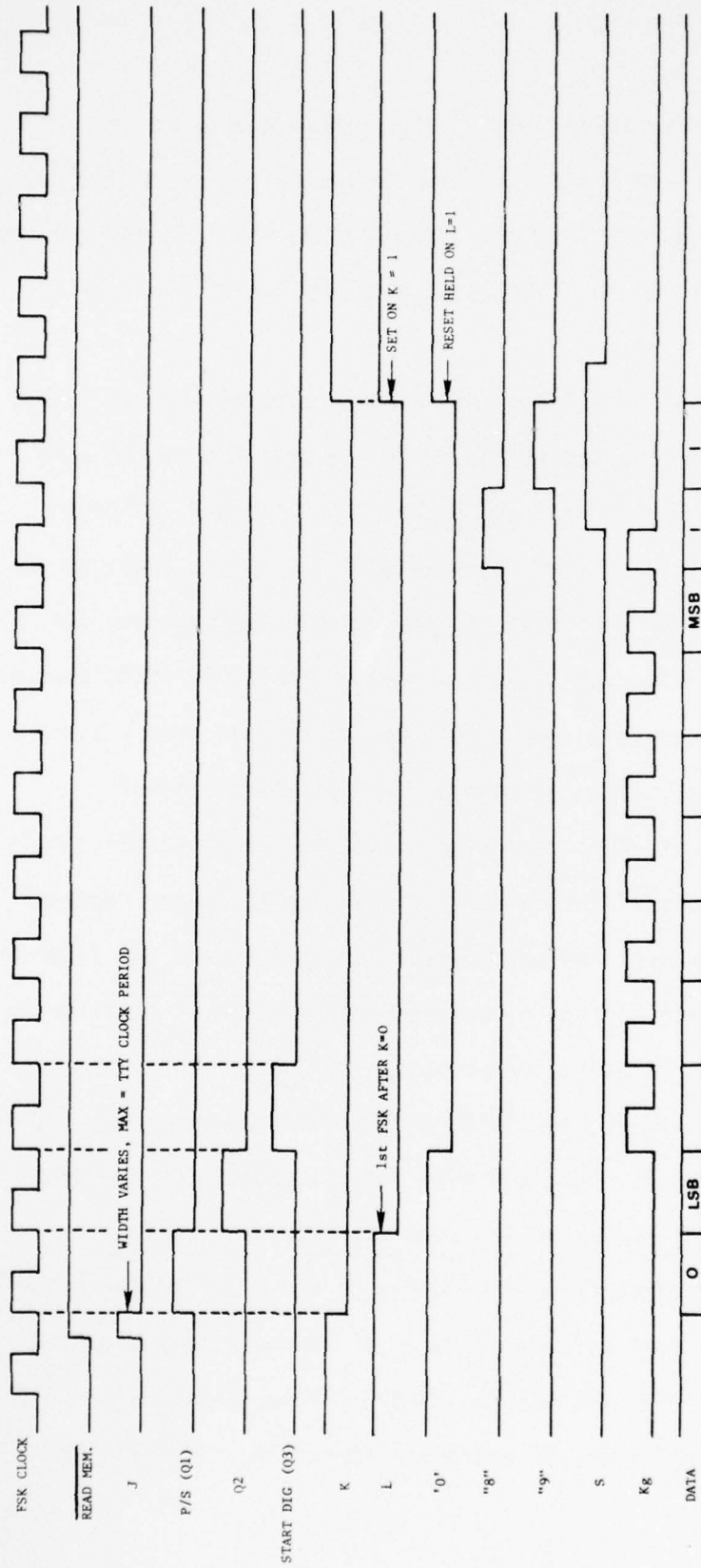
ICs 7, 10, 12 and 13; for every 8 data shifts there are three gaps in this clock stream as it is applied to the long telemetry register. During these gaps in the gated clock stream, ICs 6, 7, 10, 12 & 13 utilize the ungated clock, K to blend the "one" stop bits and "zero" start bit into the output data stream.

IC9/1 toggles on "parallel shift" signals alternating the frame synchronization word applied to the shift register IC8 at the head of the long telemetry shift register between 00001111 and 11110000. ICs 5, 11, 12, 13 & 14, with their associated DIP switch, count up the number of bytes in a scan and when the preset value selected by the switch is reached, cause a continuous stream of "ones" to be telemetered.

The telemetry process is controlled by the signals from ICs 9 & 5. When the digitization process is complete a "read mem." signal is sent to this circuit which generates a parallel shift signal. This controls the data transfer into a part of the long telemetry register not serviced by the memory and multiplexer card and starts the telemetry circuit. Finally, this control circuit generates a "start digitizer" signal to restart the digitization process.

Square waves, F and 2F, are integrated using components R2, R3, R4, R5 and C2, C3, C4 and C5. Data and  $\overline{\text{data}}$  control switch IC4 and cause the appropriate one of these two frequencies to be applied to a differential shaping circuit comprising Q1, R6 and R7. The logarithmic transfer function of this circuit produces an approximately sinusoidal output and components Q2, C6, C7, R8, R7 & R10 form an amplifier to drive the output transformer, T1 and hence the cable. Typically the

Fig. 3.1.12(2)



TTY/FSK TIMING

signal level at this point is 2v p-p (see wave form at Section 2.4).

A dc current is applied through the primary winding of T1 to generate a magnetic field opposing that caused by the 100mA supply current from the deck unit through the secondary to prevent the transformer from being saturated by the supply current.

## SIGNAL GENERATOR

The signal generator produces a 10 kilohertz reference sine wave and a second sine wave phase shifted by precisely  $90^{\circ}$  relative to the reference (i.e., in quadrature to the reference).

The reference sine wave is used to excite the analog sensors while the quadrature signal is multiplied in a servo controlled loop in the comparator and used to null the small quadrature component caused by the reactance of the leads between the sensors and their interface circuits (thus presenting the digitizer circuit with a signal precisely in phase with the reference signal.)

Square waves used in the generation of the sine waves and having a precise phase relationship to them are used to operate synchronous detectors in the comparator circuit. They are also divided in binary counters to generate the frame clock which controls the operating rate of the digitizer circuitry and the frequency shift key clock which controls the telemetry rate.

The 640 kHz crystal with Q1, R1, R2, R3, C1 and C2 forms an oscillator. IC3 is a binary divider which generates an 80 kHz source for the FSK clock and a 40 kHz clock input which enables the two stages of D type flip-flop, IC4, to generate 10 kHz outputs  $90^{\circ}$  out of phase with one another. If the pin 1 output is designated  $180^{\circ}$  then pin 2 is at  $0^{\circ}$ , pin 13 is at  $+90$  and pin 12 is at  $-90^{\circ}$ . R6, R7, R8, R9 and Q3 form a buffer amplifier between IC4 and the series/parallel resonant



filter comprising C3, C4, C5, C6, T1, L1 and R10 producing a 10 kHz sinusoidal wave form between output pins 23 and 24.

C7 couples the in phase sine wave into the operational amplifiers in IC5 to produce the  $\pm 90^\circ$  sine waves on pins 29 and 30.

IC1 divides the 40 kHz clock by 10 to produce the 4 kHz clock for the oxygen interface, this 4 kHz clock is then further divided by the binary counter IC2 to produce the 250 Hz clock for the oxygen interface and the 31.25 Hz frame clock. Q4 inverts the frame clock in order to satisfy timing constraints in the oxygen interface.

## DISPLAY

The display card provides engineering unit displays of pressure in decibars, temperature in degrees Celsius and conductivity in millimhos as measured by the underwater unit and updated 31.25 times per second. A fourth display labelled "frame sync" displays a number that is established to provide a check on the telemetry link and enable a computer connected by the serial data link to synchronize on the beginning of each data frame. This "frame sync" word alternates between 240 and 015 on adjacent frames so that the display will appear as a blur. When the display sample hold switch is put into the hold position the displays freeze, but the analog and computer outputs are not affected. When the displays are frozen the "frame sync" will read either 240 or 015 if the CTD is functioning correctly.

Each BCD character is displayed by a Hewlett Packard dot matrix light emitting diode element (HP-5082-7302) these elements have internal latches decoders and drivers. The parallel BCD data is presented to all of the columns having the same BCD weight (ten thousand, thousands, hundreds, tens, or units) in parallel and the appropriate row or variable is strobed with a pulse at the correct time for that variable every 32 ms.

This "correct time" is determined by "ANDING" four inputs.

- 1) Hundreds bit time
- 2) Tens bit time
- 3) Units bit time - all from demodulator "Bit time" counter.

4) Enable time - from number converter to scale the display.

For example the temperature display is strobed at bit time 054 and enable E15, one latter causing the display to be one half of the 16 bit binary number generated in the underwater unit. Variables displayed on the right side of the display board have a sign option. The signs are incorporated by latching the contents of the sign byte into ICs 15 and/or 18 and outputting them to the appropriate sign displays.

## NUMBER CONVERTER

The second card in the deck unit is the number converter, which converts a 16 bit binary number into 20 bit binary coded decimal (BCD). This technique is described by Couleur (1958). As the binary number is shifted Most Significant Bit (MSB) first into a 21 bit register the value of each BCD stage is tested and the value of any BCD stage greater than 4 is increased by 3; the new number is then serially shifted one place left and each stage retested. After 16 such shifts the conversion is complete.

As an example Fig. 3.2.2 shows conversion of the 8 bit binary number 1000,0000.

The clock for the conversion process is generated on the number converter board using a two inverter RC oscillator IC30. A '4017' counter counts 20 pulses of this clock gated with  $\bar{L}$  or S depending upon the data source. During the positive half cycle of the bit time clock K the data source for the number converter is the parallel in serial out shift register on the demodulator card. If the computer has strobed data into the shift registers on the number converter card during the previous cycle time, a flag S' will have been set and during the negative half cycle of the bit time clock the number converter data source becomes the parallel-in serial-out registers IC1 and IC8. Data steering is done with IC28 and the bit clock K. (See fig. 3.2.2(2) )

The clock is counted with IC16 and the first half of IC29. Enable pulses used for scaling in powers of 2,  $E_6$  thru  $E_9$  and  $E_{14}$

Fig. 3.2.2

H	T	U		TEST	ACTION	BCD
			10000000			0
		1	0000000	<5	SHIFT	1
		10	000000		SHIFT	2
		100	00000	<5	SHIFT	4
		1000	0000	U>5	ADD 3	8
		1011	0000		SHIFT	
	1	0110	000	U>5	ADD 3	16
	1	1001	000		SHIFT	
	11	0010	00	<5	SHIFT	32
	110	0100	0	T>5	ADD 30	64
	1001	0100	0		SHIFT	
1	0010	1000				128

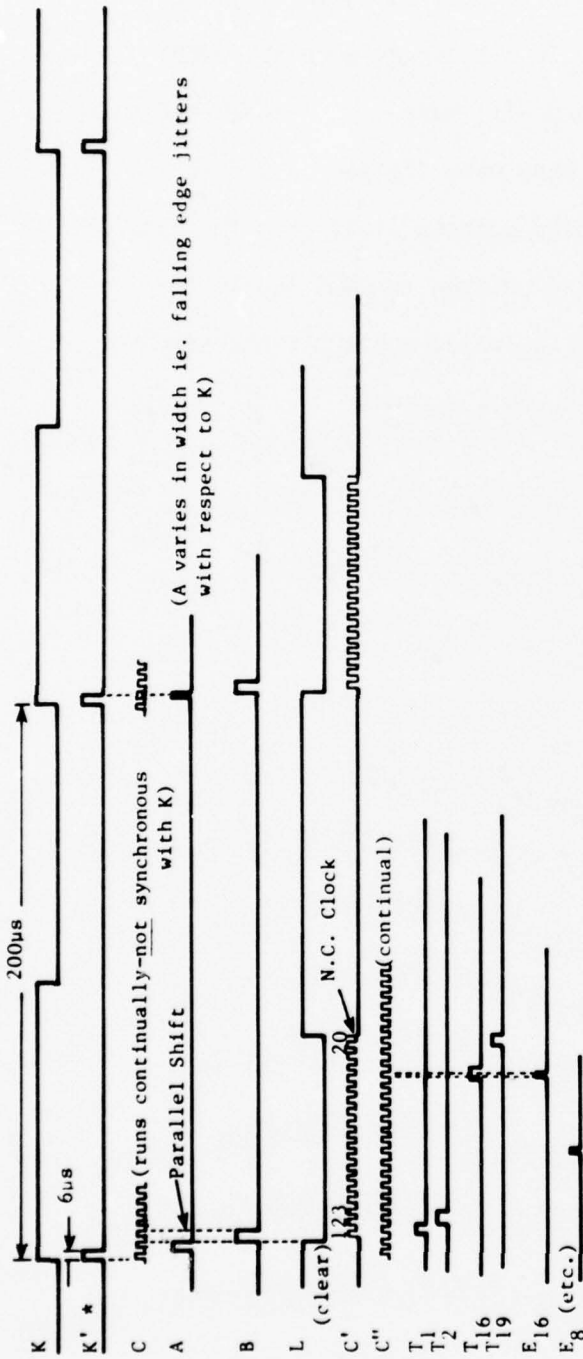
BINARY TO BCD CONVERSION



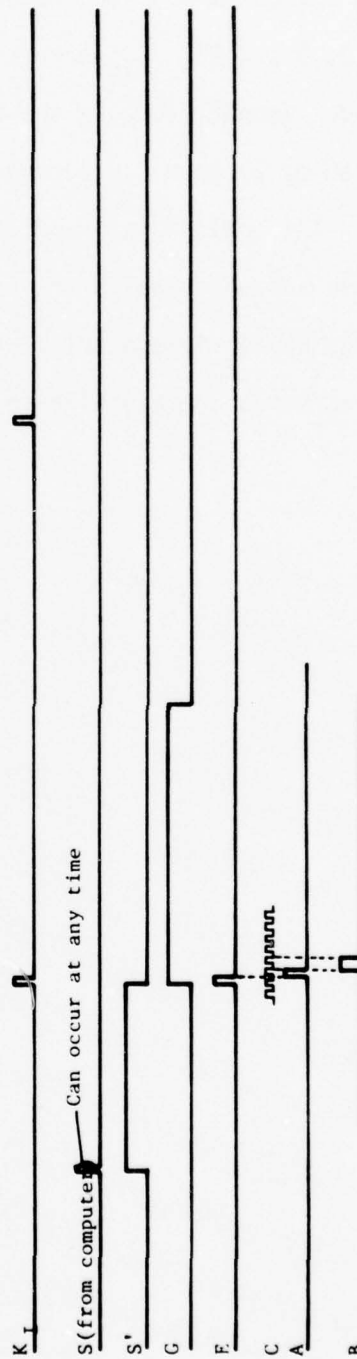
thru  $E_{17}$  are gated from the decoded counter outputs using the pulse  $C''$  and ICs 2, 9 and 23.  $E_{16}$  occurs when the 16 bit binary word has been converted. When  $E_{17}$  occurs the binary word will have been decoded and multiplied by 2, when  $E_{15}$  occurs it will have been divided by 2, etc.

This board also handles the sensor address lines from the computer; the address signals are inverted and shifted to CMOS levels to select the appropriate display or digital to analog converter channel. These levels must remain high for at least 200  $\mu$  seconds.

Fig. 3.2.2(2)



\*The sequence shown above can also be initiated by input signal E which can occur 1/2 clock time i.e. 100μs after K. E. occurs after a computer interrupt's S (see next part II)



NUMBER CONVERTER TIMING DIAGRAM

## DECK UNIT DIGITAL TO ANALOG CONVERTER

These circuits provide three 0 to 10 volts dc analog outputs proportional to temperature, pressure and conductivity, each capable of driving a channel of a recorder. For example temperature and conductivity can be plotted as a function of pressure with a 3 parameter, 2 axis recorder.

Of the four least significant BCD characters from the Number Converter three contiguous characters are selected by means of IC3, IC4 IC5 and IC9 in conjunction with the analog range select switches on the data terminal front panel. At the appropriate byte time and enable time selected by ICs 1 & 2 each variable is strobed into a different pair of hex latches, ICs 16 & 15, IC14 & 13, or IC12 & 11, if the analog Sample Hold switch is in the Sample position. The outputs of these pairs of latches are connected to digital to analog converter modules generating continuous analog outputs updated every 32 milliseconds.

As only three of five characters are converted, when a character overflows the analog output "pages" to zero volts. For example, if the temperature range switch is set at 10, a change from 9.99° to 10.00° in temperature will cause the output to go from 9.99 volts to zero volts.

## DEMODULATOR

The demodulator in the deck unit is a phase locked loop with four phase sensitive detectors two of which are in the loop with their outputs added linearly. When the loop is locked the VCO runs at 40 kHz and is subsequently divided down in binary dividers to 10 and 5 kHz to provide the reference frequencies for the two phase sensitive detectors. Thus either frequency at the input will cause the loop to phase lock with the VCO running at 40 kHz with no discontinuity in the loop operation as the input frequencies jump from one to the other.

The third and fourth phase sensitive detectors are supplied with reference signals at  $90^0$  to the reference signal as supplied to the first two detectors. These last two detectors then each synchronously detect one of the two input frequencies. When one frequency (say 5 kHz) is present the one detector output averages to a negative value while the other averages to zero. Conversely, when a 10 kHz signal is present one detector has zero average output while the other averages to a positive value. The sum of the two detector outputs is applied to the input of a limiting amplifier resulting in a logic level signal in serial TELETYPE format.

At this point the signal can be connected directly to a computer using a standard computer TELETYPE interface card modified to run at a bit rate of 5 kHz.

There is a brief discussion of phase locked loops and synchronous detectors in appendix 7.5.



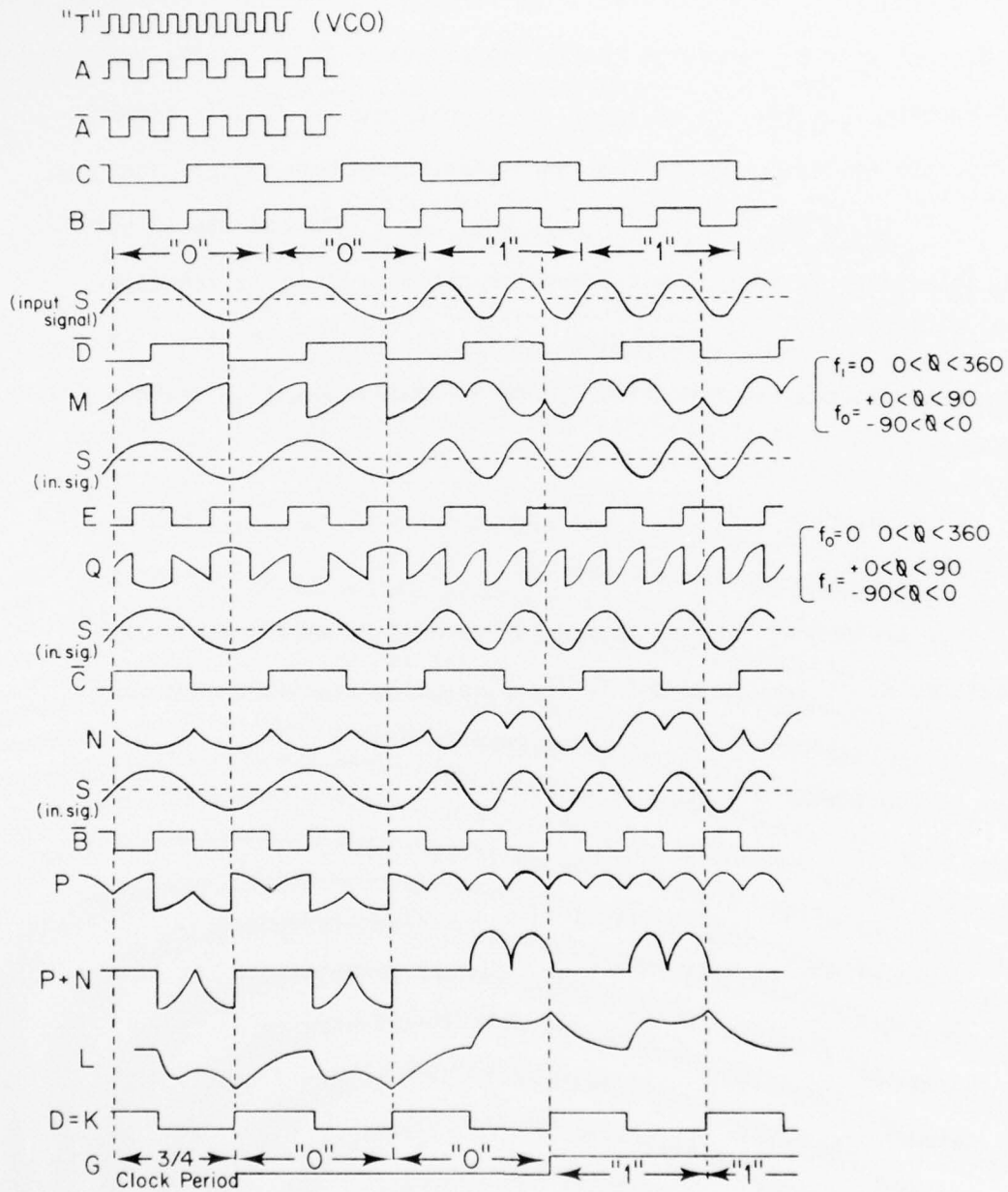


Refer to block diagram of the phase locked loop, Figure 3.2.4 and timing diagram, Figure 3.2.4(2). The first and second detectors are  $\emptyset_0$  and  $\emptyset_1$ , detector  $\emptyset_0$  generates correction signals and servos the V.C.O. while frequency  $f_0$  (5kHz) is on line; the output from  $\emptyset_1$  at this time will integrate to zero. Detector  $\emptyset_1$  generates correction signals and servos the V.C.O. while frequency  $f_1$  (10 kHz) is on line and the output from  $\emptyset_0$  integrates to zero. This generates the data transmission clock. Using this clock and phase derivatives of it, the input data stream (S) will be demodulated using the third and fourth phase-sensitive detectors,  $\emptyset_0'$  and  $\emptyset_1'$ .

Detectors  $\emptyset_0'$  and  $\emptyset_1'$ , see Figure 3.2.4(3), are switched by the derived waveforms  $\bar{C}$  and  $\bar{B}$  respectively, producing the waveforms, N and P, which are summed into an integrator to produce waveforms, L and G. Waveform, G, is then detected by positive-going transitions of waveform, D, to recreate the data stream delayed by 3/4 of a clock period as shown by the timing diagram.

The data now passes through an 11 bit window on the data stream, Figure 3.2.4(4). When all 11 bits are high (logical one) the 'ANDED' output of the 11 bits goes high. In TTY format the first of a group of 11 bits is the "start" bit and will always be a zero; therefore only during the no-data time between frames is a continuous stream of ones telemetered causing this frame synchronization signal to go high. The "frame sync" pulse is used to reset the bit time counter IC13, IC14 & IC15 which counts clock transitions, K after the first start bit has caused "frame sync" to go low.

Fig. 3.2.4(2)



The output of the bit time counter is used with the interrupt time gates, IC1, IC2, IC3, IC4, IC5 and IC6, to control the displays and Analog outputs as well as the parallel output to a computer. A gated clock, Kg, is generated from K using IC16, IC17 and IC23 in order to shift data into registers IC9 and IC10 without the start and stop bits. Every bit time the contents of IC9 and IC10 are parallel shifted into registers IC7 and IC8 the data is then clocked by the Number Converter, from IC7 and IC8, most significant bit first, into the Number Converter. The data is always telemetered in the same sequence, so the bit time when a particular variable is in the 16 bit window in the serial data stream is unique and can be calculated using:

$$\text{Interrupt Bit Time} = (\text{MS Byte \#} \times 11) - 1.$$

<u>Data Byte</u>	<u>Interrupted Bit Time</u>
FRAME SYNC WORD	010
PRESSURE	032
TEMPERATURE	054
CONDUCTIVITY	076
SIGNS	087
OXYGEN CURRENT	109
OXYGEN TEMPERATURE	120

Compare figures 3.2.4, 3.2.4(3), 3.2.4(4) and schematic 5.2.4

The amplifier having output signal S is A1/1, Q1, Q2 and associated components

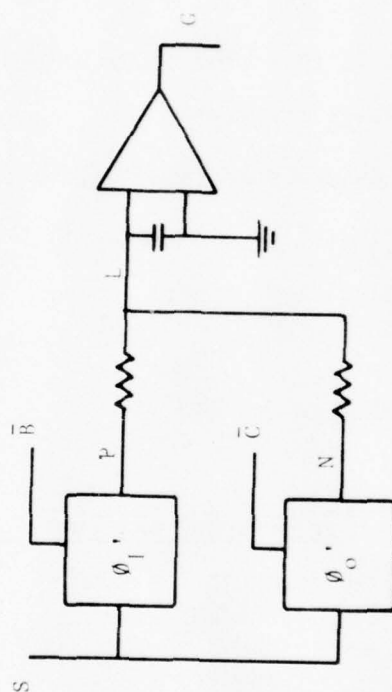
$\emptyset_0$  is A3/1 and associated components

$\emptyset_1$ , is A3/13 and associated components

$\emptyset_0$ , is A2/1 and associated components

$\emptyset_1$  is A2/13 and associated components

Fig. 3.2.4(3)



The integrator that generates L and finally G from P & N is A1/13 and associated components.

The filter is  $A_4$  and associated components

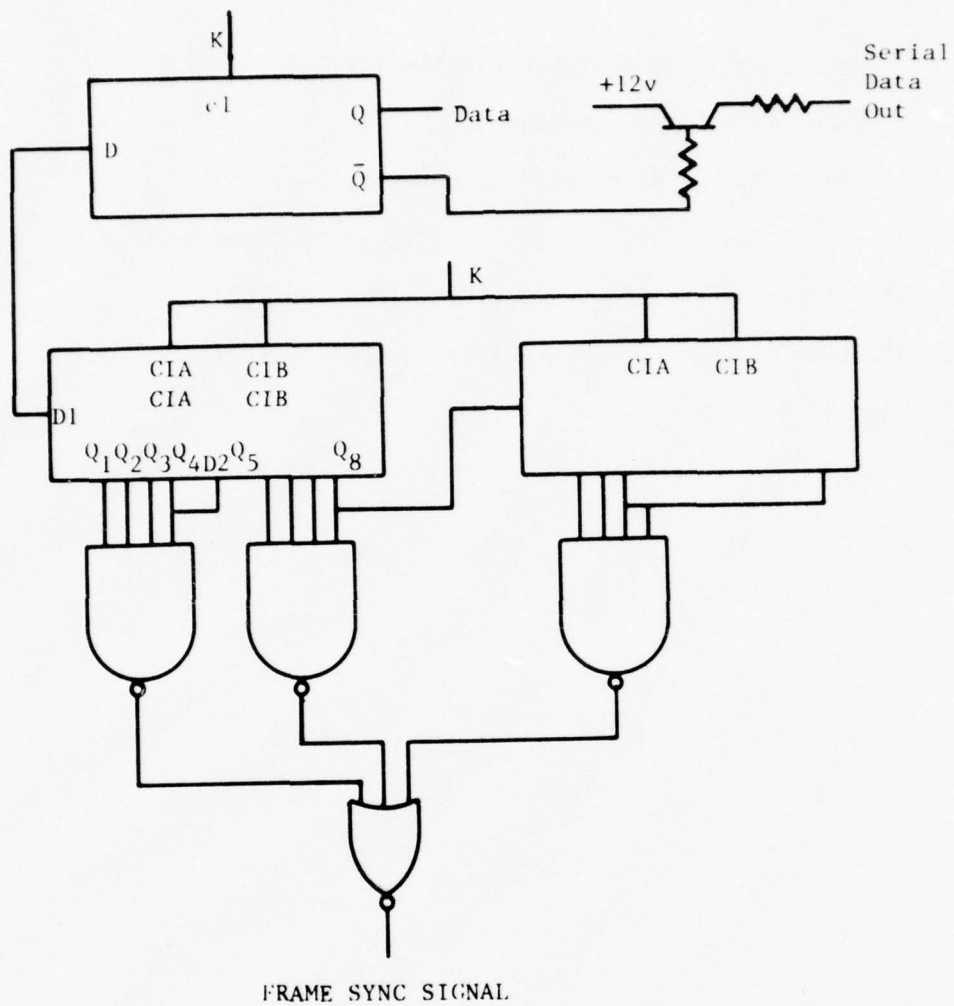
The V.C.O. is IC37 (NE566U) and its associated components

The 11 bit window is IC18, IC19, IC20, IC21 and IC23

The division of the V.C.O. frequency is done by IC27, IC28 IC29 and IC30.



Fig. 3.2.4(4)



### CONSTANT CURRENT POWER SUPPLY

Refer to the circuit diagram of the constant current power supply shown on the back panel schematic, Figure 5.2.6. Constant current dc power is supplied to the Underwater Unit from a circuit driven by a 50 volt power supply. The Zener current for CR1 and base current for Q1 is provided through R2. The voltage across R1 and P1 regulates to the Zener voltage minus the base emitter voltage of Q1 thus establishing a constant current equal to

$$\frac{V_{CR1} - 0.6}{R_1 + P_1}$$

A reversing switch enables polarity reversal when the system is to be used in conjunction with a Rosette multi-sampler that identifies a positive current down the cable as a signal to fire a sample bottle. For the CTD to operate in a reverse polarity mode a factory installed optional DC-DC converter is necessary, and the nominal 100 mA constant current must be increased to 160 mA. For use with long cables with a dc resistance greater than 125 ohms the 50 volt power supply needs to be replaced with a 100 volt power supply.

The choke, L1 and capacitor, C<sub>2</sub> are used to decouple the ac data signal from the underwater unit and the dc constant current supply to the underwater unit. The various audio transformers provide the correct impedance match between different data sources and destinations

and free users from grounding problems with audio tape recorders.

Thermistor, Th1 is in series with the 110V line to the chopper power supply to prevent power up current surges.

130  
FRONT AND BACK PANELS

The under side of the deck unit chassis is built with "wire wrap" interconnections to the four (optionally five) pairs of circuit card jacks and two 90 pin Elco connectors, J11 & J12. Connector, J12 is an interface between the wire wrap and soldered connection to the front and back panel controls, indicators and connectors.

Plus and minus 15 volts at 350mA and 5 volts at 6 amps are generated by a chopper power supply; a regulated 12 volts is generated on the demodulator card and all of these are buss lines on the under-side of the deck unit chassis.

S1 selects the data source; either Direct from J13 or Replay from J15.

S2 & S3 reverse the phase of the two inputs to switch S1.

S4 controls the 110 volt ac input Power.

S5 is the Display S/H switch.

S6 is the analog output S/H switch.

S7, S8 & S9 control the range of the analog outputs available on connector J17 on the back panel.

S10 controls the Pressure Display range.

S11 controls a phase shift network intended to correct for phase shifts in the signal due to transmission up the sea cable.

P1 controls the Signal Level.

P2 controls the center frequency of the V.C.O.

P3 controls the Audio level on the speaker mounted on the front panel.

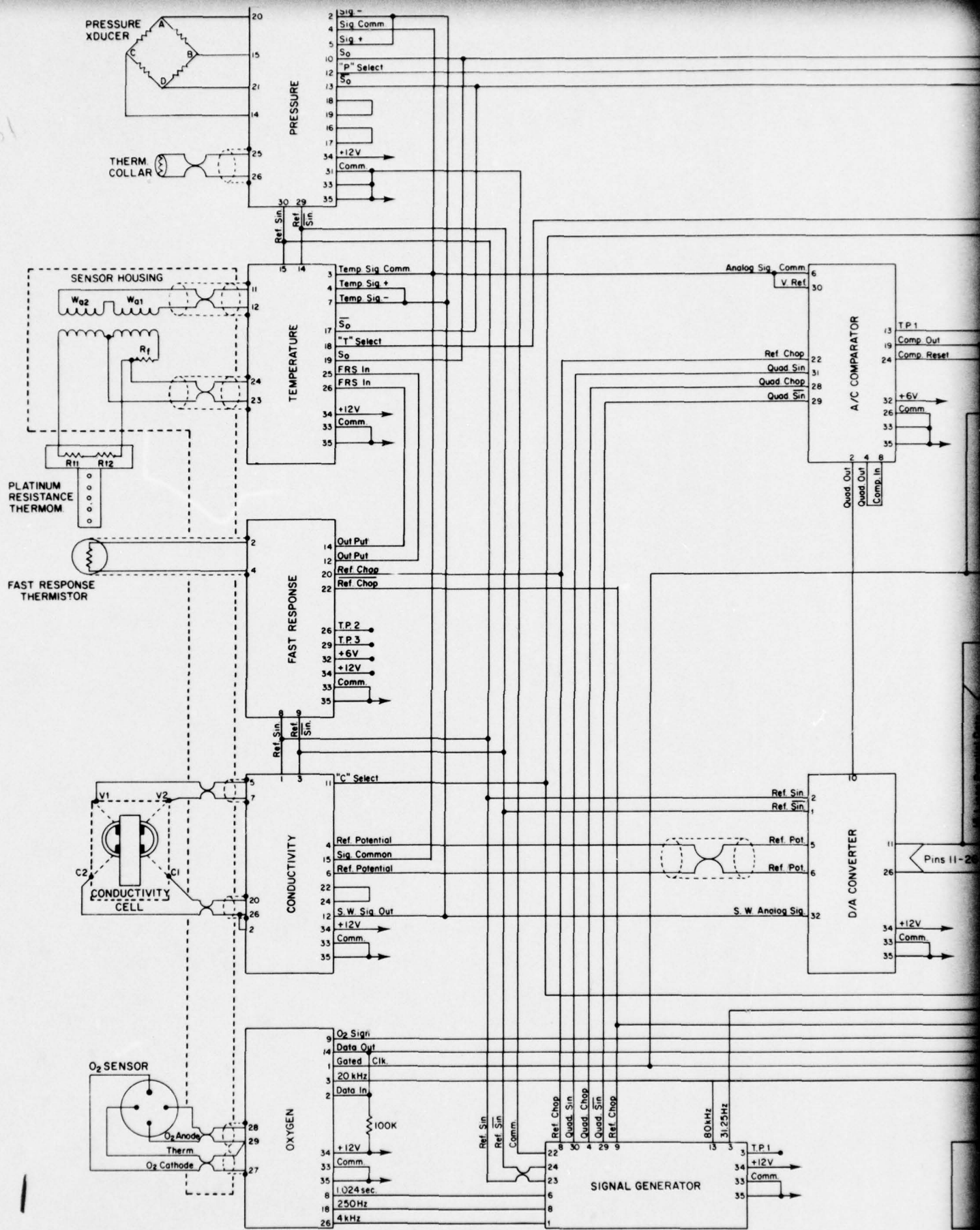
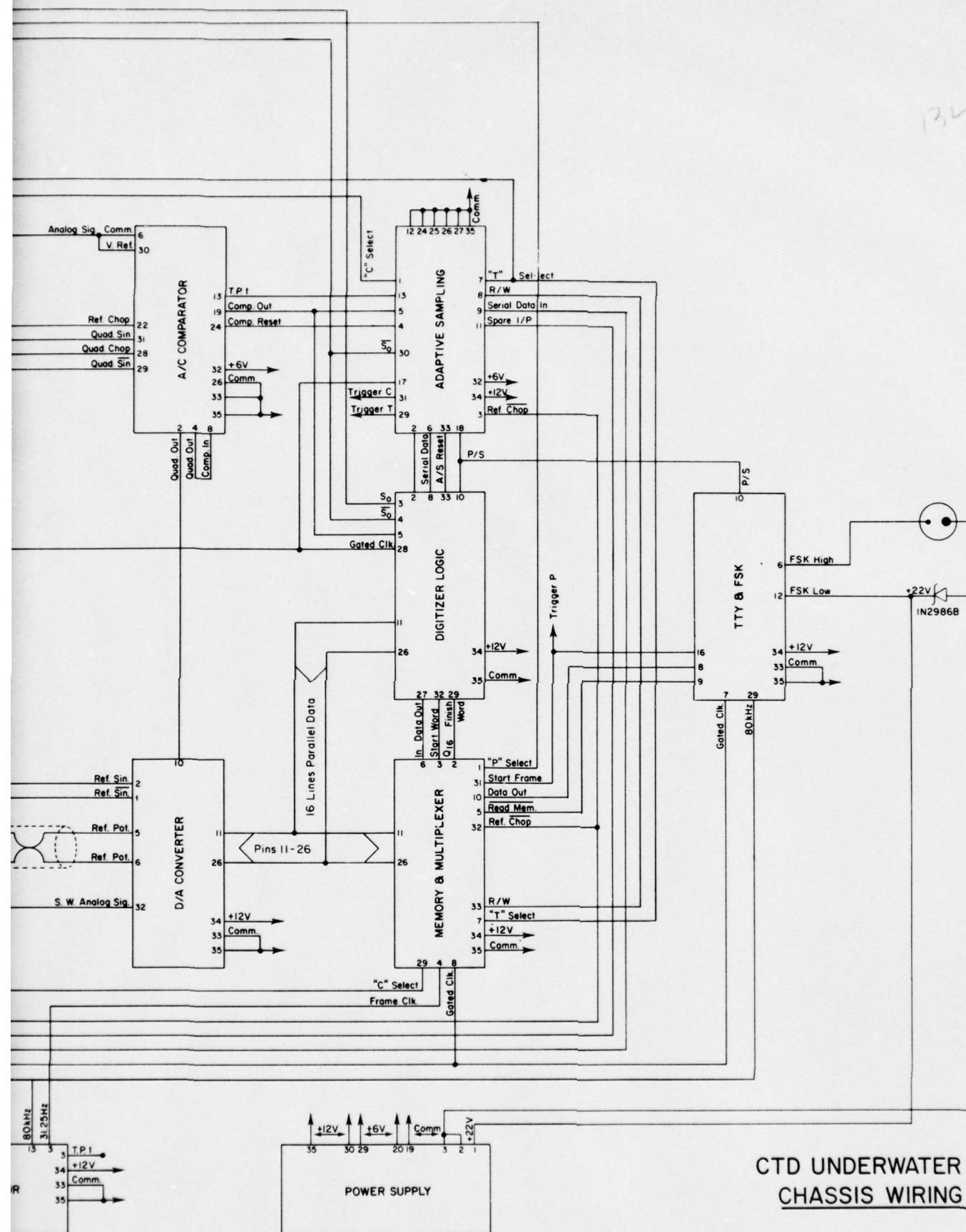




Fig. 4.1

CTD UNDERWATER UNIT MK III  
CHASSIS WIRING DIAGRAM

# UNDERWATER UNIT INTERWIRING

Each termination is given a four digit number; the first two digits designate the board number, the second two digits designate the connector pin number. F

Pin	J 01 PRESSURE	J 02 TEMPERATURE	J 03 FAST RESPONSE	J 04 CONDUCTIVITY	J 05 OXYGEN	J 06 POWER SUPPLY	J 07 A/C COMPARATOR	J 08 D/A CONVERTER	J 09 DIGITIZER
1				0214, 0802 1322, 0309, 0219	1008, 1207 0928, 1117	End Plate P.S.		0129, 0214 1324, 0509, 0403	
2	0412, 0832 0204, 0105, 0207		Sensor Hd #3	0426	0514, 1109	End Plate 0603	0830	0130, 0215 1323, 0308, 0401	1102
3		0706, 0104, 0730 0105, 0832		0214, 0801 1324, 0309, 0129	1313, 1229	0602			0219, 0
4	0706, 0730 0203, 0415	0412, 0102, 0207	Sensor Hd #2	0805			0708		0217, 1
5	0412, 0832 0102, 0204, 0207			Sensor Hd #22			0734	0404	0719, 1
6				0806			0730, 0415	0406	
7		0412, 0832 0204, 0102, 0105		Sensor Hd #21			0601		
8			0215 1323, 0401, 0130		1306		0704		1106
9			0129, 0214 1324, 0309, 0403		1111				
10	0219, 0903								1118, 0
11		Sensor Hd #14		1101, 1029 0102, 0105		0535		0911, 1011	1011, 0
12	1001	Sensor Hd #15	0215	0832, 0204, 0207		0735		0912, 1012	1012, 0
13	0217, 1130, 0904	0309, 0403 1324, 0129	0226		1109, 0502	0435	1113	0913, 1013	1013, 0
14	Bendix Conn. C	0308, 0401		0730		0835		0914, 1014	1014, 0
15	Bendix Conn. B	1323, 0130, 0215		0706, 0203, 0104		0335		0915, 1015	1015, 0
16	0117					0935		0916, 1016	1016, 0
17	0116	0904, 0113, 1130				0235		0917, 1017	1917, 0
18	0119	1107, 1007			1302	1335		0918, 1018	1018, 0
19	0118	0903, 0110				0135	0905, 1105	0919, 1019	1019, 0
20	Bendix Conn. A		1308, 0722	0402 Sensor Hd #17				0920, 1020	1020, 0
21	Bendix Conn. D							0921, 1021	1021, 0
22			1309, 1032, 1103	0424			1308, 0320	0922, 1022	1022, 0
23		Sensor Hd #4						0923, 1023	1023, 0
24		Sensor Hd #12		0422, 0402		0732	1104	0924, 1024	1024, 0
25		0312						0925, 1025	1025, 0
26		0314		Sensor Hd #18	1301	1132	0733, 0735	0926, 1026	1026, 0
27					Sensor Head #13				1006
28					Sensor Head #15		1304		1117 1008, 0503
29	0309, 0403 1324, 0214, 0801				Sensor Head #12	0332	1329		1002
30	0401, 0802 1323, 0215, 0308				Sensor Head #14	0734, 0834	0706, 0203, 0104	0702	
31	0133, 1322					0534, 0434	1330		
32			0626			0934	0627	0207, 0102, 0104 0412, 0204	1003
33	1322, 0131, 0135	0235	0335	0435	0535	0434, 0334	0726, 0735	0835	1133
34	0634	0633	0632	0631	0631	1334	0630, 0705	0631	0632, 11
35	0619, 0133	0617, 0233	0615, 0333	0613, 0433	0611, 0533	0234, 0134	0612, 0733	0614, 0833	0616, 11

Fig. 4.2

## UNDERWATER UNIT INTERWIRING

ate the board number, the second two digits designate the connector pin number. For example 0412 connects to pin 12 of circuit board 4.

J 05 OXYGEN	J 06 POWER SUPPLY	J 07 A/C COMPARATOR	J 08 D/A CONVERTER	J 09 DIGITIZER LOGIC	J 10 MEM. & MULT.	J 11 ADAPTIVE SAMPLING	J 12 TTY/FSK	J 13 SIGNAL GENERATOR
1008, 1207 0928, 1117	End Plate P.S.		0129, 0214 1324, 0509, 0403 0130, 0215		0112	1029, 0411		0526
0514, 1109	End Plate 0603	0830	1323, 0308, 0401	1102	0929	0902		0518
1313, 1229	0602			0219, 0110	0932	1032, 0322, 1309		1004
		0708		0217, 1130, 0113	1303	0724		0728
		0734	0404	0719, 1105	1209	0719, 0905		
		0730, 0415	0406		0927	0908	End Cap 1117, 1008, 0501, 0928	0508
1306		0601			1107, 0218 0928, 1207 0501, 1117	1007, 0218	1010	0722, 0320
1111		0704		1106		1033	1005	0322, 1103, 1032
				1118, 0210	1208	0514, 0502	0910, 1118	
	0535		0911, 1011	1011, 0811	0911	0509		
	0735		0912, 1012	1012, 0812	0912	1124	End Cap	
	0435	1113	0913, 1013	1013, 0813	0913	0713		1229
1109, 0502	0835		0914, 1014	1014, 0814	0914			
	0335		0915, 1015	1015, 0815	0915			
	0935		0916, 1016	1016, 0816	0916		1031	
	0235		0917, 1017	1917, 0817	0917	0501, 0928 1207, 1008		
1302	1335		0918, 1018	1018, 0818	0918	0910, 1210		
	0135	0905, 1105	0919, 1019	1019, 0819	0919			
			0920, 1020	1020, 0820	0920			
			0921, 1021	1021, 0821	0921			
		1308, 0320	0922, 1022	1022, 0822	0922			0133, 0131, 0135
			0923, 1023	1023, 0823	0923			0215, 0130, 0802 0401, 0108, 0801 0214, 0128, 0801 0403, 0309
	0732	1104	0924, 1024	1024, 0824	0924	1112, 1125		
			0925, 1025	1025, 0825	0925	1124, 1126		
1301	1132	0733, 0735	0926, 1026	1026, 0826	0926	1125, 1127		
Sensor Head #13				1006		1126, 1135		
Sensor Head #15		1304		1117 1008, 0501, 1207				
Sensor Head #12	0332	1329		1002	1101, 0411		1313, 0503	0729
Sensor Head #14	0734, 0834	0415 0706, 0203, 0104	0702			0904, 0113, 0217		0731
	0534, 0434	1330			1216			
	0934	0627	0207, 0102, 0104 0412, 0204	1003	1103, 1309, 0322	0625		
0535	0434, 0334	0726, 0735	0835	1133	1108	0933	1235	1335
0631	1334	0630, 0705	0631	0632, 1034	1134	1234	1134	0634
0611, 0533	0234, 0134	0612, 0733	0614, 0833	0616, 1035	0935	1127, 1035	1135, 1233	0618, 1333

2

## CIRCUIT BOARDS

<u>Circuit Jack #</u>	<u>Underwater Unit</u>	<u>Part Number</u>	<u>Page</u>
J1	Pressure Interface	001-PC-01-2	5.1.1
J2	Temperature Interface	002-PC-01-2	5.1.2
J3	Fast Response Temp. Interface	003-PC-01-1	5.1.3
J4	Conductivity Interface	004-PC-01-2	5.1.4
J5	Oxygen Interface (Optional)	020-PC-01-0	5.1.5
J6	Power Supply (U.W.U.)	008-PC-01-0	5.1.6
J7	Comparator	005-PC-01-1	5.1.7
J8	D/A Converter	006-PC-01-1	5.1.8
J9	Digitizer Logic	007-PC-01-1	5.1.9
J10	Memory & Multiplexer	010-PC-01-1	5.1.10
J11	Adaptive Sampling	C10009-	5.1.11
J12	TTY Formatter & FSK Modulator	014-PC-01-1	5.1.12
J13	Signal Generator	C10066-	5.1.13
J14	Sensor Head	019-PC-01-1	5.1.14
<u>Circuit Jack #</u>	<u>Deck Unit</u>	<u>Part Number</u>	<u>Page</u>
J1-J2(D)	Display Card	016-PC-02-1	5.2.1
J3-J4(D)	Number Converter	015-PC-02-0	5.2.2
J5-J6(D)	D/A Converter	017-PC-02-1	5.2.3
J7-J8(D)	Demodulator	014-PC-02-1	5.2.4
J9-J10(D)	Option Card		5.2.5
	Power Supply (D.U.)	018-PC-02-0	5.2.6
	Chassis Mounted Circuits		5.2.7



Fig. 5.1

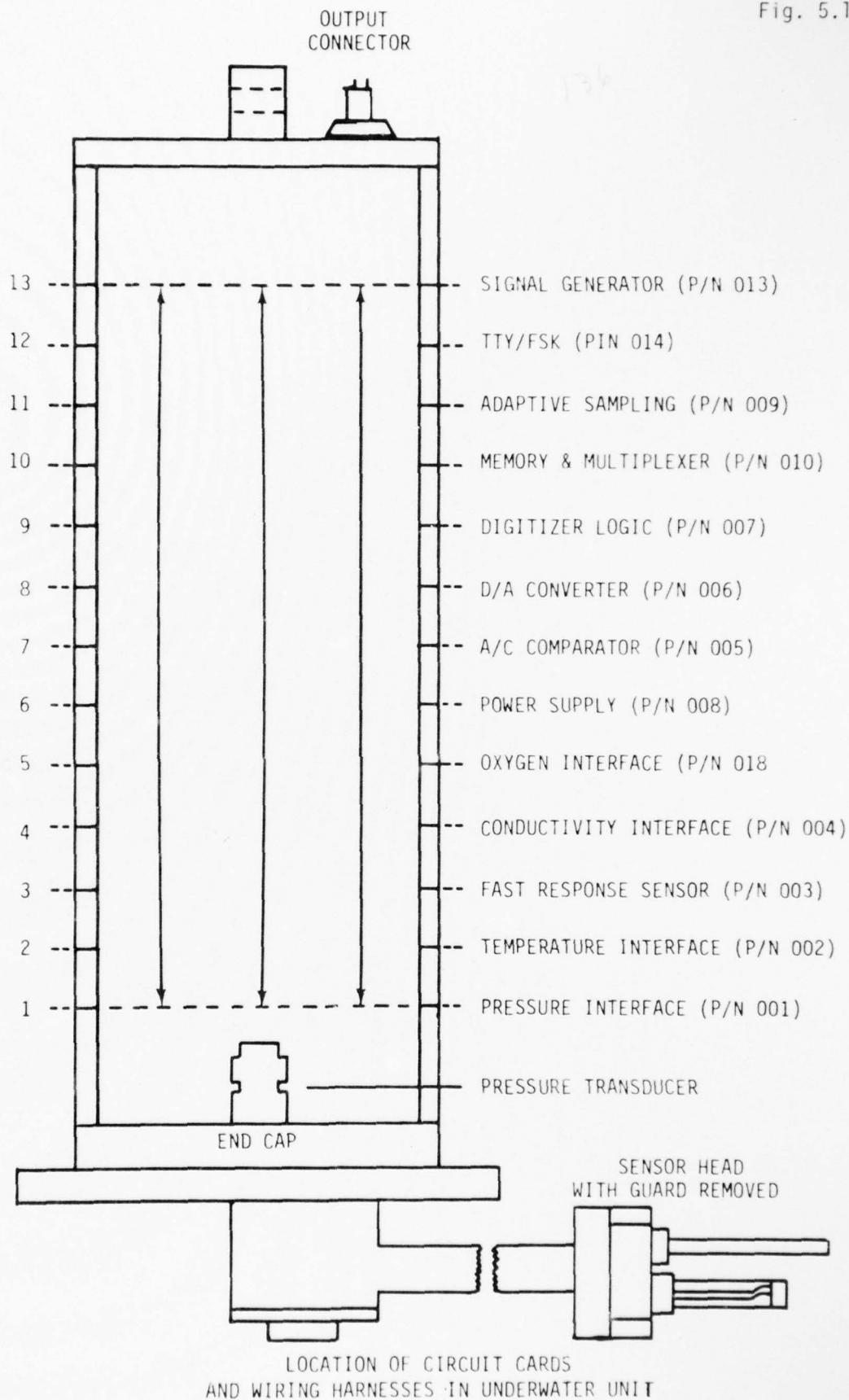
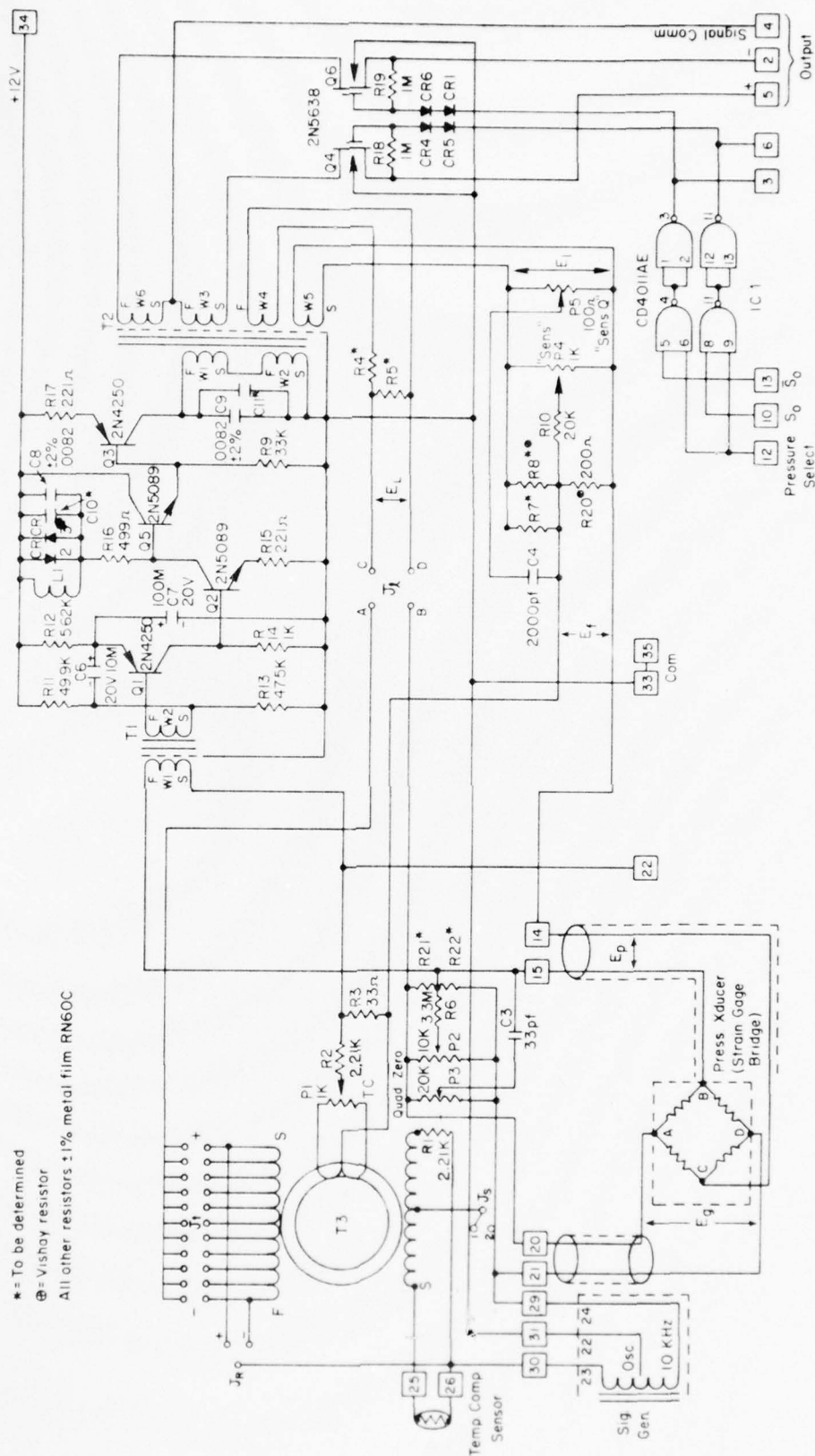




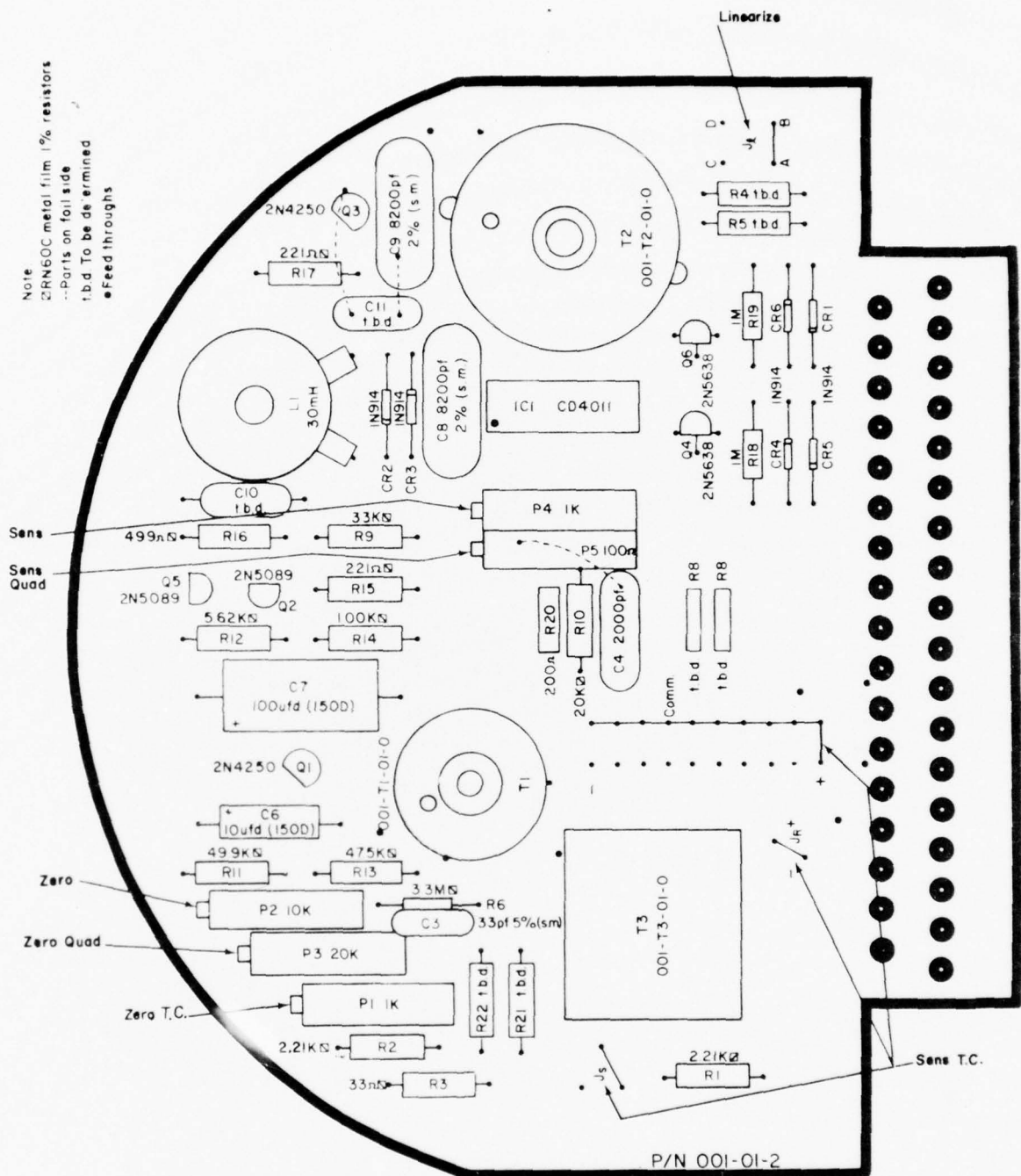
Fig. 5.1.1



\* = To be determined  
 @ = Vishay resistor  
 All other resistors ±1% metal film RN60C

CTD UNDERWATER UNIT MK III PRESSURE INTERFACE

Fig. 5.1.1(2)

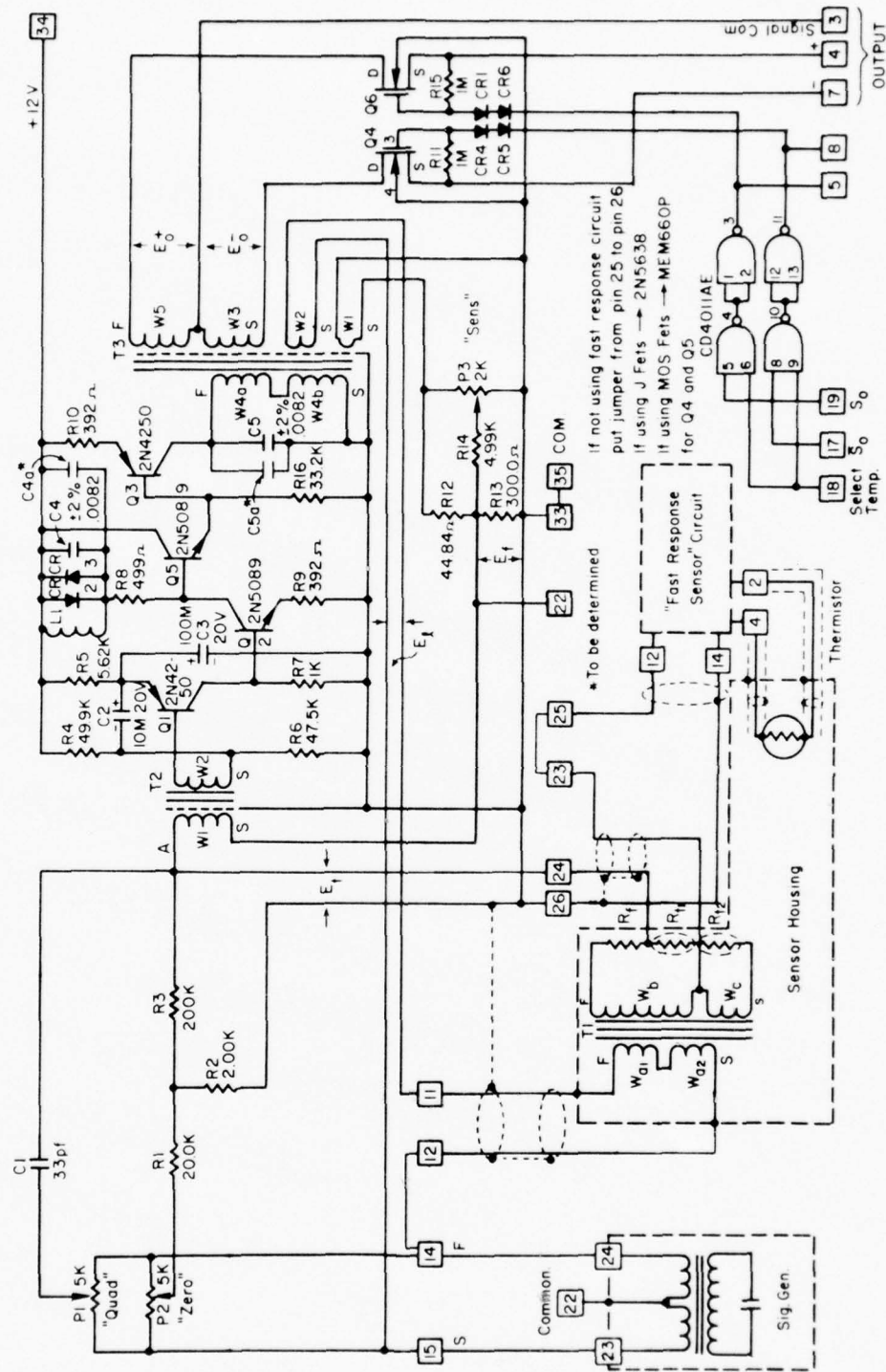


PRESSURE INTERFACE

Board Title PRESSUREBoard Number 01

Pin #	Function	Connected To	Color	Harness Posn			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1									
2	SIGNAL -	0412, 0832 0204, 0105, 0207	wh			X		COAX	X
3	SELECT SIG -				X				
4	SIGNAL COMM.	0706, 0730 0203, 0413 0412, 0832	wh			X		COAX	X
5	SIGNAL +	0102, 0204, 0207	wh						
6	SELECT + SIG								
7									
8									
9									
10	So	0219, 0903	ylw		X				
11									
12	SELECT PRESS.	1001	wh/ylw		X				
13	So	0217, 1130, 0904	grn		X				
14	(PRESS. TRANS)	Bendix Conn. C	blk			X		0115	
15	(DUCER O/P )	Bendix Conn. B	wh			X			
16	JUMPER	0117	wh						
17	JUMPER	0116	wh						
18	JUMPER	0119	wh						
19	JUMPER	0118	wh						
20	(TRANSDUCER)	Bendix Conn. A	blk			X		0121	
21	(EXCITATION)	Bendix Conn. D	wh			X		0120	
22	T.P.								
23									
24									
25	(TEMP. COMP.)					X			
26	(THERMISTOR )					X			
27									
28									
29	REF SINE	0309, 0403 1324, 0214, 0801	wh/blk			X	0130		
30	REF SINE	0401, 0802 1323, 0215, 0308	wh/red			X	0129		
31	TRANS. C. T.	0133, 1322							
32									
33	COMMON	1322, 0131, 0135	blk						
34	+12V	0634	red		X		0135		
35	COMMON	0619, 0133	blk		X		0134		

Fig. 5.1.2



CTD UNDERWATER UNIT MK III TEMPERATURE INTERFACE

Fig. 5.1.2(2)

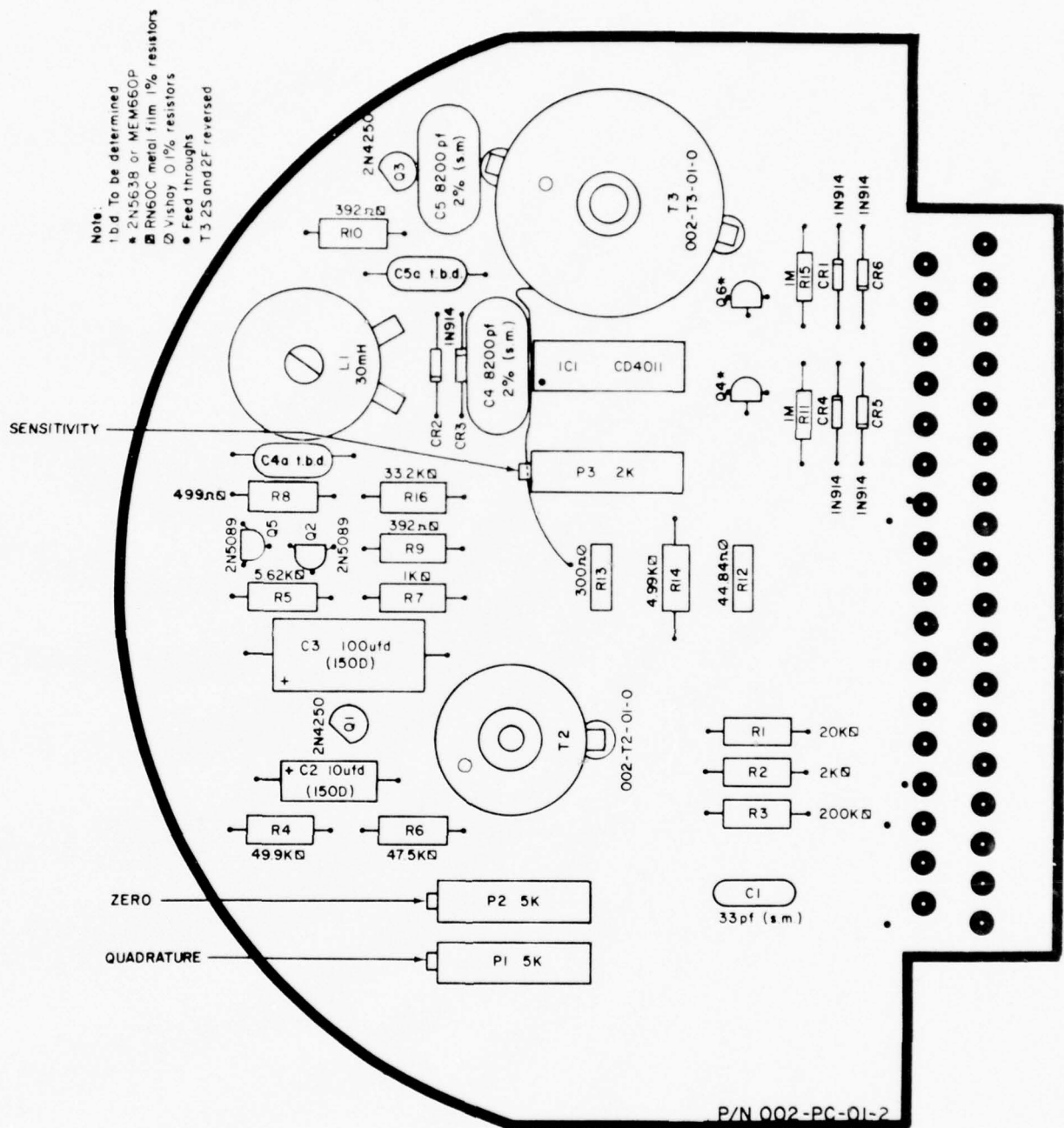




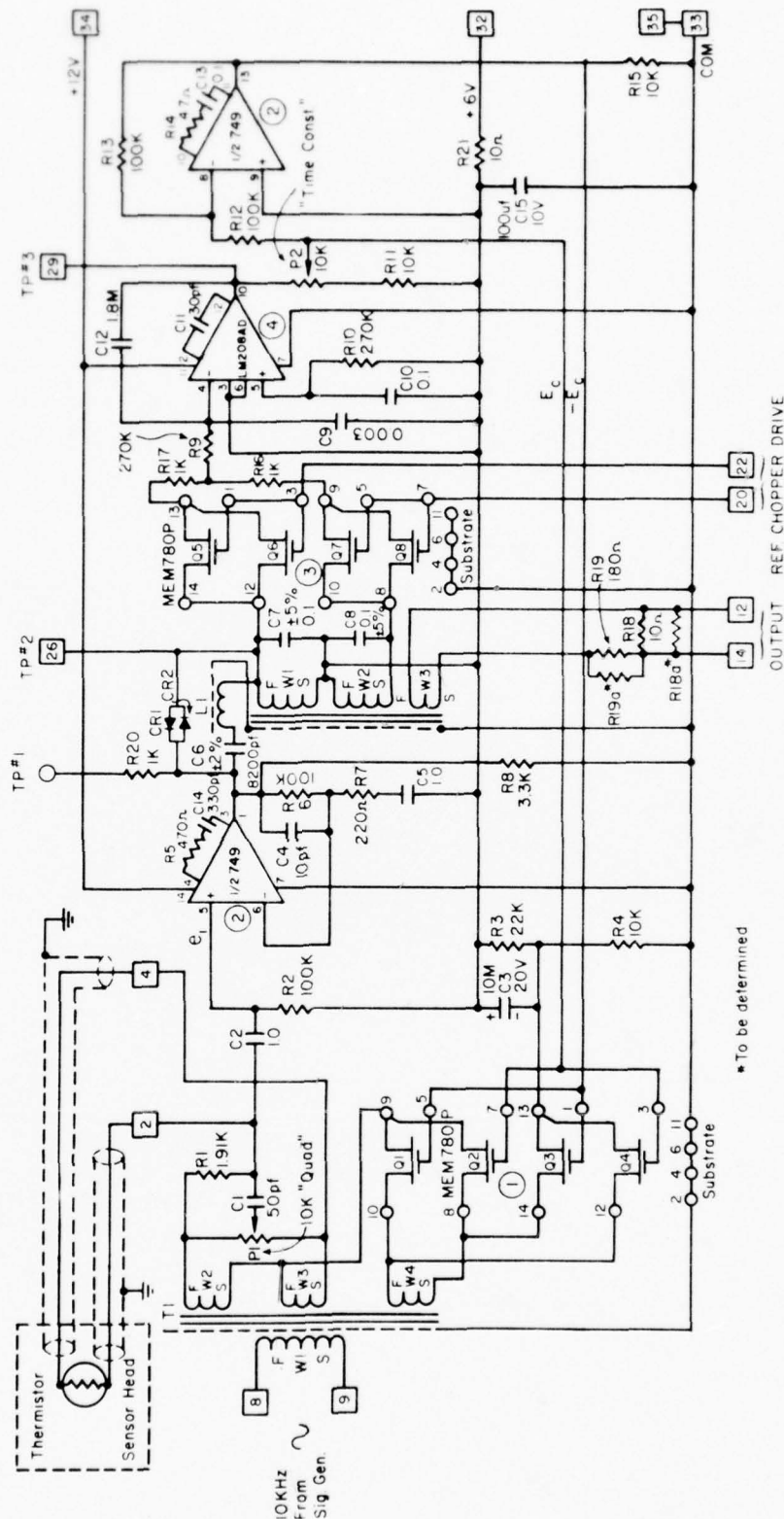
Fig. 5.1.2(3)

Board Title TEMPERATUREBoard Number 02

Pin #	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1									
2									
3	TEMP. SIGNAL COM	0706 0415, 0104, 0730	wh					COAX	X
4	TEMP. SIG. +	0105, 0832 0412, 0102, 0207	wh					COAX	X
5	SELECT + O/P								
6									
7	TEMP. SIG. -	0412, 0832 0204, 0102, 0105	wh						X
8	SELECT - O/P								
9									
10									
11	(SENS BRIDGE)	Sensor Hd #14	blk			X		0212	X
12	{ DRIVE }	Sensor Hd #15	wh			X		0211	X
13									
14	REF SINE	0309, 0403 1324, 0129	wh/blk			X	0215		
15	REF SINE	0308, 0401 1323, 0130, 0215	wh/red			X	0214		
16									
17	S <sub>0</sub>	0904, 0113, 1130	grn						
18	SELECT TEMP	1107, 1007	wh/blk						
19	S <sub>0</sub>	0903, 0110	ylw						
20									
21									
22									
23	(SENSOR BRIDGE)	Sensor Hd #4	blk			X		0224	
24	{ OUTPUT }	Sensor Hd #12	wh			X		0223	
25	FAST. RESP. IN	0312							
26	FAST. RESP. IN	0314							
27									
28									
29									
30									
31									
32									
33	COMMON	0235							
34	+12V	0633							
35	COMMON	0617, 0233							

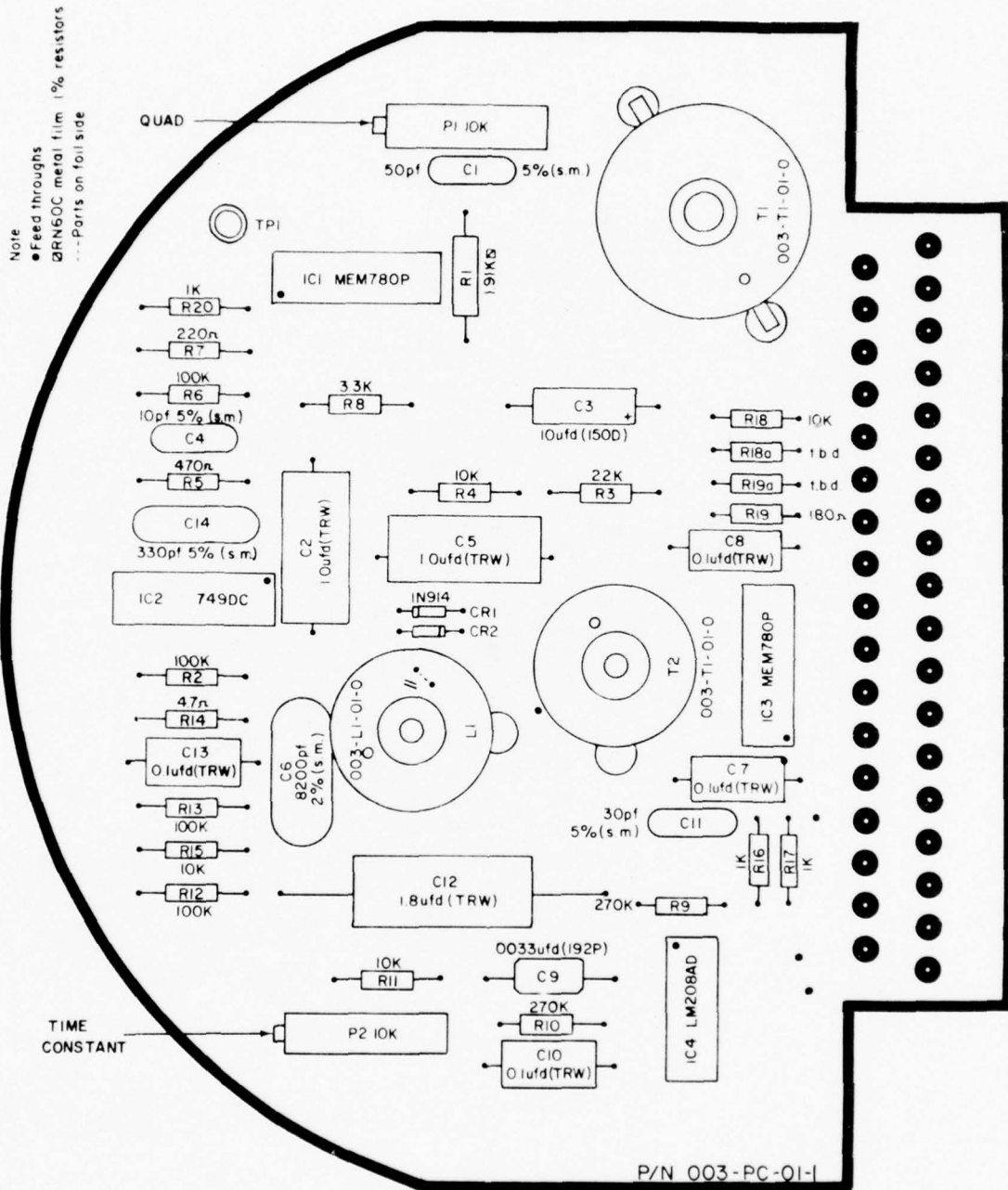
MKIIIb CTD

Fig. 5.1.3



CTD UNDERWATER UNIT MK III FAST RESPONSE TEMPERATURE INTERFACE

Fig. 5.1.3(2)



CTD Underwater Unit Mk III

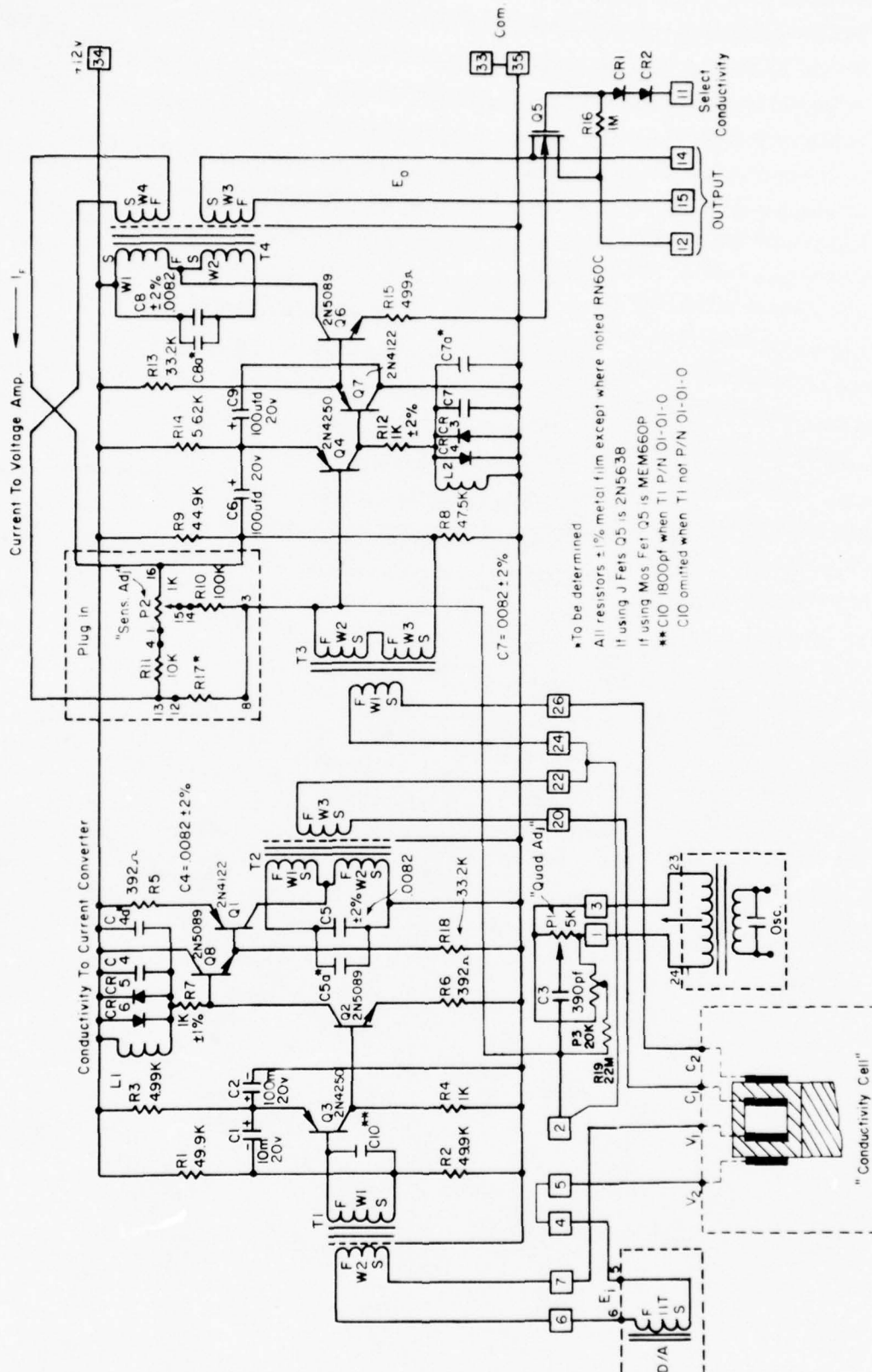
FAST RESPONSE TEMPERATURE INTERFACE

Fig. 5.1.3(3)

Board Title FAST RESPONSEBoard Number 03

Pin #	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1									
2	THERMISTOR HI	Sensor Hd #3	wh						
3									
4	THERMISTOR LO	Sensor Hd #2	wh						
5									
6									
7									
8	REF SINE	0215 1323, 0401, 0130	wh/red			x	0309		
9	REF SINE	0129, 0214 1324, 0309, 0403	wh/blk			x	0308		
10									
11									
12	OUTPUT	0225	blu				0314		x
13									
14	OUTPUT	0226	blk				0312		x
15									
16									
17									
18									
19									
20	REF CHOP	1308, 0722	blu		x		0322		
21									
22	REF CHOP	1309, 1032, 1103	gra		x		0320		
23									
24									
25									
26	T. P. #2								
27									
28									
29	T. P. #3								
30									
31									
32	+6V	0626	orn	x			0334, 0335		
33	COMMON	0335	link						
34	+12V	0632	red	x			0332, 0335		
35	COMMON	0615, 0333	blk	x			0332, 0334		

Fig. 5.1.4

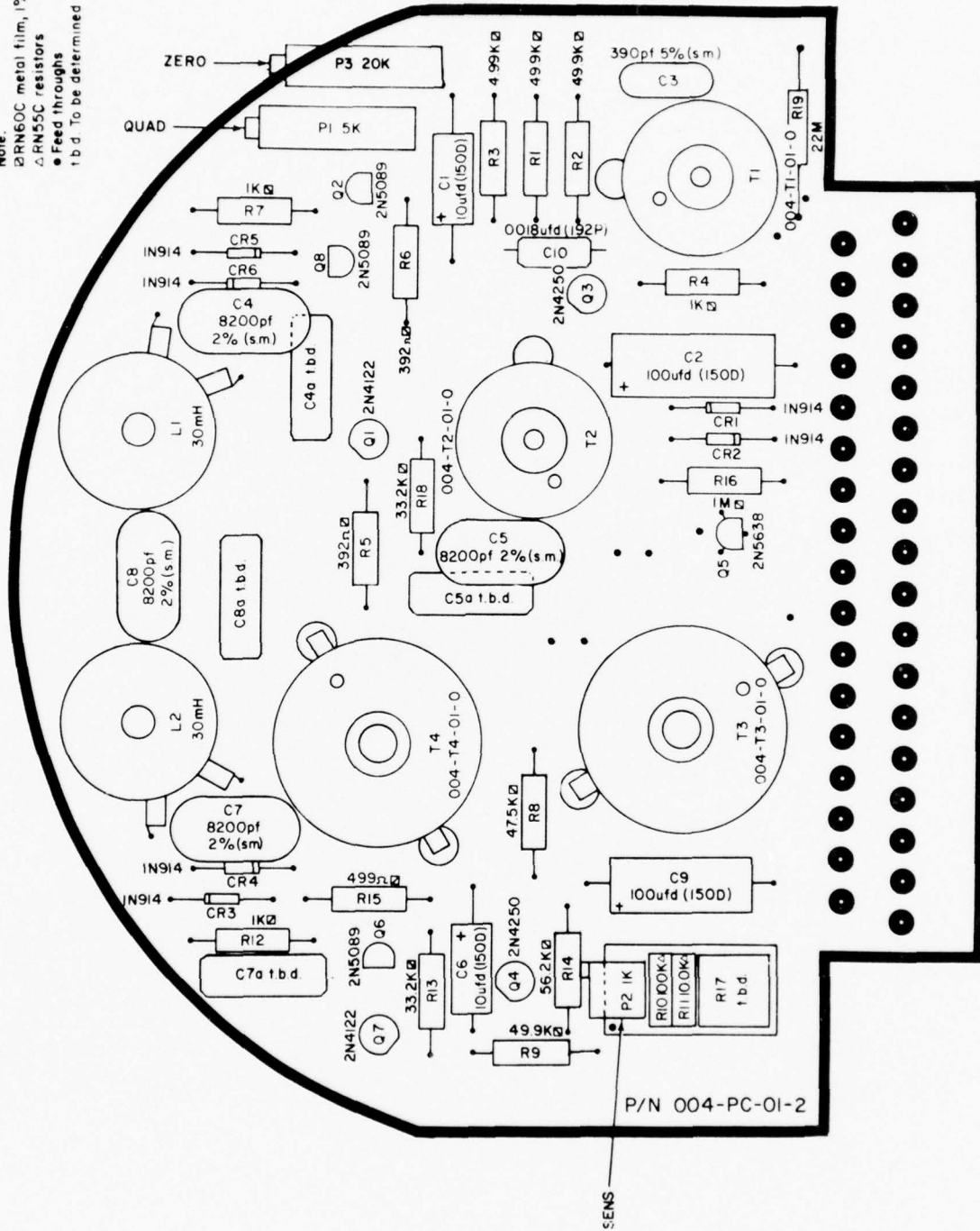


CTD UNDERWATER UNIT MK III CONDUCTIVITY INTERFACE



Fig. 5.1.4(2)

Note:  
 ▽ RN60C metal film, 1% resistors  
 △ RN55C resistors  
 ● Feed throughs  
 t.b.d. To be determined



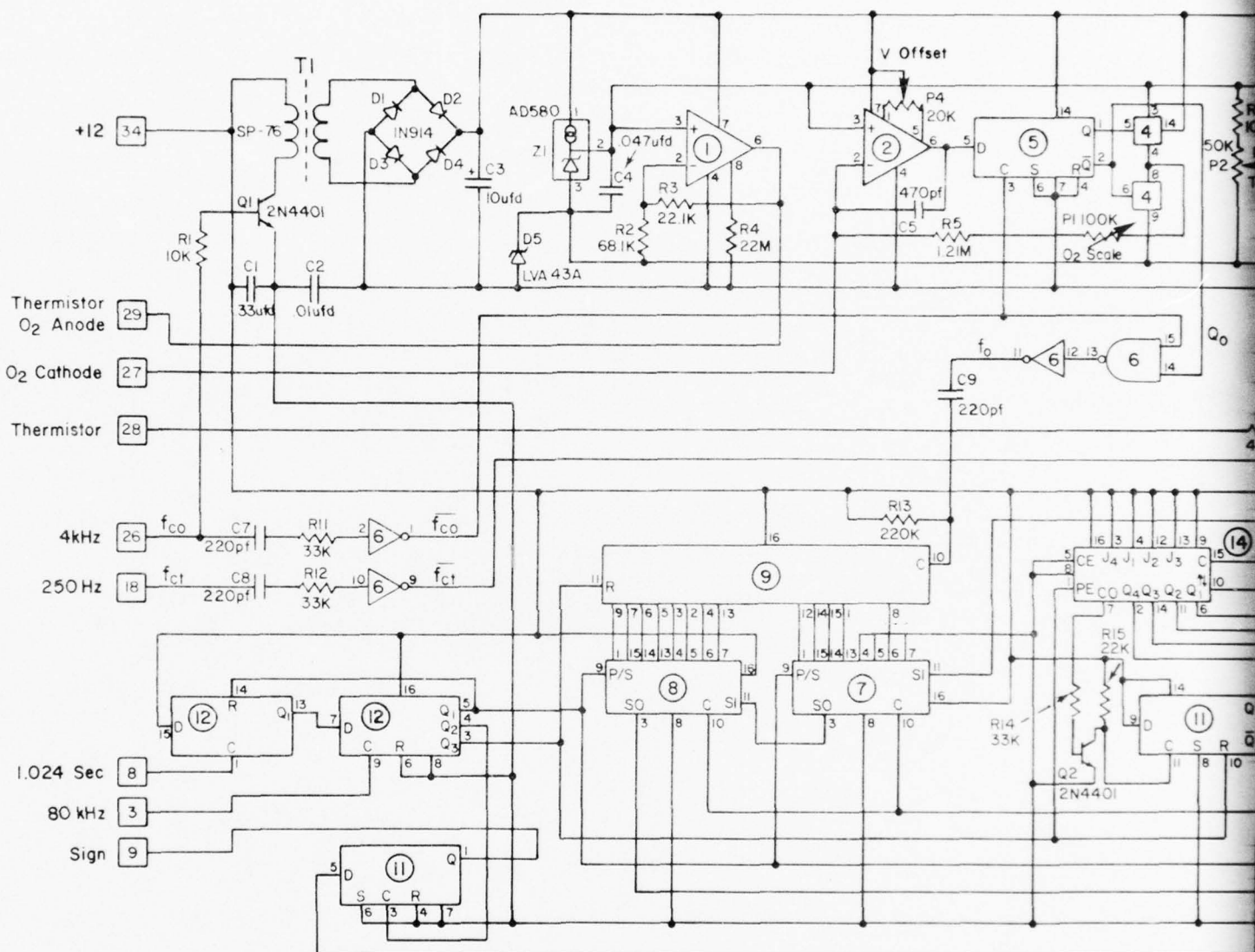
CONDUCTIVITY INTERFACE

Fig. 5.1.4(3)

Board Title CONDUCTIVITY (3CM CELL)Board Number 04

Pin	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1	REF SINE	0214, 0802 1323, 0309, 0219	wh/red			X	0403		
2	QUAD OUT	0423	orn						X
3	REF SINE	0214, 0801 1324, 0309, 0129	wh/blk			X	0401		
4	D/A REF	0805	ylw			X	0406		
5	V2 ELECTRODE	Sensor Hd #2C	blk					0407	
6	D/A REF	0806	grn			X	0404		
7	V1 ELECTRODE	Sensor Hd #C1	wh					0405	
8									
9									
10									
11	COND. SELECT	1101, 1029	wh		X				
12	S. W. SIGNAL OUT	0102, 0105 0832, 0204, 0207	wh			X		COAX	X
13									
14	SIGNAL OUT					X		COAX	X
15	SIG. COMMON	0730 0706, 0203, 0104	wh			X		COAX	X
16									
17									
18									
19									
20	C2. ELECTRODE	0402 Sensor Hd #17	red					0420	
21									
22	CURRENT LOOP	0424	wh						
23	QUAD IN	0402							
24	CURRENT LOOP	0422	wh						
25									
26	C1. ELECTRODE	Sensor Hd #18	blk					0426	
27									
28									
29									
30									
31									
32									
33	COMMON	0435							
34	+12V	0631	red	X			0435		
35	COMMON	0613, 0433	blk	X			0434		

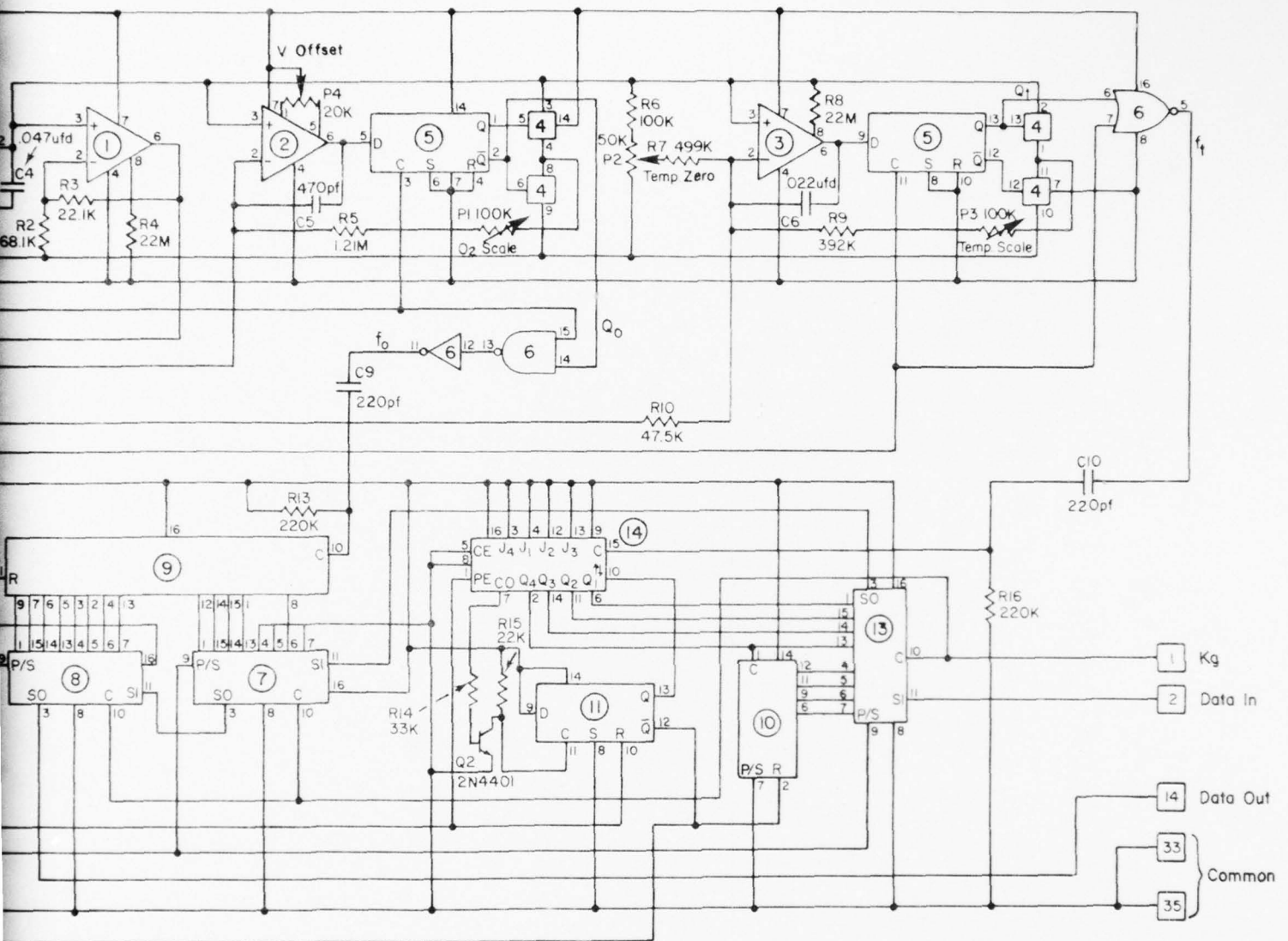
MK11



- |                 |                 |                         |              |
|-----------------|-----------------|-------------------------|--------------|
| (4) = CD4066AE  | (10) = CD4024AE | (5) (11) = CD4013AE     | (2) = LF355H |
| (6) = MCI4572CP | (12) = CD4015AE | (1) (3) = $\mu$ A776    |              |
| (9) = CD4040AE  | (14) = CD4029AE | (7) (8) (13) = CD4021AE |              |

CTD UNDERWATER UNIT MK III OXYGEN INTERFACE (

Fig. 5.1.5



= CD4013AE (2) = LF355H

=  $\mu$ A776

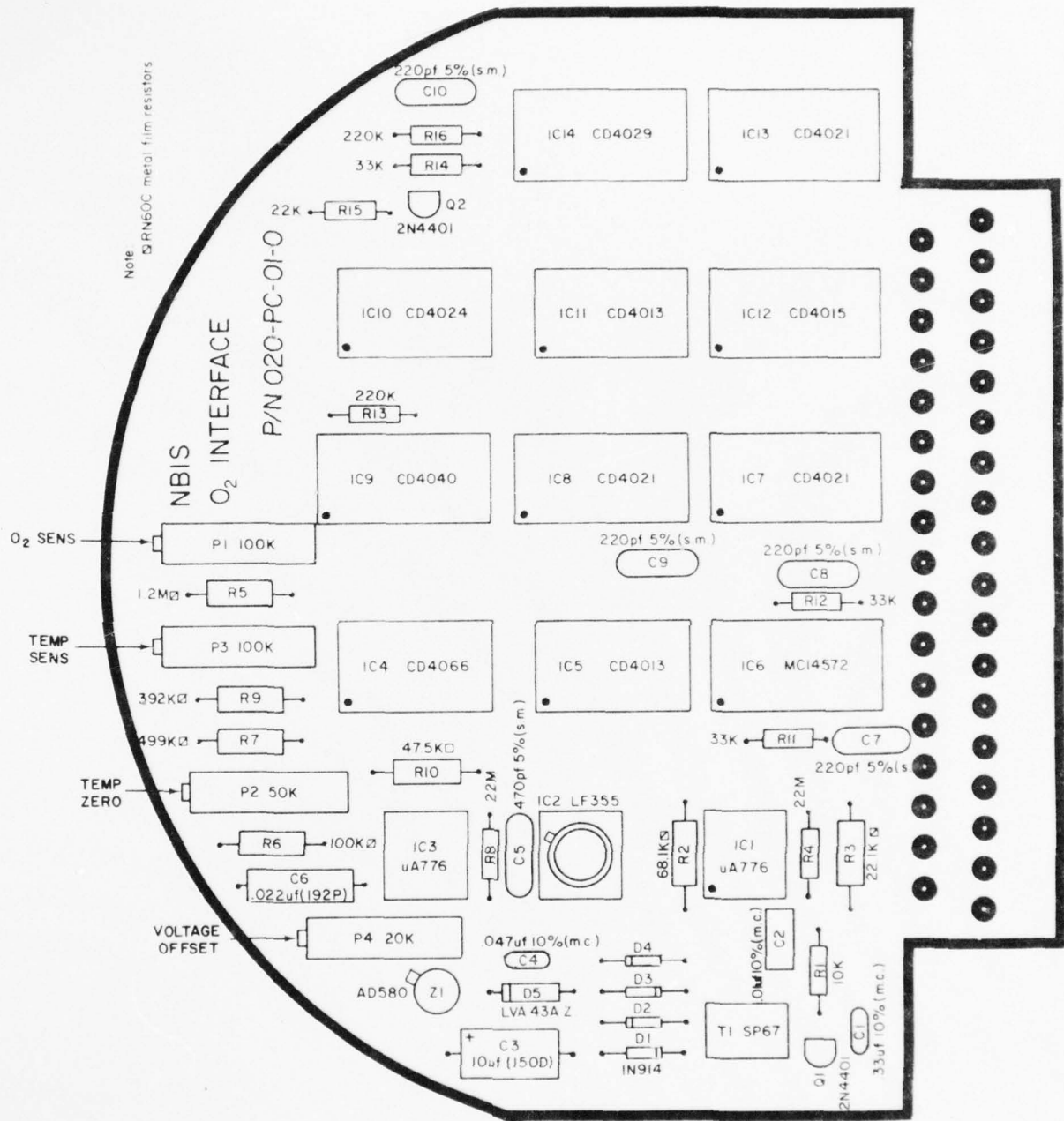
(13) = CD4021AE

UNDERWATER UNIT MK III OXYGEN INTERFACE (12 BIT)

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2

Fig. 5.1.5(2)



OXYGEN INTERFACE (12 BIT)

CTD Underwater Unit MK III



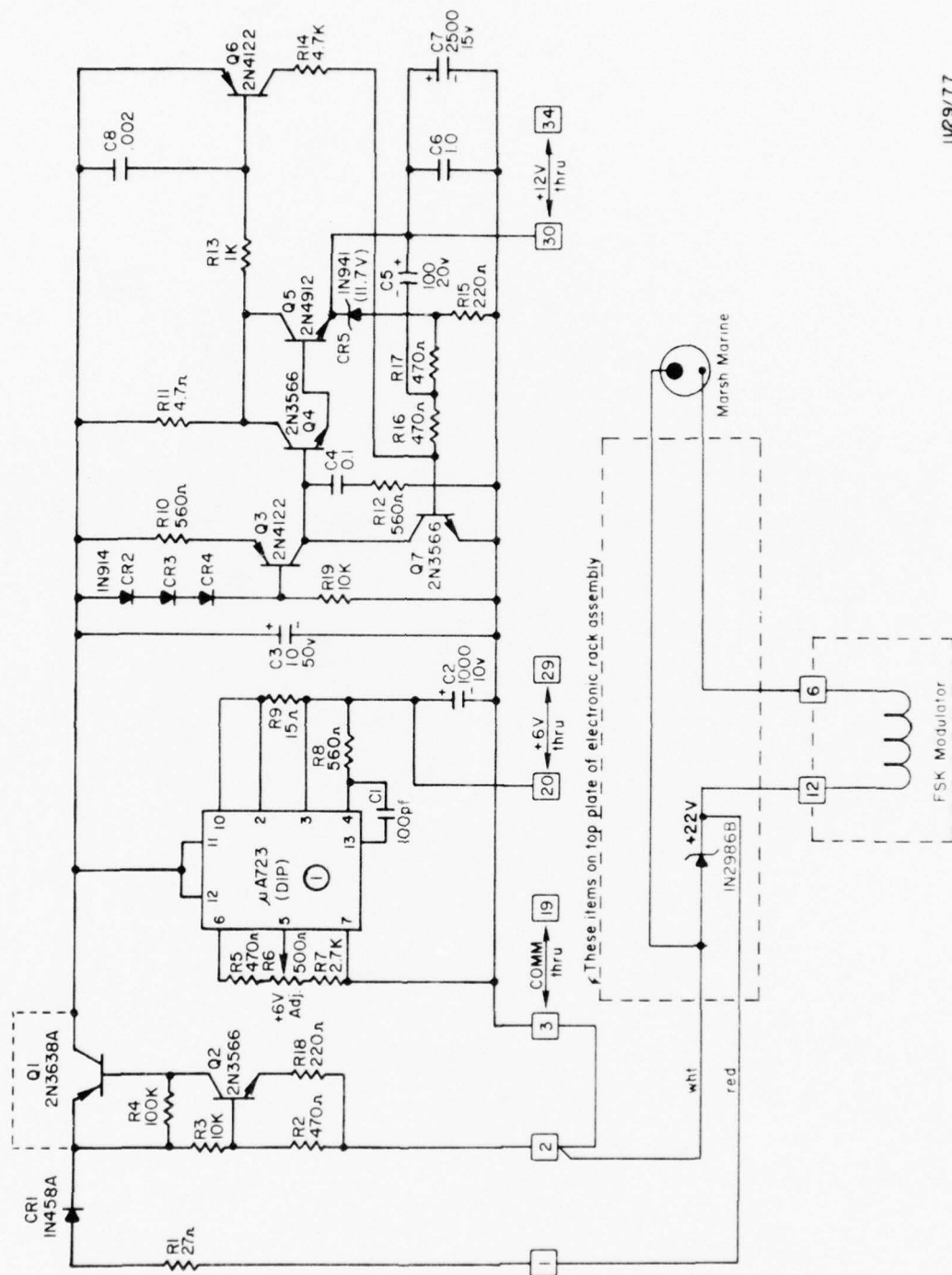
Fig. 5.1.5(3)

Board Title 12-BIT OXYGENBoard Number 05

Pin #	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1	GATED CLK	1008, 1207 0928, 1117	wh/blu		X				
2	DATA IN	0514, 1109	ylw		X				
3	80 KHz	1313, 1229	brn		X				
4									
5									
6									
7									
8	1.024 SEC	1306	vio		X				
9	O <sub>2</sub> SIGN	1111	gra		X				X
10									
11									
12									
13									
14	DATA OUT	1109, 0502	ylw		X				X
15									
16									
17									
18	250 Hz	1302	grn/wh		X				
19									
20									
21									
22									
23									
24									
25									
26	4 KHz	1301	orn/wh		X				
27	O <sub>2</sub> CATHODE	Sensor Head #13	red			X			
28	THERMISTOR	Sensor Head #15	red			X			
29	O <sub>2</sub> ANODE THERMISTOR	Sensor Head #12 #14	blk/blk			X			
30									
31									
32									
33	COMMON	0535		X					
34	+12V	0631		X					
35	COMMON	0611, 0533		X					

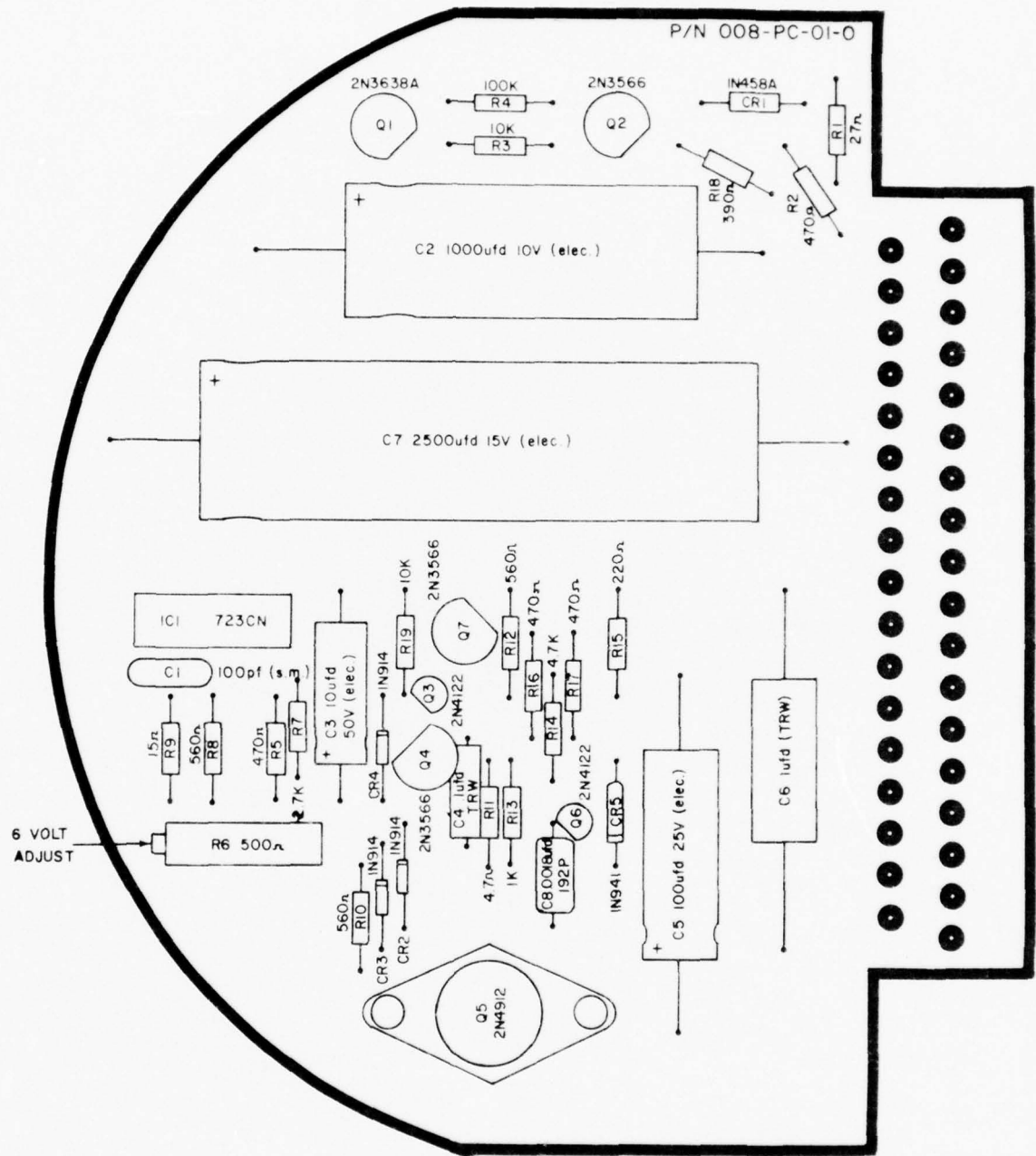
MKIIIb CTD

Fig. 5.1.6



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Fig. 5.1.6(2)



U.W.U. POWER SUPPLY

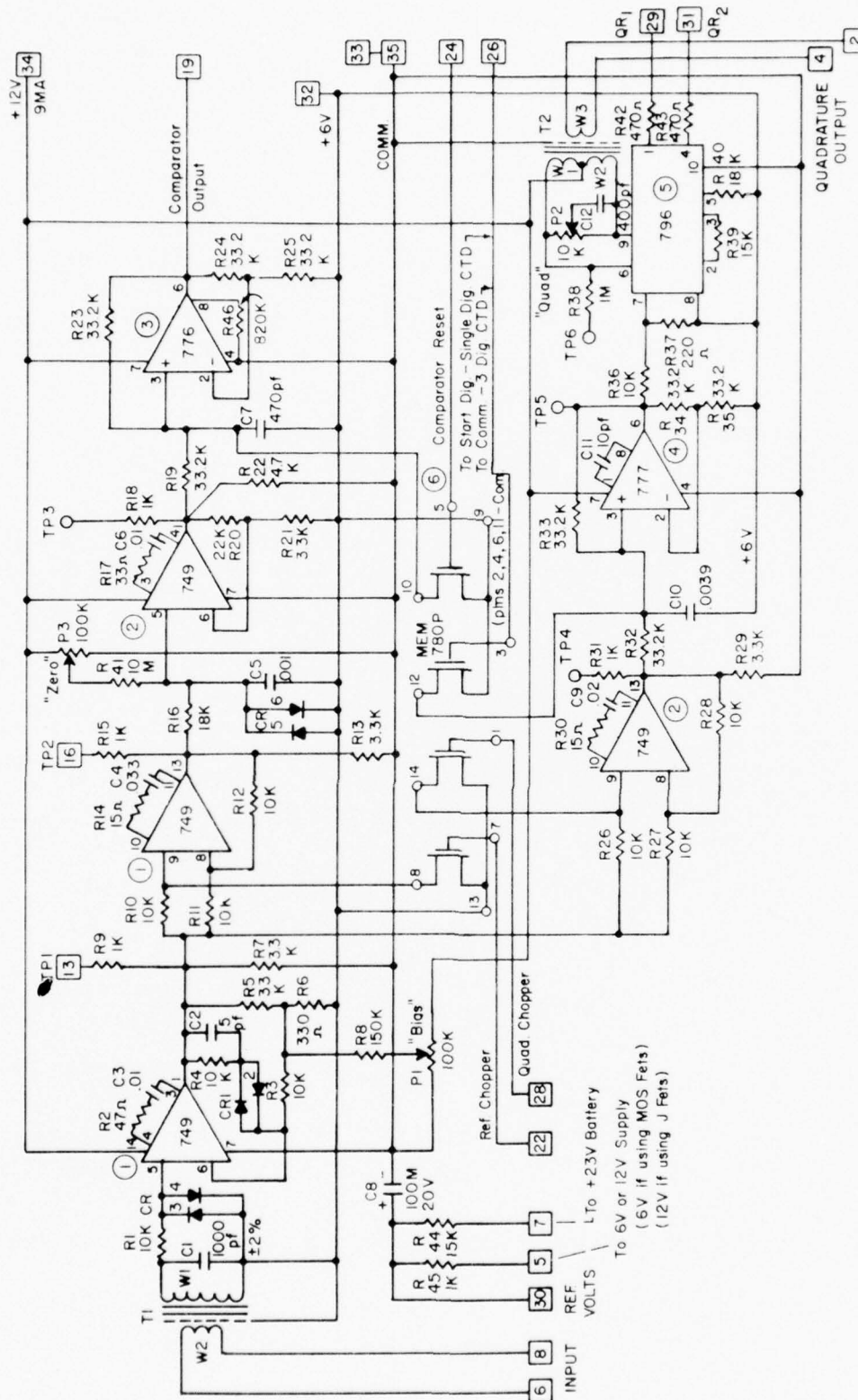
CTD Underwater Unit MK III  
11/77

Fig. 5.1.6(3)

Board Title POWER SUPPLYBoard Number 06

Pin #	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1	+22V IN	End Plate P.S.	red	X					
2	SWITCH	End Plate 0603	wh	X					
3	COMMON	0602	blk	X					X
4	COMMON			X					X
5	COMMON			X					X
6	COMMON			X					X
7	COMMON			X					X
8	COMMON			X					X
9	COMMON			X					X
10	COMMON			X					X
11	COMMON	0535	blk	X					X
12	COMMON	0735	blk	X					X
13	COMMON	0435	blk	X					X
14	COMMON	0835	blk	X					X
15	COMMON	0335	blk	X					X
16	COMMON	0935	blk	X					X
17	COMMON	0235	blk	X					X
18	COMMON	1335	blk	X					X
19	COMMON	0135	blk	X					X
20	+6V			X					X
21	+6V			X					X
22	+6V			X					X
23	+6V			X					X
24	+6V	0732	orn	X			0630, 0612		X
25	+6V			X					X
26	+6V	1132	orn	X					X
27	+6V			X					X
28	+6V			X					X
29	+6V	0332	orn	X			0633, 0615		X
30	+12V	0734, 0834	red	X			0612, 0614		X
31	+12V	0534, 0434	red	X			0611, 0613		X
32	+12V	0934	red	X			0616		X
33	+12V	0434, 0334	red	X			0613, 0615		X
34	+12V	1334	red	X			0618		X
35	+12V	0234, 0134	red	X			0617, 0619		X

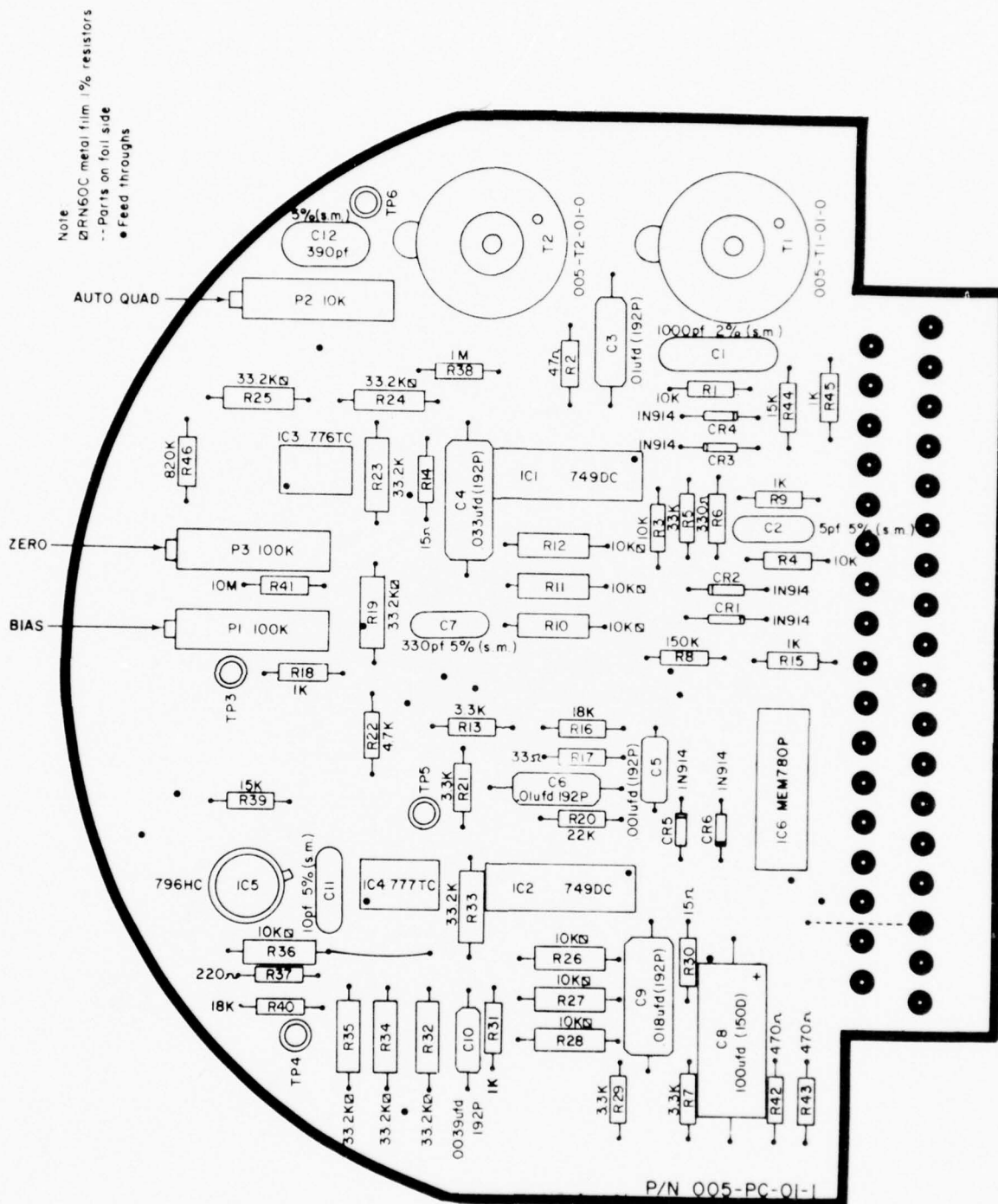
Fig. 5.1.7



CTD UNDERWATER UNIT MK III A.C. COMPARATOR



Fig. 5.1.7(2)



A/C COMPARATOR

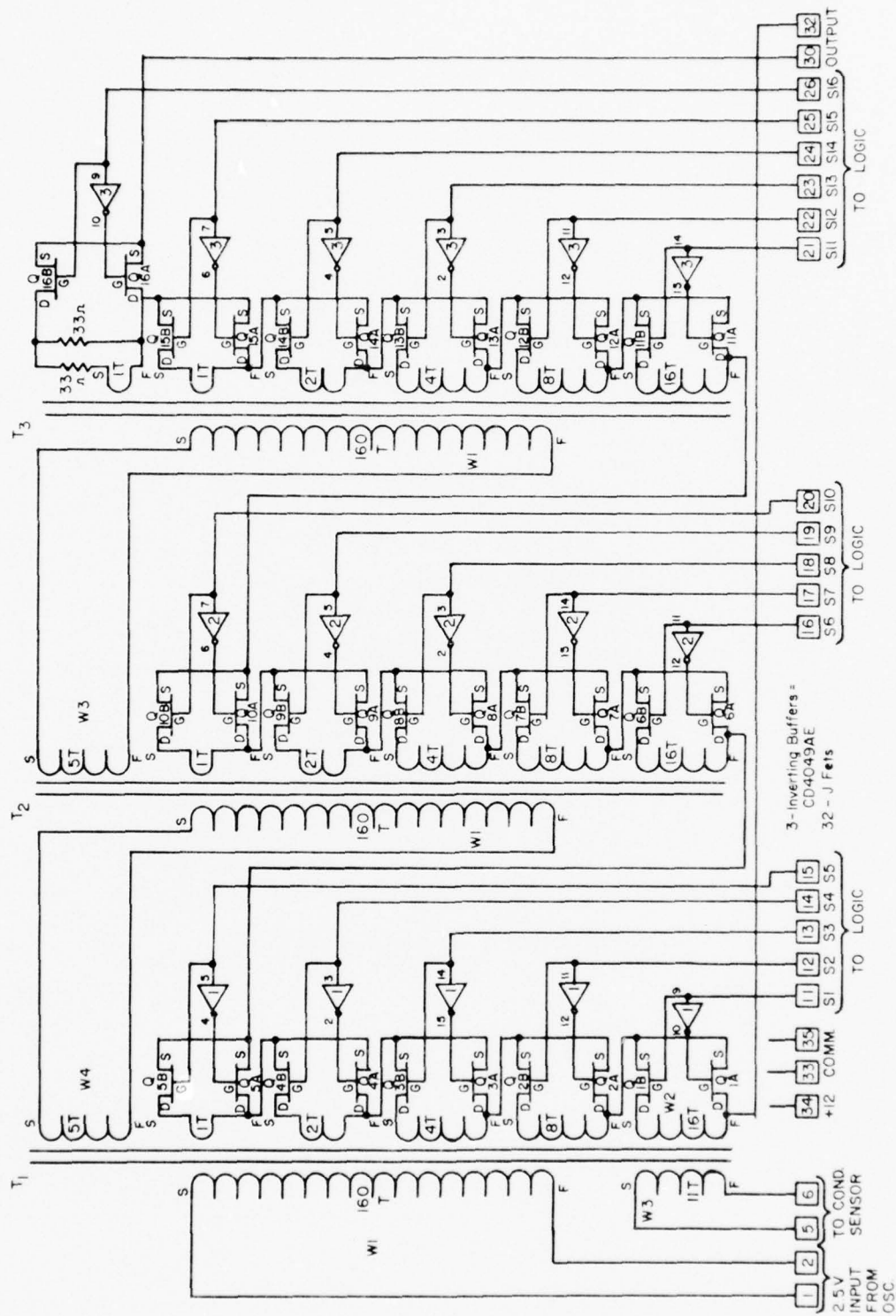
Fig. 5.1.7(3)

Board Title COMPARATORBoard Number 07

Pin X	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1									
2	QUAD OUTPUT	0830	wh			X		COAX	X
3									
4	QUAD OUTPUT	0708	wh/red			X			X
5	12V	0734	red						
6	COMPARATOR I/P	0730, 0415	red/wh			X		COAX	
7	+22V	0601	blu	X					
8	COMPARATOR I/P	0704	wh/red						
9									
10									
11									
12									
13	T. P. #1	1113	wh/blu		X				X
14									
15									
16	T. P. #2								
17									
18									
19	COMPARATOR O/P	0905, 1105	blu		X				X
20									
21									
22	REF CHOP	1308, 0320	blu		X		0728		
23									
24	COMP. RESET	1104	brn		X				
25									
26	START DIG	0733, 0735	blk						
27									
28	QUAD CHOP	1304	grn		X		0722		
29	QUAD SINE	1329	orn			X	0731		
30	VOLTAGE REF	0415 0706, 0203, 0104	red						X
31	QUAD SINE	1330	wh			X	0729		
32	+6V	0627		X					
33	COMMON	0726, 0735	blk						
34	+12V	0630, 0705	red	X					
35	COMMON	0612, 0733	blk	X					

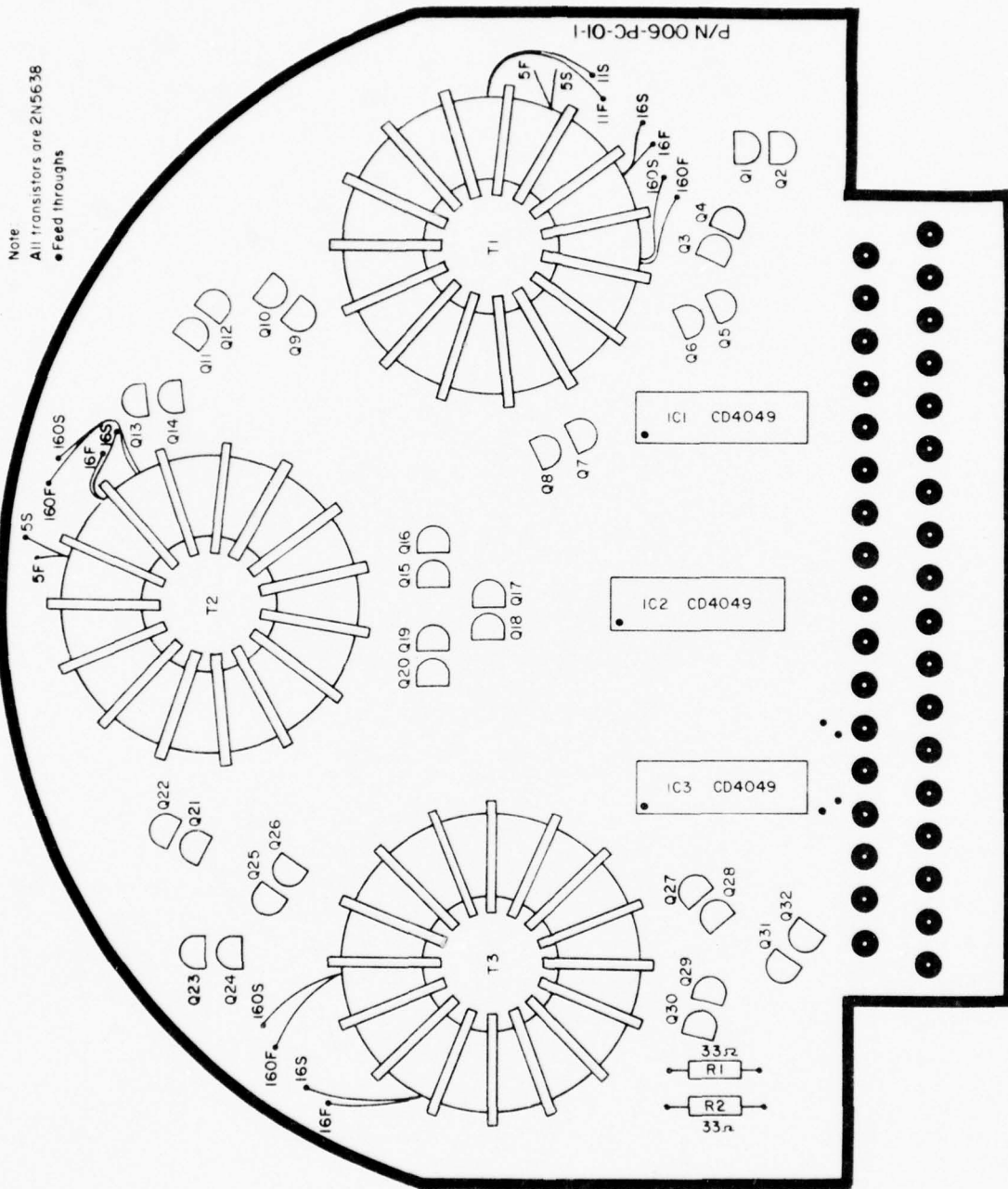
NB1S .

Fig. 5.1.8



CTD UNDERWATER UNIT MK III D/A CONVERTER

Fig. 5.1.8(2)



D/A CONVERTER

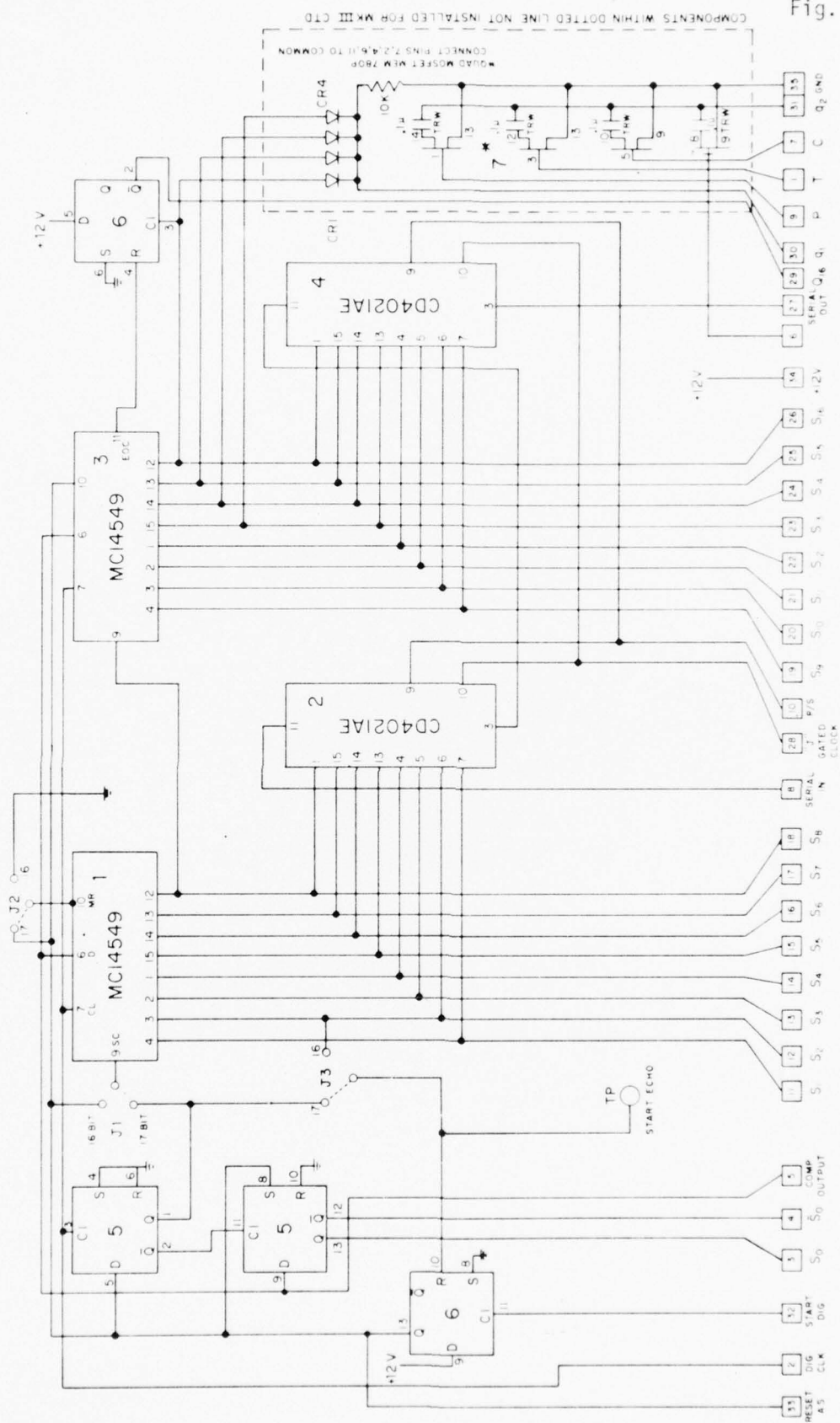
CTD Underwater Unit MK III

Fig. 5.1.8(3)

Board Title D/A CONVERT.Board Number 08

Pin	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1	REF. SINE	0129, 0214 1324, 0509, 0403	wh/blk			X	0802		
2	REF. SINE	0130, 0215 1323, 0308, 0401	wh/red			X	0801		
3									
4									
5	COND REF	0404	ylw			X	0806		X
6	COND REF	0406	brn			X	0805		X
7									
8									
9									
10									
11	BIT #1	0911, 1011	red						
12	BIT #2	0912, 1012	"						
13	BIT #3	0913, 1013	"						
14	BIT #4	0914, 1014	"						
15	BIT #5	0915, 1015	"						
16	BIT #6	0916, 1016	"						
17	BIT #7	0917, 1017	"						
18	BIT #8	0918, 1018	"						
19	BIT #9	0919, 1019	"						
20	BIT #10	0920, 1020	"						
21	BIT #11	0921, 1021	"						
22	BIT #12	0922, 1022	"						
23	BIT #13	0923, 1023	"						
24	BIT #14	0924, 1024	"						
25	BIT #15	0925, 1025	"						
26	BIT #16	0926, 1026	"						
27									
28									
29									
30	D/A OUTPUT	0702	wh			X		COAX	
31									
32	D/A OUTPUT	0207, 0102, 0104 0412, 0204, 0403	wh			X		COAX	
33	COMMON	0835	link						
34	+12V	0631	red	X					
35	COMMON	0614, 0833	blk	X					





CTD UNDERWATER UNIT MK III DIGITIZER LOGIC

Fig. 5.1.9(2)

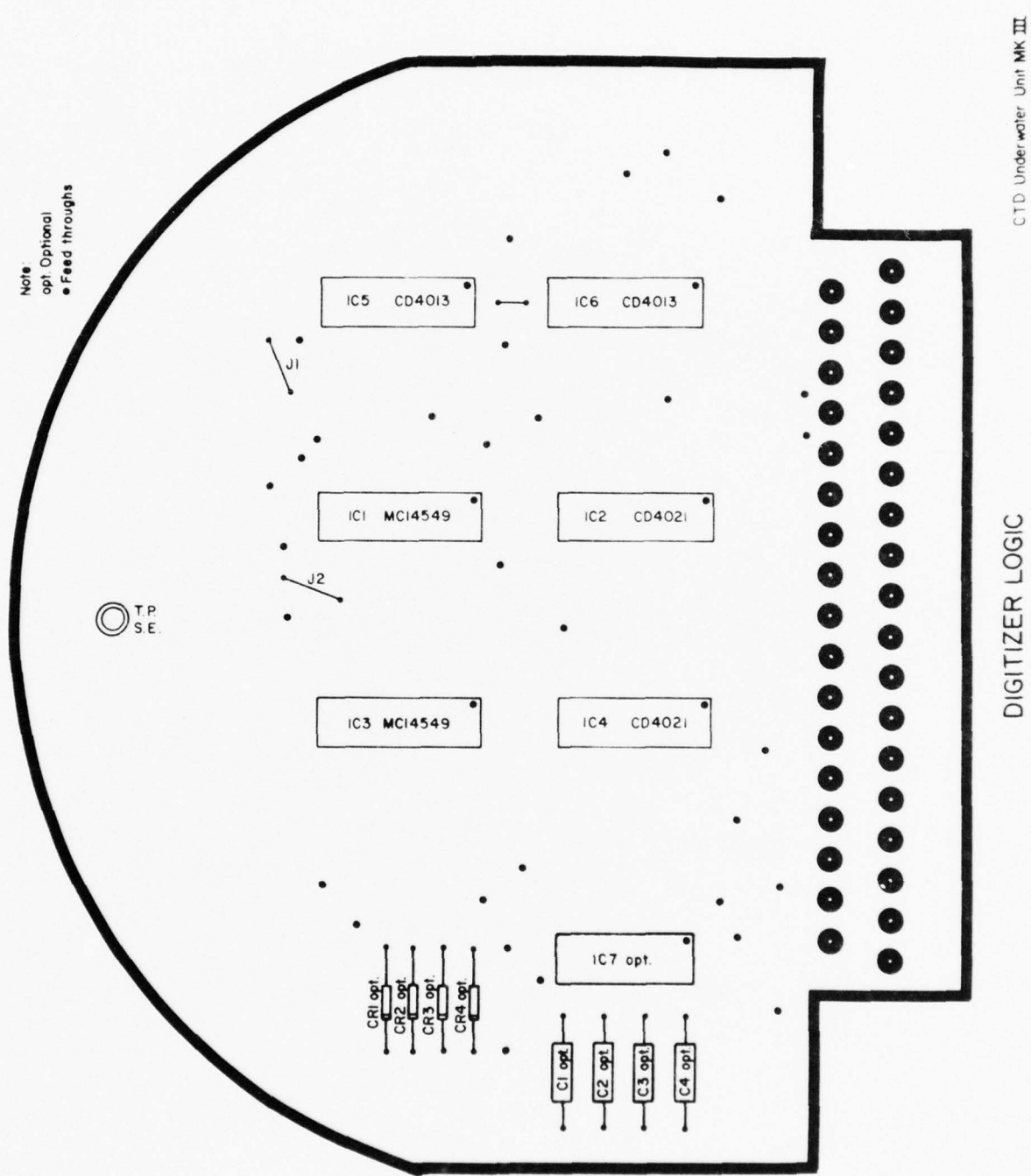


Fig. 5.1.9(3)

Board Title DIGI. LOGICBoard Number 09

Pin #	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1	Q. MEM. T.				X				
2	DIGI CLK	1102	wh/grn		X				
3	S <sub>Q</sub>	0219, 0110	ylw		X				X
4	S <sub>O</sub>	0217, 1130, 0113	grn		X				X
5	COMP. OUTPUT	0719, 1105	blu		X				
6									
7	Q. MEM. C.				X				
8	SER. DATA IN	1106	gra		X				
9	W. MEM. P.				X				
10	P/S	1118, 0210	wh/grn		X				
11	BIT #1	1011, 0811	red						X
12	BIT #2	1012, 0812	"						X
13	BIT #3	1013, 0813	"						X
14	BIT #4	1014, 0814	"						X
15	BIT #5	1015, 0815	"						X
16	BIT #6	1016, 0816	"						X
17	BIT #7	1917, 0817	"						X
18	BIT #8	1018, 0818	"						X
19	BIT #9	1019, 0819	"						X
20	BIT #10	1020, 0820	"						X
21	BIT #11	1021, 0821	"						X
22	BIT #12	1022, 0822	"						X
23	BIT #13	1023, 0823	"						X
24	BIT #14	1024, 0824	"						X
25	BIT #15	1025, 0825	"						X
26	BIT #16	1026, 0826	"						X
27	SER DATA OUT	1006	wh/ylw		X				
28	<b>GATED CLK</b>	<sup>1117</sup> 1008, 0501, 1207	wh/blu		X				
29	Q 16	1002	red		X				X
30	Q. MEM. q1								
31	Q. MEM. q2								
32	START DIG	1003	brn						
33	A/S RESET	1133	ylw/wh						
34	+12V	0632, 1034	red	X					
35	COMMON	0616, 1035	blk	X					

Fig. 5.1.10

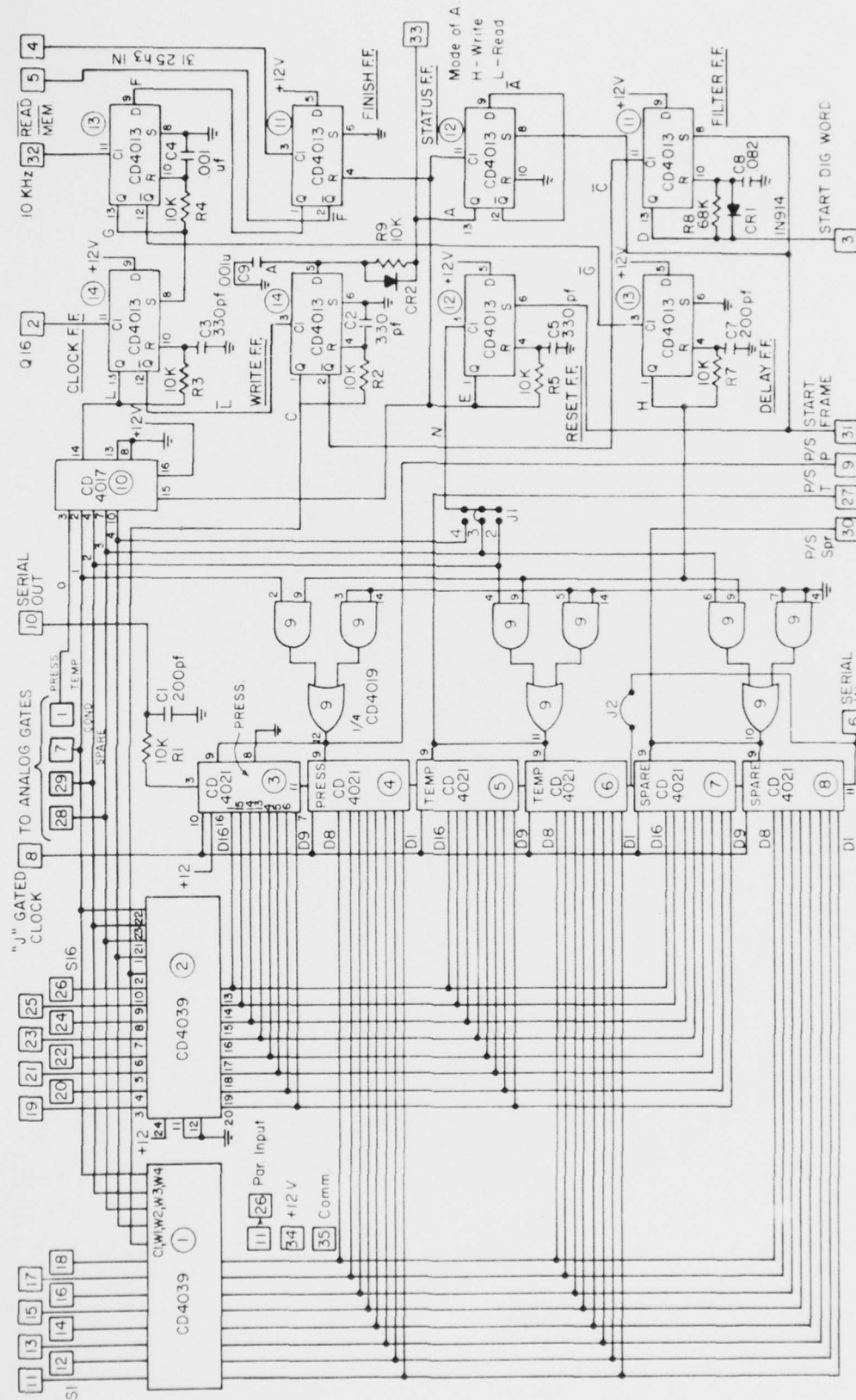


Fig. 5.1.10(2)

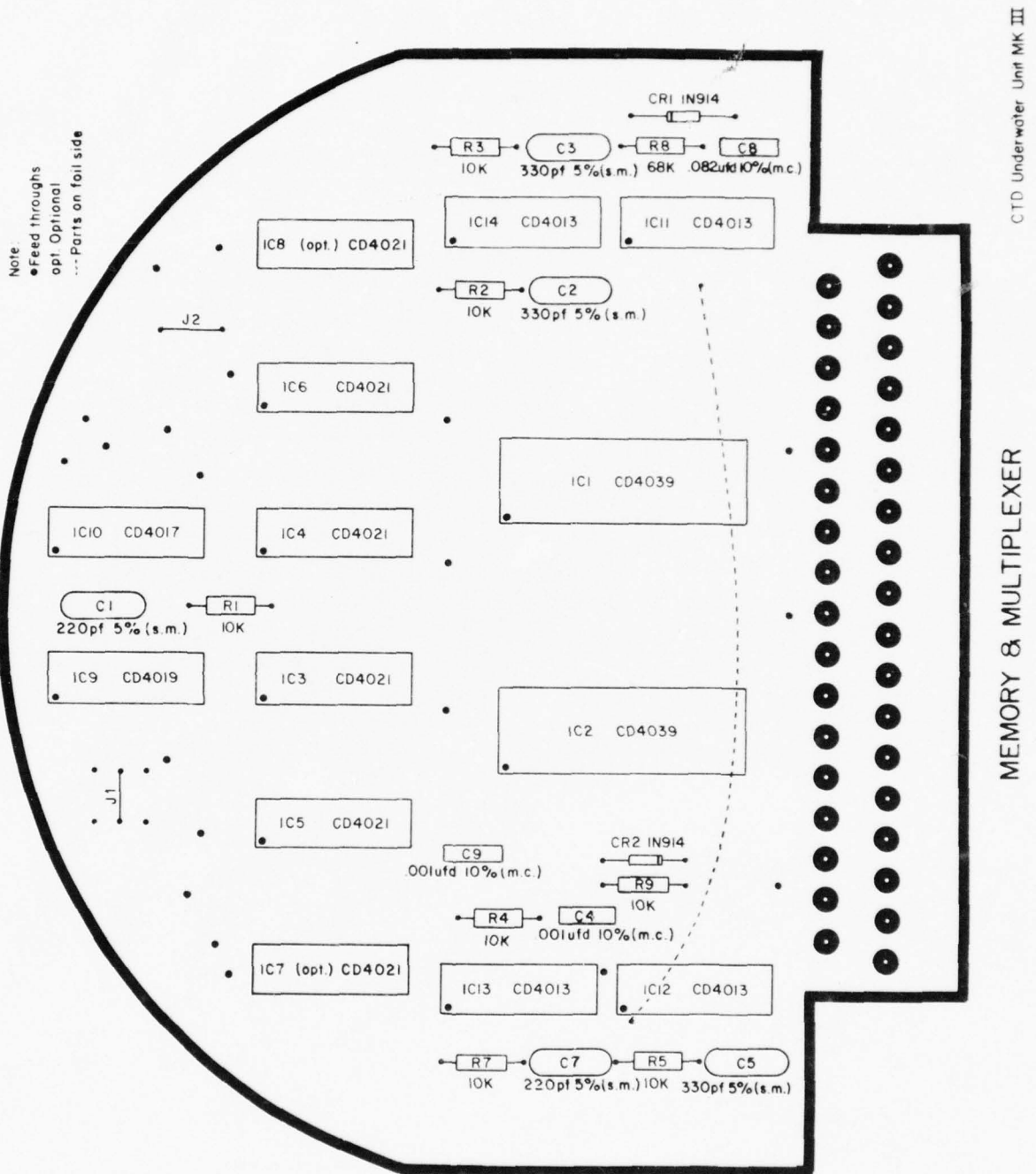


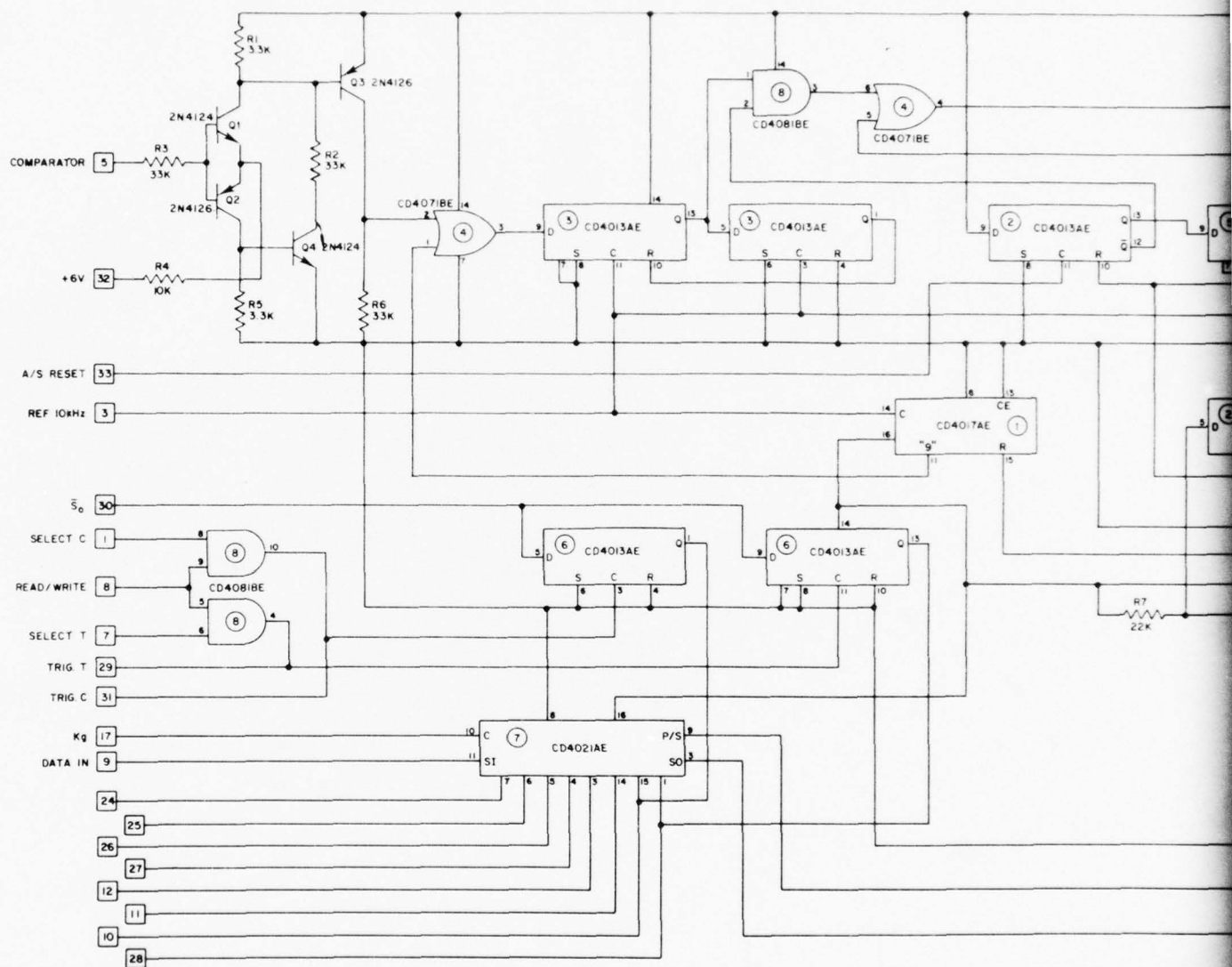


Fig. 5.1.10(3)

Board Title MEM + MULT.Board Number 10

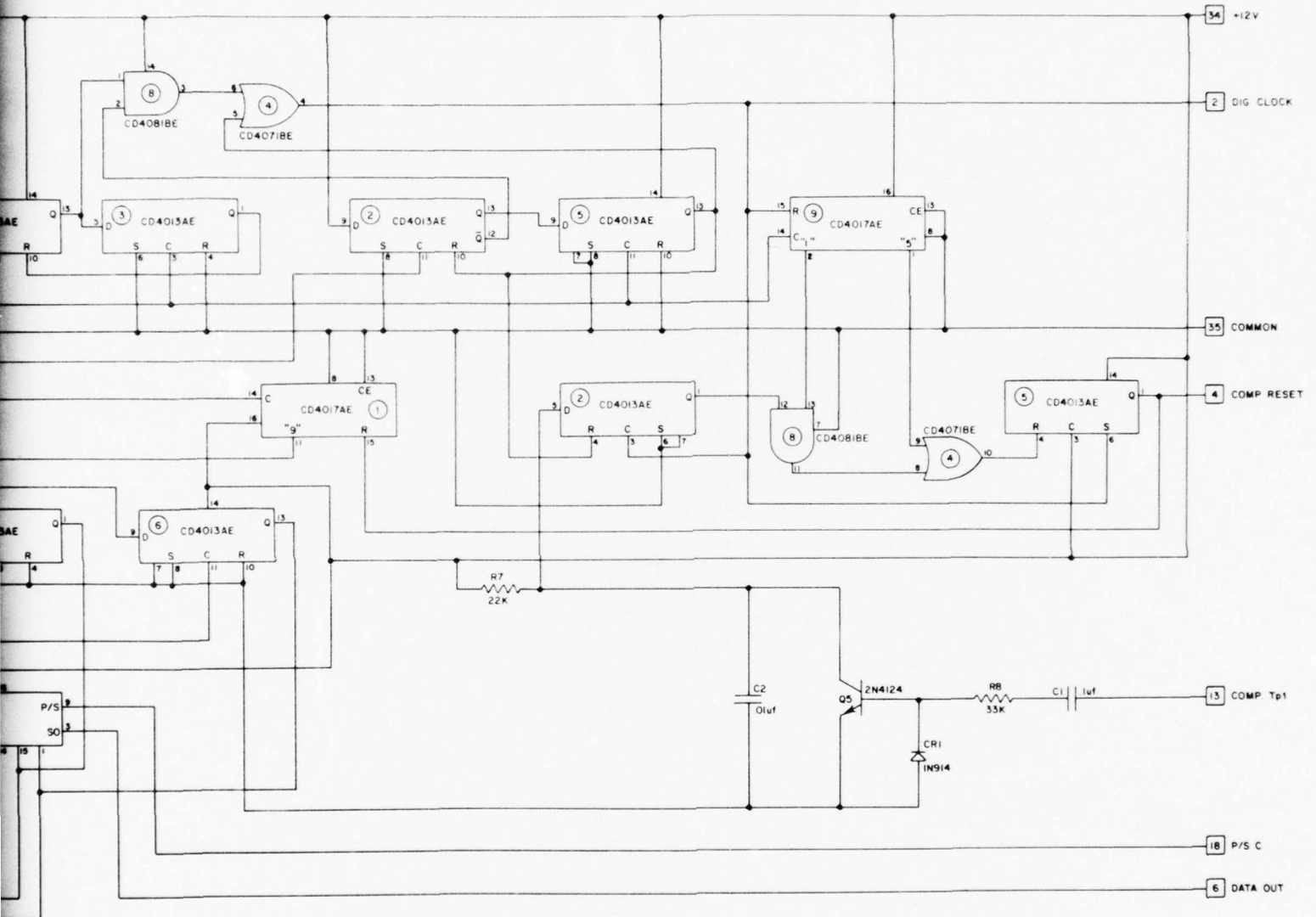
Pin ✱	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1	SELECT P	0112	wh/ylw		X				X
2	Q 16	0929	red		X				
3	START DIG W	0932	brn		X				X
4	FRAME CLK	1303	wh/orn		X				
5	READ MEM.	1209	grn		X				
6	SER. DATA IN	0927	wh/ylw		X				
7	SELECT T.	1107, 0218	wh/blk		X				X
8	GATED CLK.	0928, 1207 0501, 1117	wh/blu		X				
9	P/S P.				X				X
10	SER. DATA OUT	1208	ylw		X				
11	BIT #1	0911	red						
12	BIT #2	0912	red						
13	BIT #3	0913	red						
14	BIT #4	0914	red						
15	BIT #5	0915	red						
16	BIT #6	0916	red						
17	BIT #7	0917	red						
18	BIT #8	0918	red						
19	BIT #9	0919	red						
20	BIT #10	0920	red						
21	BIT #11	0921	red						
22	BIT #12	0922	red						
23	BIT #13	0923	red						
24	BIT #14	0924	red						
25	BIT #15	0925	red						
26	BIT #16	0926	red						
27	P/S T.				X				X
28	SELECT SPARE				X				
29	SELECT C.	1101, 0411	wh		X				X
30	P/S SPARE				X				X
31	START FRAME	1216	blu		X				
32	REF. CHOP	1103, 1309, 0322	gra		X				
33	READ/WRITE	1108	vio		X				X
34	+12V	1134	red	X					
35	COMMON	0935	blk	X					

NBIS



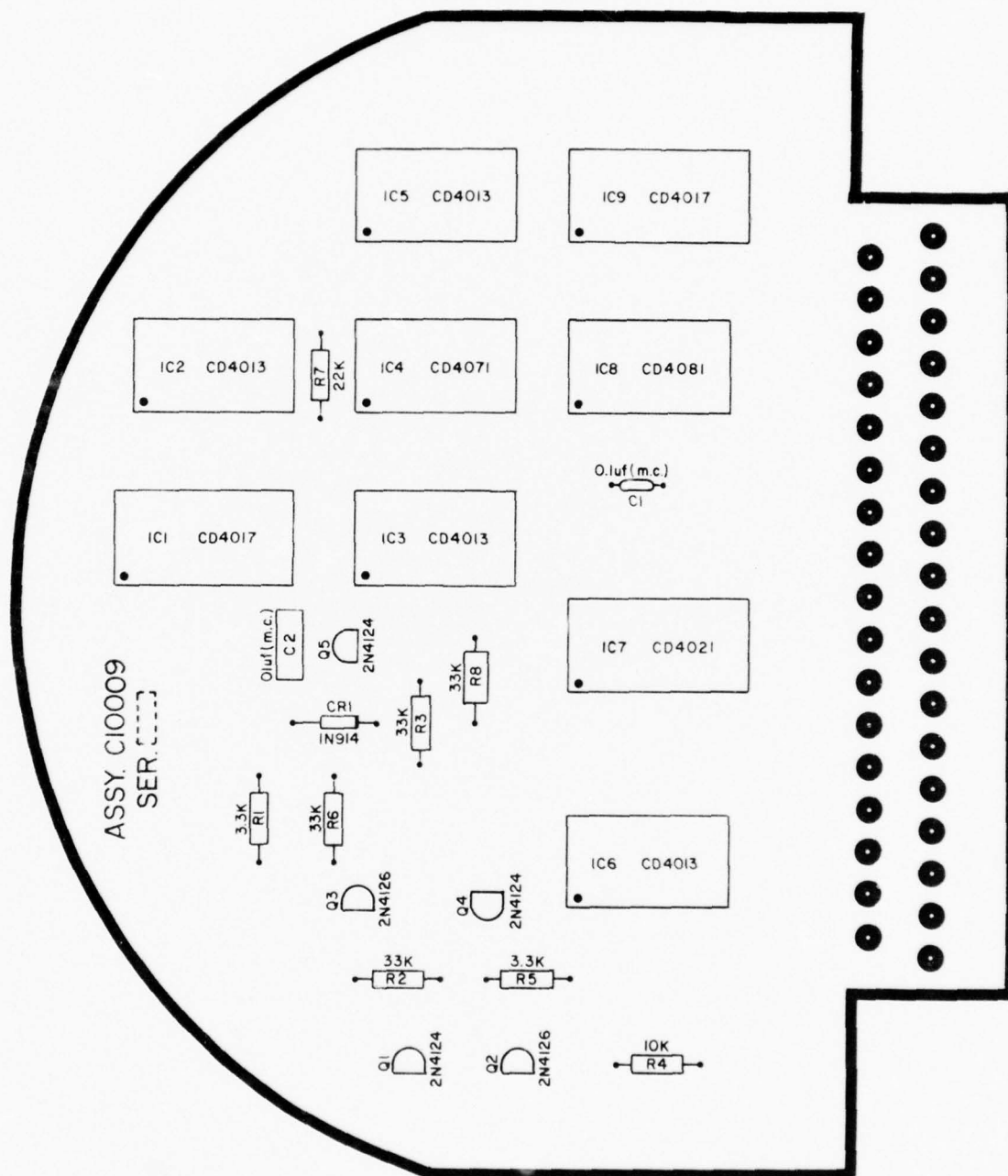
CTD UNDERWATER UNIT MK III ADAPTIVE SAM

Fig. 5.1.11



2

Fig. 5.1.11(2)



ADAPTIVE SAMPLING

CTD Underwater Unit

Fig. 5.1.11(3)

Board Title ADAPT. SAMP.Board Number 11

Pin #	Function	Connected To	Color	Harness Posn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1	SELECT C.	1029, 0411	wh		X				
2	DIGI. CLOCK	0902	wh/grn		X				X
3	REF CHOP	1032, 0322, 1309	gra		X				
4	COMP. RESET	0724	grn		X				X
5	COMP. O/P	0719, 0905	blu		X				
6	SER. DATA OUT	0908	gra		X				
7	SELECT T.	1007, 0218	wh/blk		X				
8	READ/WRITE	1033	vio		X				X
9	SER. DATA IN	0514, 0502	ylw		X				
10	T. SIGN BIT								
11	SPARE I/P	0509	gra						
12	SPARE I/P	1124	blk						
13	COMP. T.P.#1	0713	wh/blu		X				
14									
15									
16									
17	GATED CLK.	0501, 0928 1207, 1008	wh/blu		X				
18	PARALLEL SHIFT	0910, 1210	wh/brn		X				
19									
20									
21									
22									
23									
24	SPARE I/P	1112, 1125	blk						
25	SPARE I/P	1124, 1126	blk						
26	SPARE I/P	1125, 1127	blk						
27	SPARE I/P	1126, 1135	blk						
28	PRESS. SIGN BIT								
29									
30	$\overline{S_0}$	0904, 0113, 0217	grn		X				
31									
32	+6V	0625	orn	X			1134, 1135		
33	A/S RESET	0933	ylw/wh		X				
34	+12V	1234		X			1132, 1135		
35	COMMON	1127, 1035		X			1132, 1134		



Fig. 5.1.12

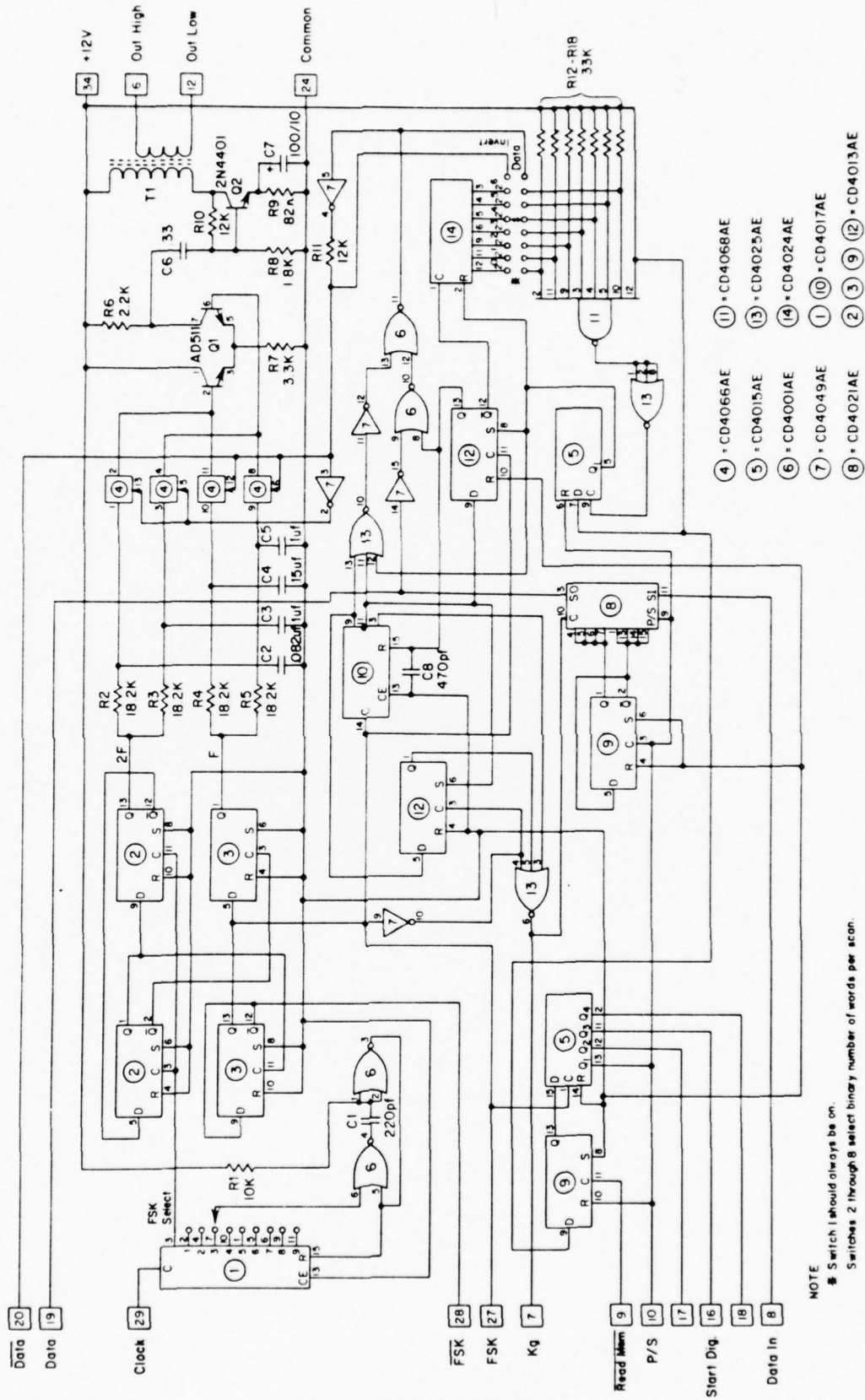
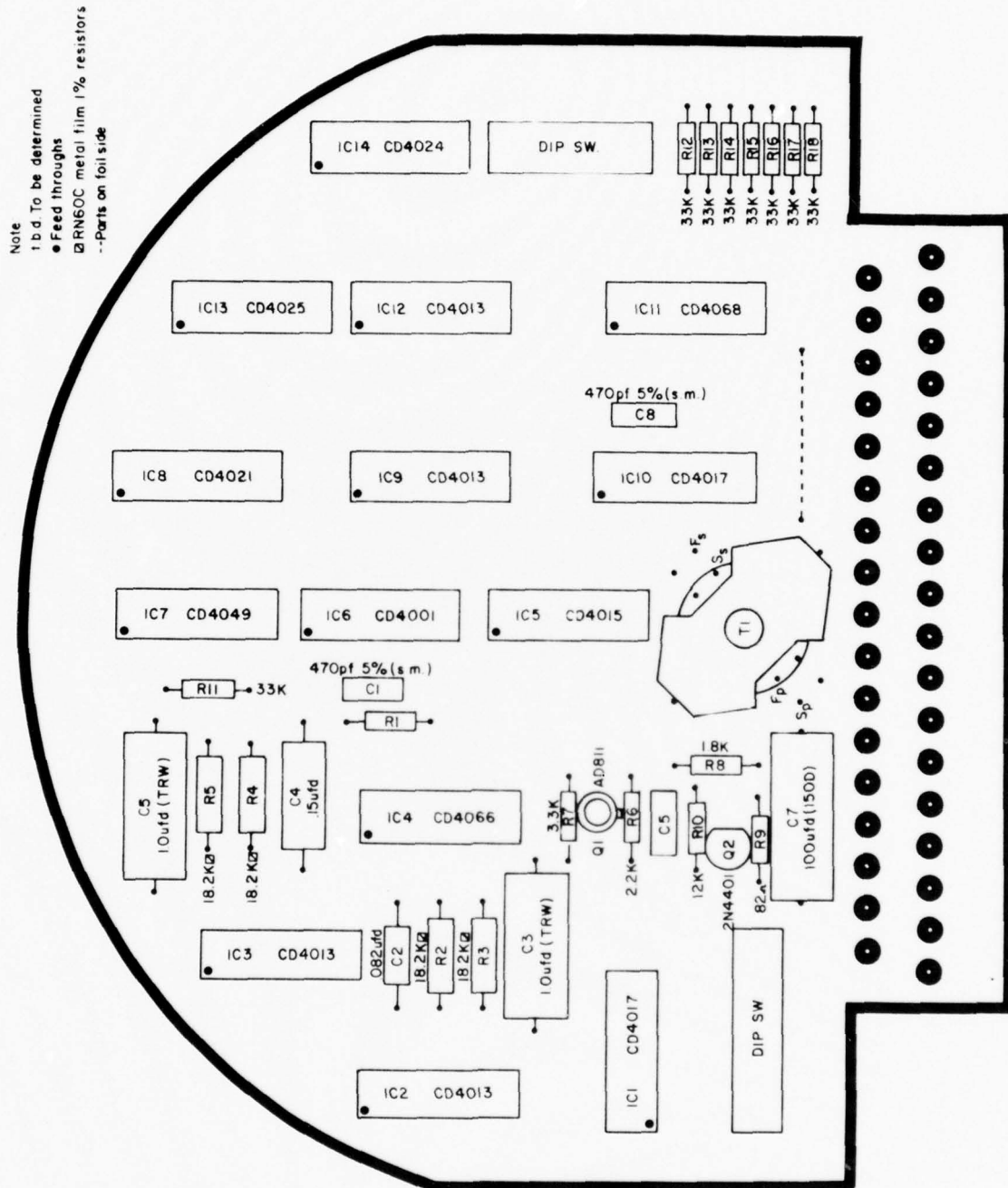


Fig. 5.1.12(2)



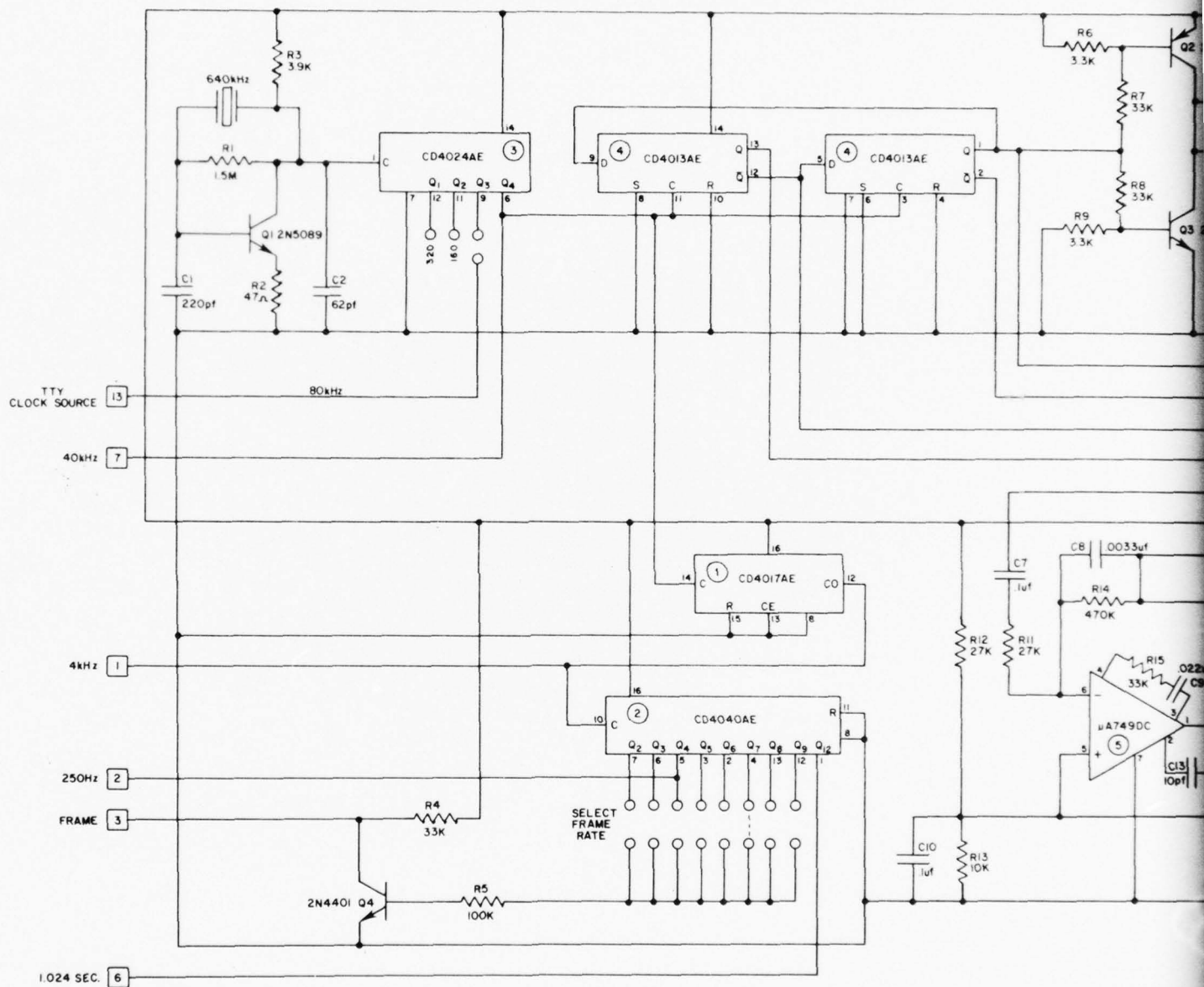
CTD Underwater Unit MK III

TTY FORMATTER & FSK MODULATOR

Fig. 5.1.12(3)

Board Title TTY-FSKBoard Number 12

Pin #	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1									
2									
3									
4									
5									
6	FSK HI	End Cap					1212		
7	GATED CLK.	1117, 1008, 0501, 0928	wh/blu		X				X
8	DATA IN	1010	ylw		X				
9	READ MEM	1005	grn		X				
10	P/S	0910, 1118	wh/brn		X				X
11									
12	FSK LO	End Cap					1206		
13									
14									
15									
16	START DIG.	1031	blu						X
17	Q2 SPARE								
18	Q4 SPARE								
19	DATA								
20	DATA								
21									
22									
23									
24									
25									
26									
27	FSK CLK								
28	FSK CLK								
29	FREQ INPUT	1313, 0503	brn		X				
30									
31									
32									
33	COMMON	1235	link						
34	+12V	1134	red	X			1235		
35	COMMON	1135, 1233	blk	X			1234		



CTD UNDERWATER UNIT MK III SIGNAL GENERA

Fig. 5.1.13

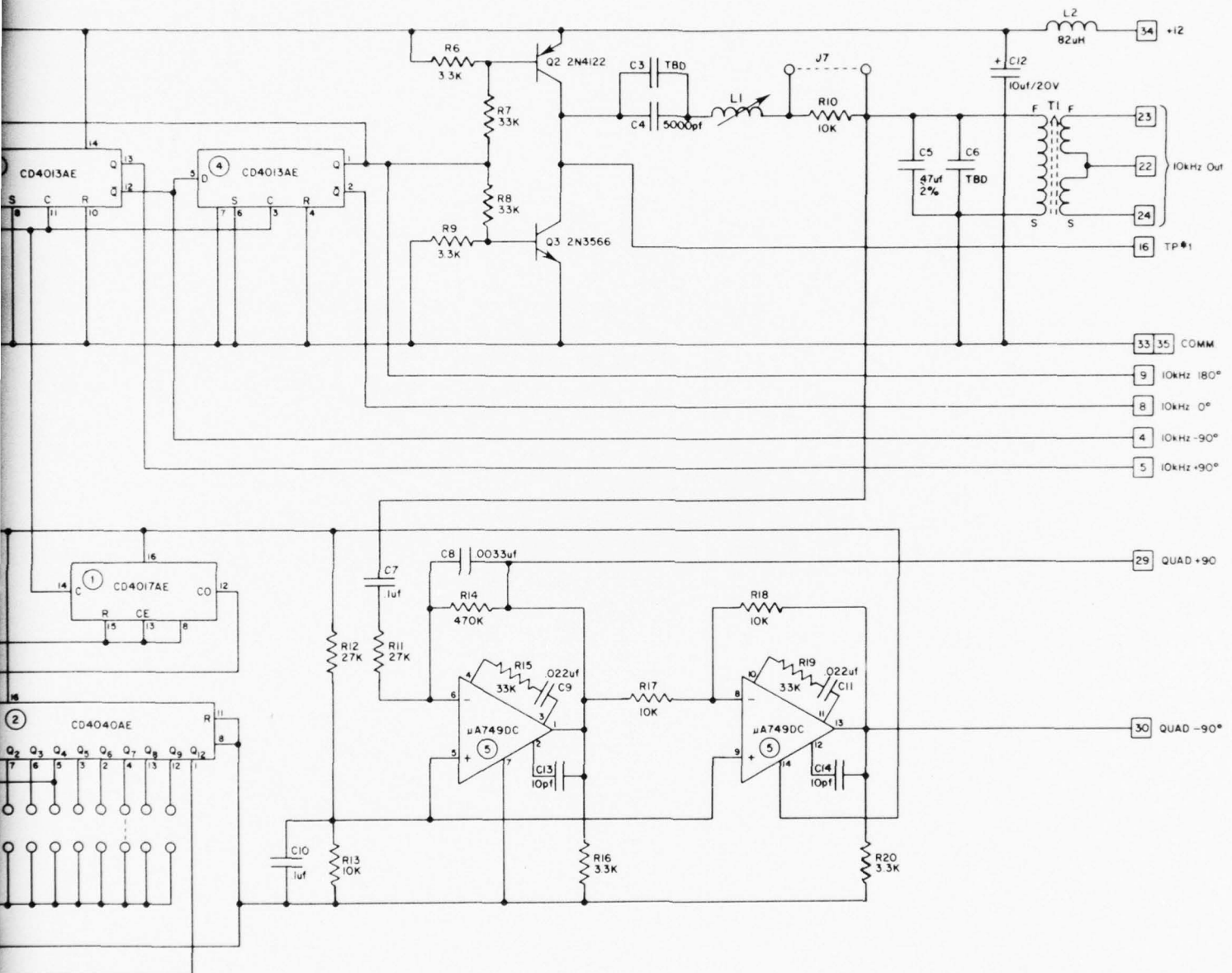




Fig. 5.1.13(2)

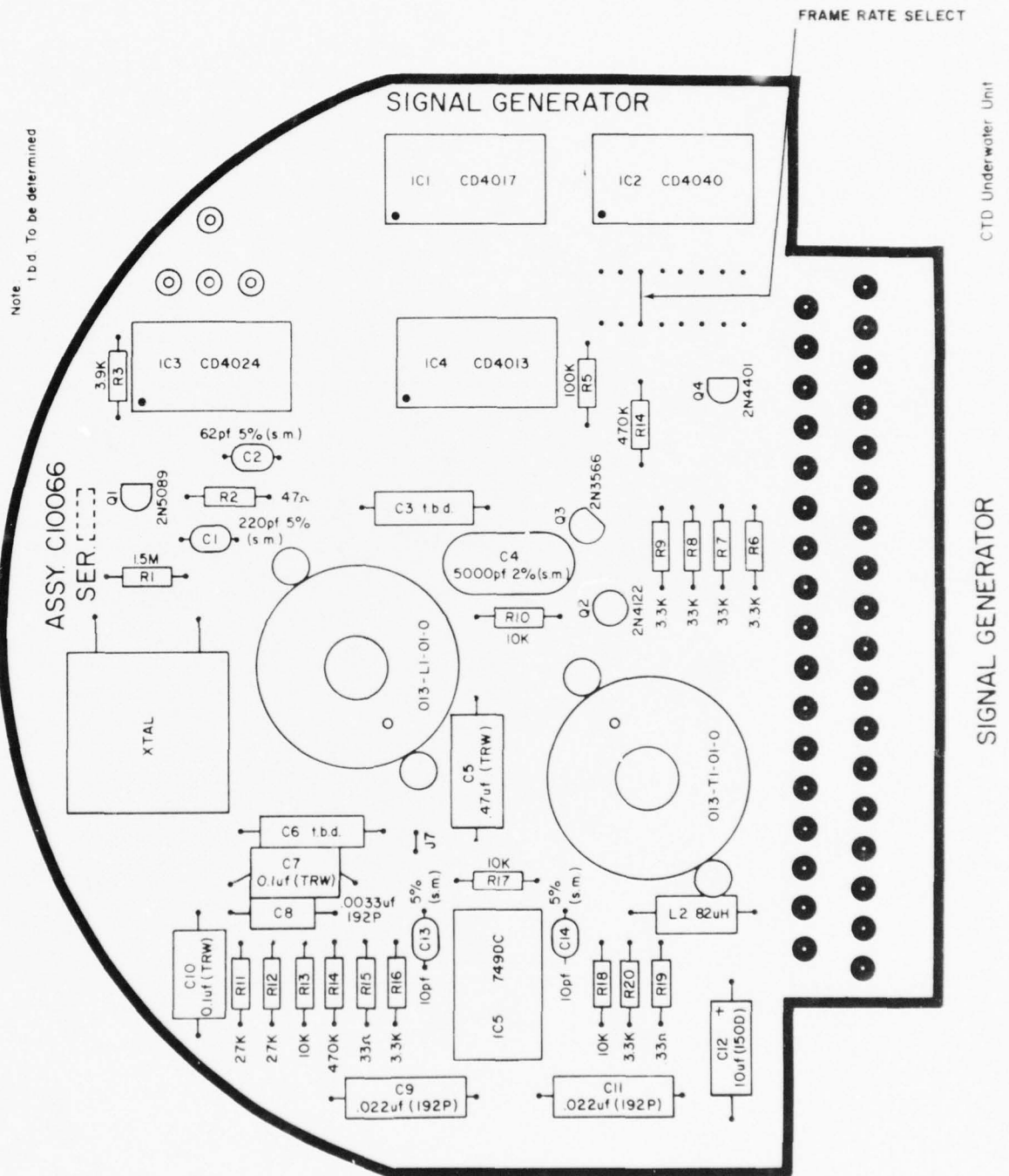


Fig. 5.1.13(3)

Board Title SIG. GEN.Board Number 13

Pin #	Function	Connected To	Color	Harness Postn.			Twisted With	Shielded & Twisted Pair With	Source
				L	C	R			
1	4Khz	0526	wh		X				X
2	250 hz	0518	wh/vio		X				X
3	FRAME CLOCK	1004	wh/grn		X				X
4	QUAD CHOP	0728	grn		X		1308		X
5	QUAD CHOP				X				X
6	1.024 SEC.	0508	gra						
7	40 Khz								
8	REF CHOP	0722, 0320			X		1304, 1309		X
9	REF CHOP	0322, 1103, 1032	gra		X				X
10	COMP. RESET								X
11									
12									
13	160 Khz/80 Khz	1229	grn		X				X
14									
15									
16	T.P. #1								
17									
18									
19									
20									
21									
22	O/P SINE C.T.	0133, 0131, 0135	blk			X			X
23	REF SINE	0215, 0130, 0802 0401, 0308	wh/red			X			X
24	REF SINE	0214, 0129, 0801 0403, 0309	wh/blk			X			X
25									
26									
27									
28									
29	QUAD SINE	0729	orn			X			X
30	QUAD SINE	0731	wh			X			X
31									
32									
33	COMMON	1335	link						
34	+12V	0634	red				1335		
35	COMMON	0618, 1333	blk				1334		

# Circuit Board

## Bendix Connector

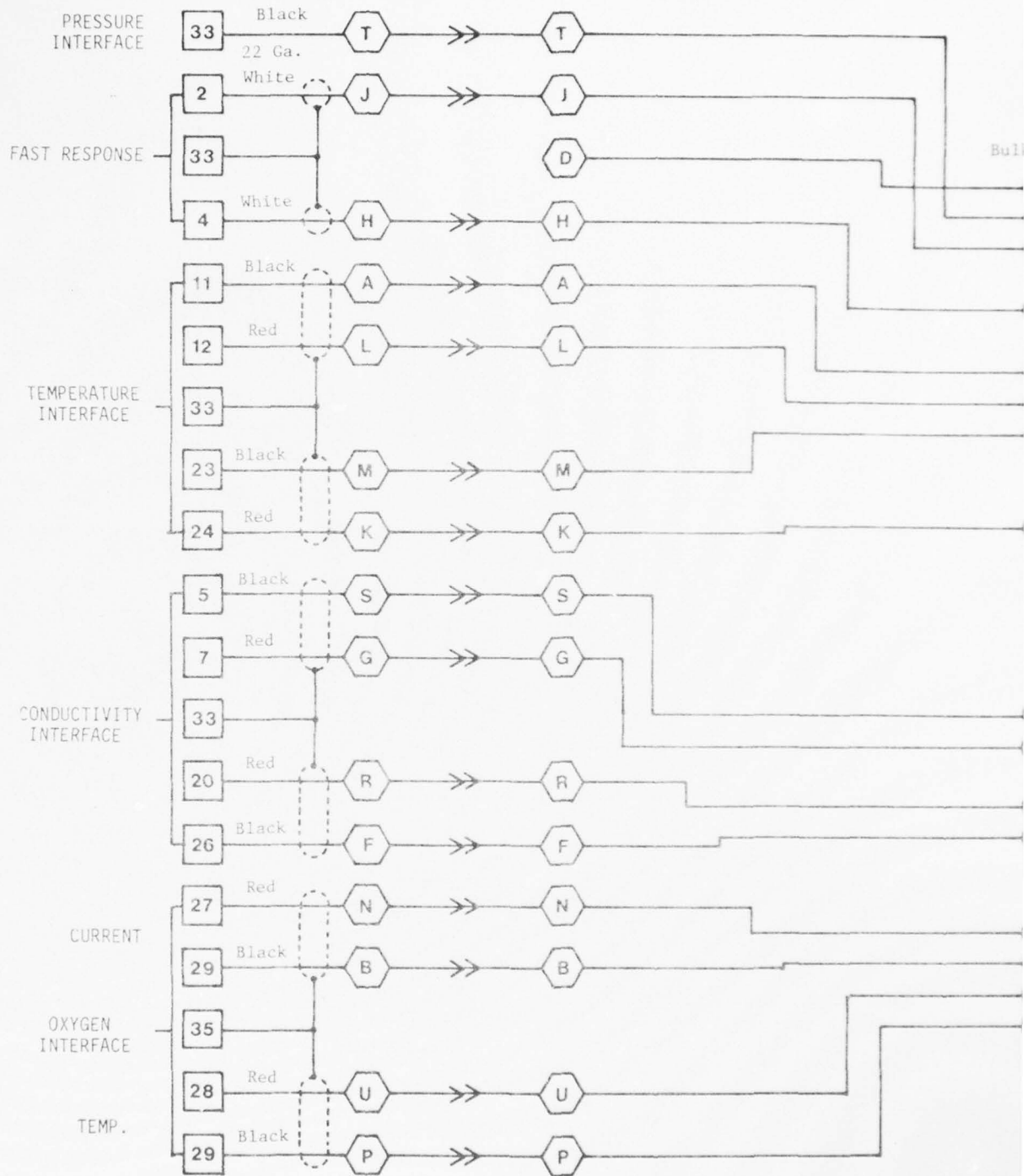
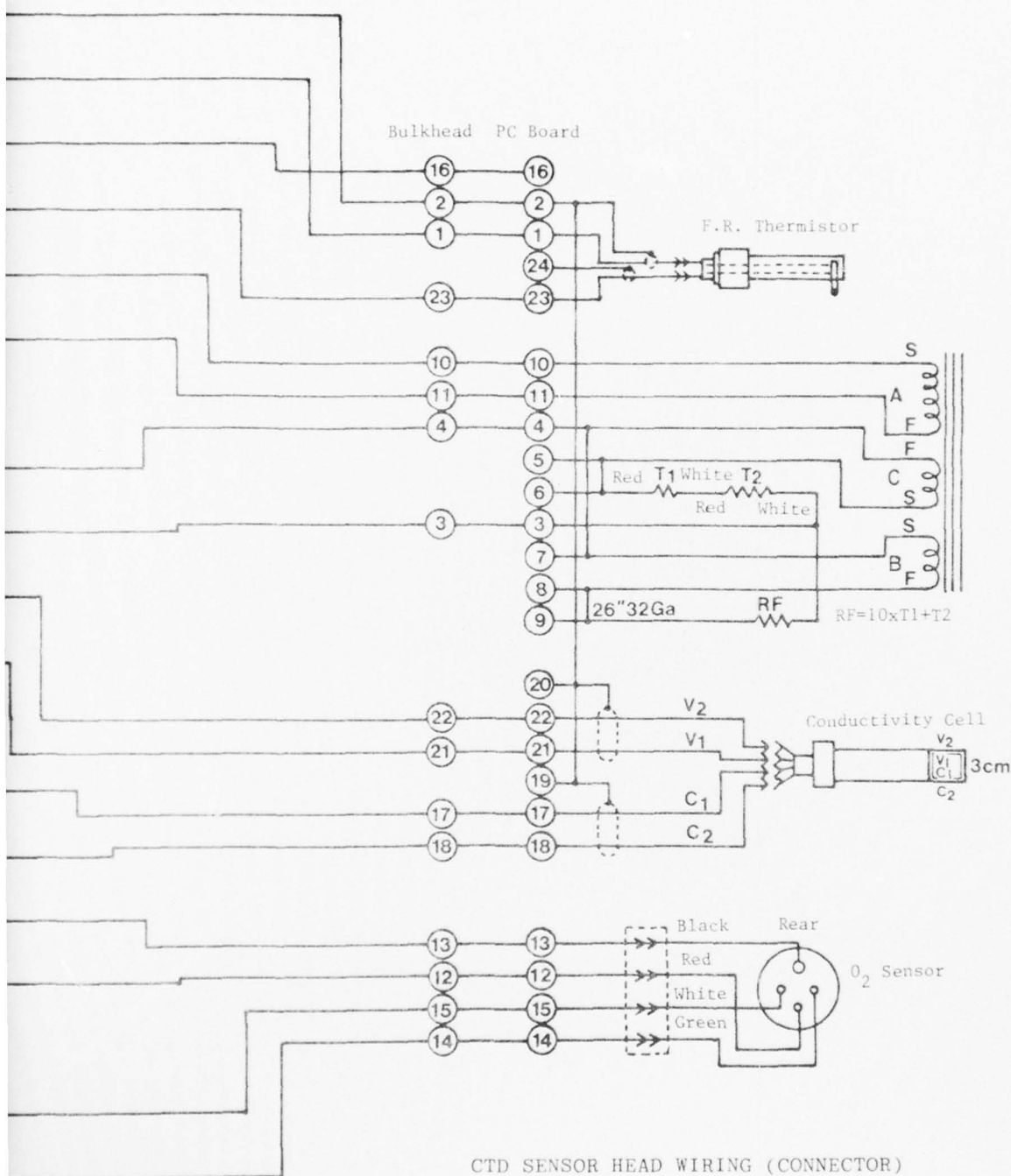
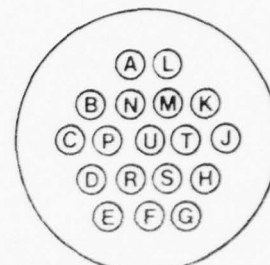


Fig. 5.1.14



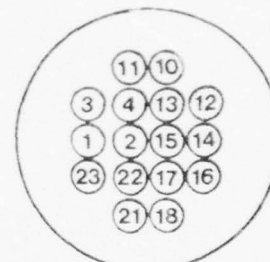
CTD SENSOR HEAD WIRING (CONNECTOR)

BENDIX



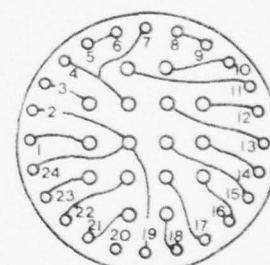
TOP VIEW

BULKHEAD



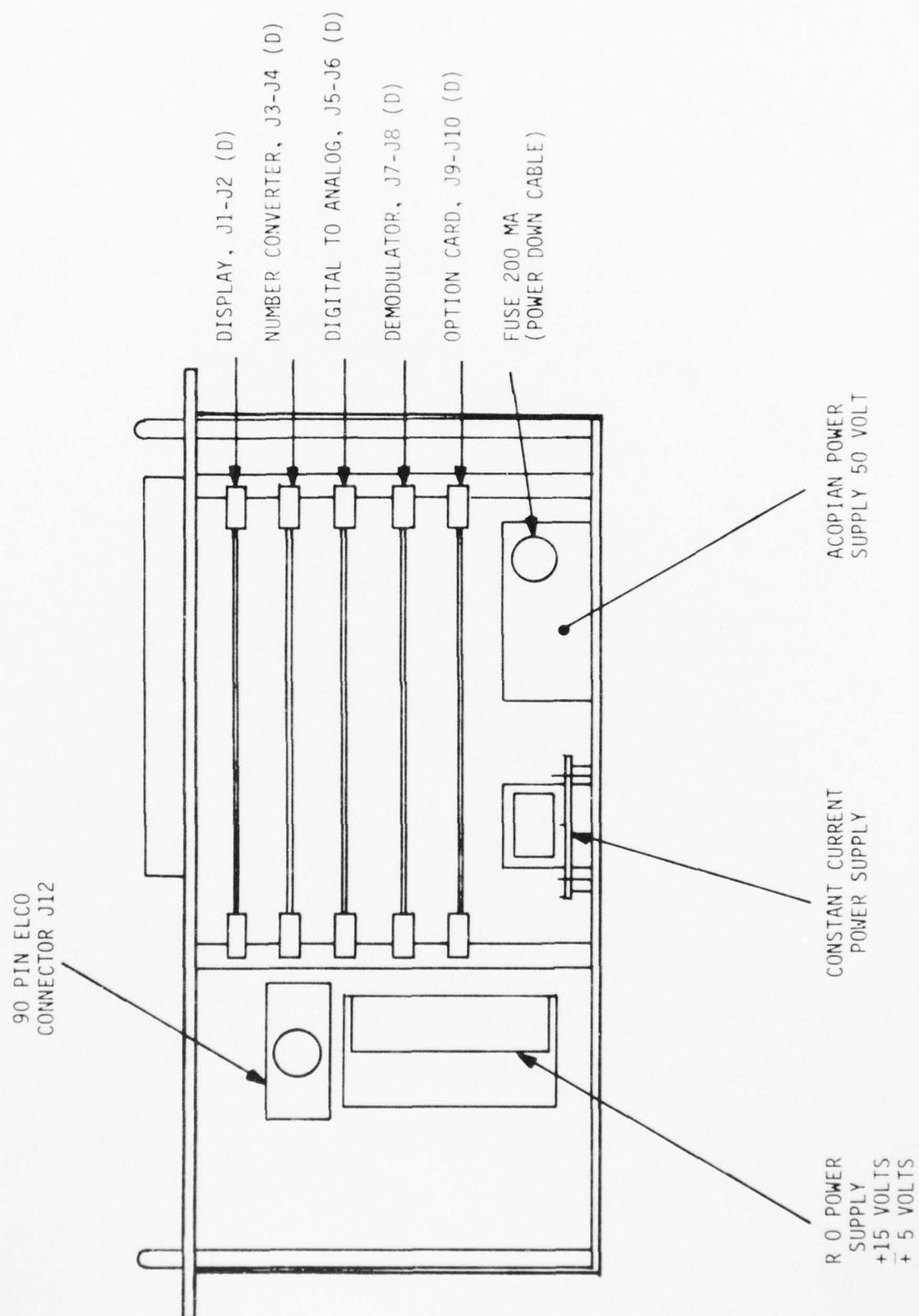
BOTTOM VIEW

PC BOARD



BOTTOM VIEW

Fig. 5.2



DECK DATA TERMINAL CHASSIS



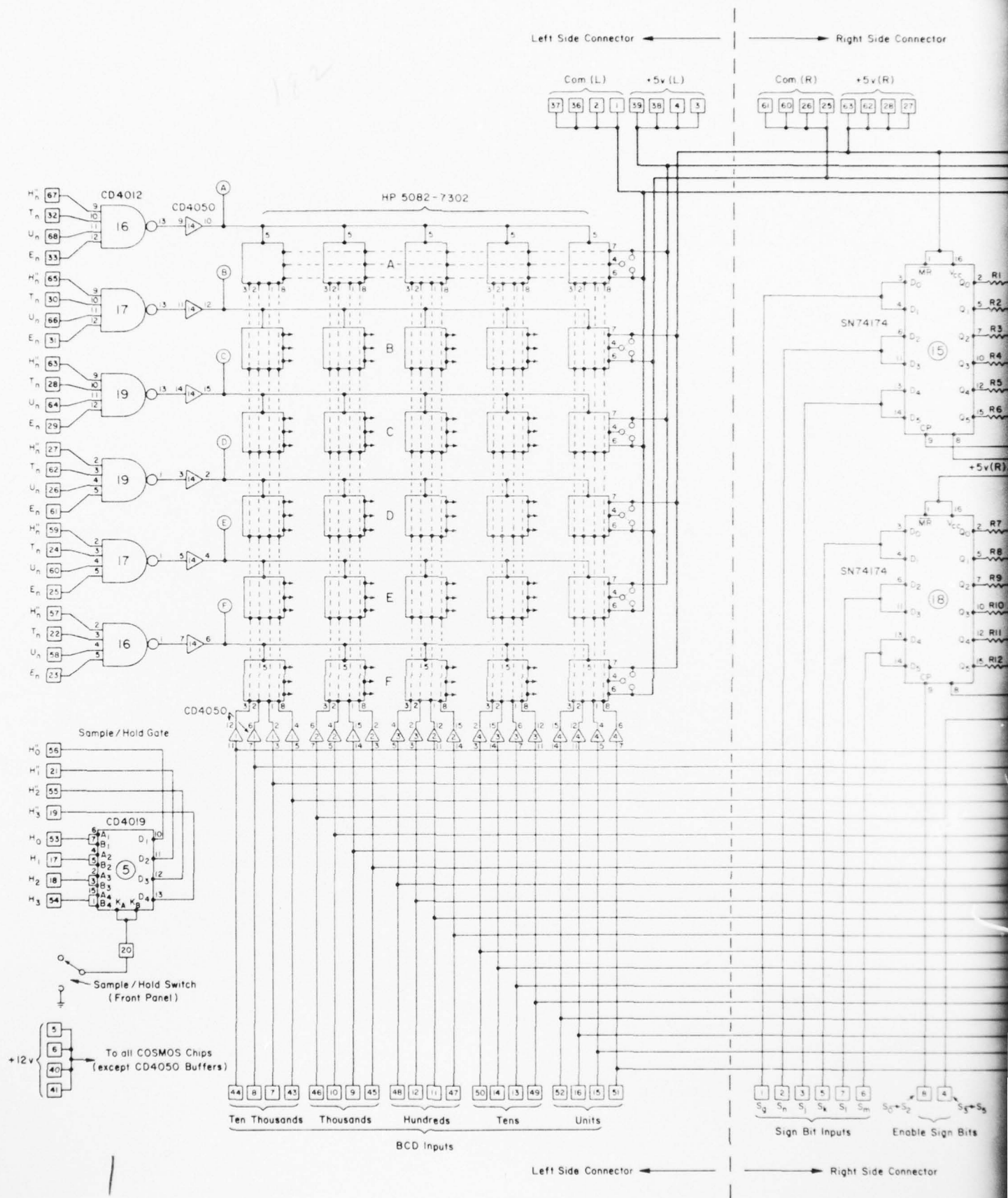
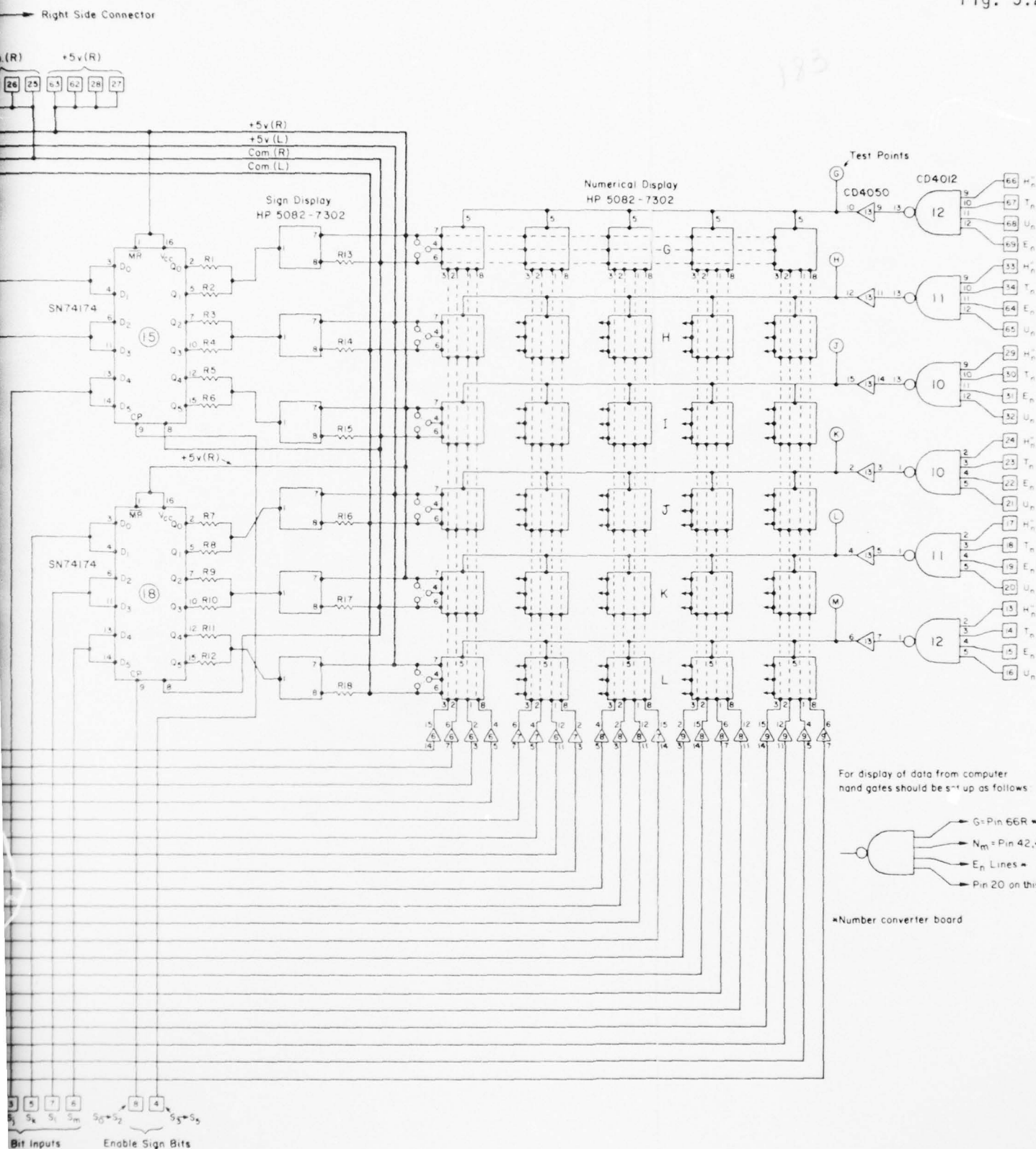


Fig. 5.2.1



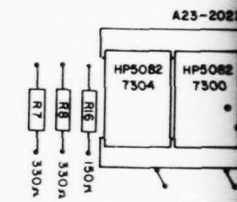
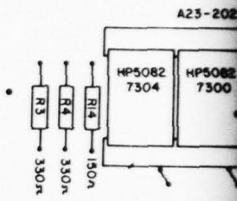
CTD DECK UNIT MK III  
DISPLAY

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① ② ③ ④ ⑤ ⑥

NBIS inc P/N 016-PC-02-1



IC15 SN74174

IC18 SN74174

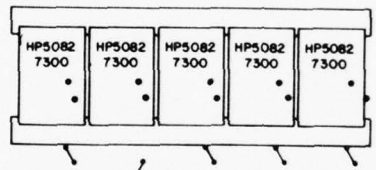
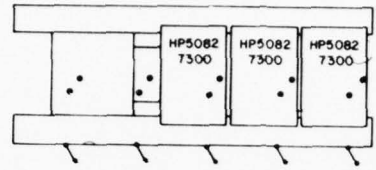
IC6 CD4050

IC14 CD4050

Optional  
IC16 CD4012

IC17 CD4012

IC19 CD4012



IC5 CD4019

IC4 CD4050

IC3 CD4050

IC2 CD4050

IC1 CD4050

CTD Deck Unit MK III

Fig. 5.2.1(2)

NBIS inc. P/N 016-PC-02-1

IC14 CD4050

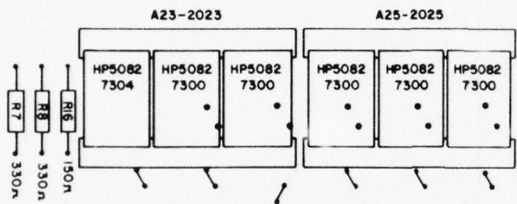
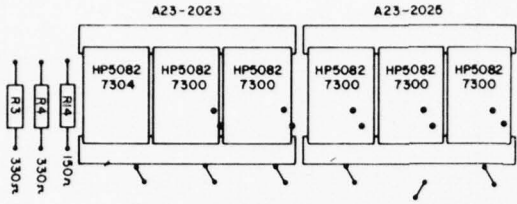
Optional  
IC16 CD4012

IC17 CD4012

IC19 CD4012

IC15 SN74174

IC18 SN74174



IC6 CD4050  
IC7 CD4050  
IC8 CD4050  
IC9 CD4050

IC13 CD4050

Optional  
IC12 CD4012

IC11 CD4012

IC10 CD4012

Note  
● Feed throughs  
--- Parts on foil side

CTD Deck Unit MK III

DISPLAY

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Pin Num	Function	Demod J7 and J8	Num Conv J3 and J4	D/A J5 and J6	Display J1 and J2	Comp I/O (J11)	Internal I/O J12	Pin Num	Function	Demod J7 and J8	Num Conv J3 and J4	D/A J5 and J6	Display J1 and J2	Comp I/O (J11)	Internal I/O J12
1L	Common from Buss				2L, 36L			1R	Sign Bit Input DisplayG						
2L	Common from Buss				1L, 58L			2R	Sign Bit Input DisplayH	38R					
3L	+5V INPUT from Buss				4L, 38L			3R	Sign Bit Input DisplayJ						
4L	+5V INPUT from Buss				3L			4R	Enable S <sub>1</sub> , S <sub>2</sub> Input	51R			8R		
5L	+12V INPUT from Buss				6L			5R	Sign Bit Input DisplayK	26L					
6L	+12V INPUT from Buss				5L, 40L			6R	Sign Bit Input DisplayM						
7L	BCD Input 10 <sup>4</sup> (2)		47R					7R	Sign Bit Input DisplayL						
8L	BCD Input 10 <sup>4</sup> (4)		46R					8R	Enable S <sub>3</sub> , S <sub>4</sub> , S <sub>5</sub> Input			4R			
9L	BCD Input 10 <sup>3</sup> (2)		51R					9R							
10L	BCD Input 10 <sup>3</sup> (4)		50R					10R							
11L	BCD Input 10 <sup>2</sup> (2)		55R					11R							
12L	BCD Input 10 <sup>2</sup> (4)		54R					12R							
13L	BCD Input 10 <sup>1</sup> (2)		59R					13R	Hundreds Count DisplayM						
14L	BCD Input 10 <sup>1</sup> (4)		58R					14R	Tens Count Display M				14R, 26R		
15L	BCD Input 10 <sup>0</sup> (2)		63R					15R	Units Count Display M				13R, 15R		
16L	BCD Input 10 <sup>0</sup> (4)		62R					16R	Enable Display M				14R, 16R		
17L	Hundreds Count H <sub>1</sub> , IN	67L						17R	Hundreds Count DisplayL				15R, 17R		
18L	Hundreds Count H <sub>2</sub> , IN	68L						18R	Tens Count DisplayL				16R, 18R		
19L	Hundreds Count H <sub>1</sub> , OUT							19R	Units Count Display L				17R, 19R		
20L	C.T. Sample Hold Switch							20R	Enable Display L				18R, 20R		
21L	Hundreds Count H <sub>1</sub> , OUT						AZ	21R	Enable Display K		39R		19R, 29R		
22L	Tens Count Display F				23L, 57L			22R	Units Count Display K	47L					
23L	Enable Display F				22L, 25L			23R	Tens Count Display K	51L					
24L	Tens Count Display E				25L, 59L			24R	Hundreds Count Display K				56L		
25L	Enable Display E				24L, 23L			25R	Common				26R, 60R		
26L	Units Count Display D	20L			56L			26R	Common				25R, 17R		
27L	Hundreds Count Display D				27L			27R	+5V INPUT				28R, 62R		
28L	Tens Count Display C				29L, 63L			28R	+5V INPUT				27R		
29L	Enable Display C				28L, 33L			29R	Hundreds Count DisplayJ				20R, 30R		
30L	Tens Count Display B	52L						30R	Tens Count Display J				29R, 31R		
31L	Enable Display B		36R					31R	Units Count Display J				30R, 32R		
32L	Tens Count Display A				33L, 67L			32R	Enable Display J				31R, 66R		
33L	Enable Display A				32L, 29L			33R	Hundreds Count DisplayH				56L		
34L								34R	Tens Count Display H	55L					
35L								35R							
36L	Common				37L, 11L			36R							
37L	Common							37R							
38L	+5V Input				39L, 31L			38R							
39L	+5V Input				38L			39R							
40L	+12V Input				41L			40R							
41L	+12V Input				40L, 51L			41R							
42L								42R							
43L	BCD Input 10 <sup>4</sup> (1)		44R					43R							
44L	BCD Input 10 <sup>4</sup> (8)		45R					44R							
45L	BCD Input 10 <sup>3</sup> (1)		48R					45R							
46L	BCD Input 10 <sup>3</sup> (8)		49R					46R							



Fig. 5.2.1(3)

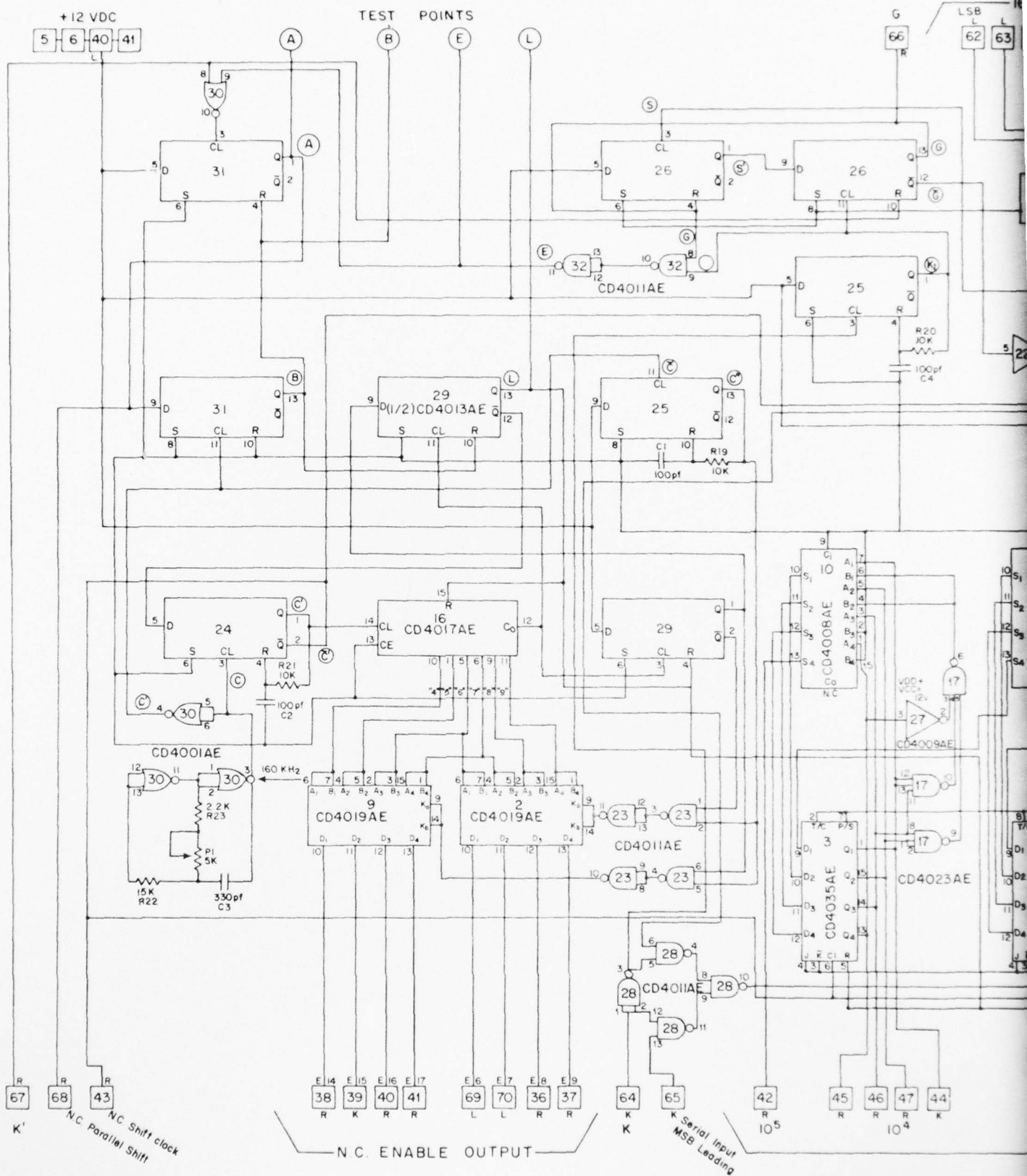
42L	Tens Count Display F	23L, 50L	42R	Units Count Display K	41L	51L	56L
23L	Enable Display F	22L, 25L	23R	Tens Count Display K			
24L	Tens Count Display E	25L, 59L	24R	Hundreds Count Display K			56L
25L	Enable Display E	24L, 23L	25R	Common			56R, 60R
26L	Units Count Display D	20L	26R	Common			55R, 11R
27L	Hundreds Count Display D	56L	27R	+5V INPUT			28R, 62R
28L	Tens Count Display C	29L, 63L	28R	+5V INPUT			27R,
29L	Enable Display C	28L, 33L	29R	Hundreds Count Display J			20R, 30R
30L	Tens Count Display B	52L	30R	Tens Count Display J			29R, 31R
31L	Enable Display B	36R	31R	Units Count Display J			30R, 32R
32L	Tens Count Display A		32R	Enable Display J			11R, 60R
33L	Enable Display A	33L, 67L	33R	Hundreds Count Display H			56L
34L		32L, 29L	34R	Tens Count Display H	55L		
35L	Common		35R				
36L	Common	37L, 11L	36R				
37L	Common		37R				
38L	+5V Input	39L, 31L	38R				
39L	+5V Input	38L	39R				
40L	+12V Input	41L	40R				
41L	+12V Input	40L, 51L	41R				
42L			42R				
43L	BCD Input 10 <sup>4</sup> (1)		43R				
44L	BCD Input 10 <sup>4</sup> (8)		44R				
45L	BCD Input 10 <sup>3</sup> (1)		45R				
46L	BCD Input 10 <sup>3</sup> (8)		46R				
47L	BCD Input 10 <sup>2</sup> (1)		47R				
48L	BCD Input 10 <sup>2</sup> (8)		48R				
49L	BCD Input 10 <sup>1</sup> (1)		49R				
50L	BCD Input 10 <sup>1</sup> (8)		50R				
51L	BCD Input 10 <sup>0</sup> (1)		51R				
52L	BCD Input 10 <sup>0</sup> (8)		52R				
53L	Hundreds Count H <sub>9</sub> , IN	66L	53R				
54L	Hundreds Count H <sub>3</sub> , IN	69L	54R				
55L	Hundreds Count H <sub>2</sub> , OUT		55R				
56L	Hundreds Count H <sub>9</sub> , OUT	27L, 63L 33R, 24R	56R				
57L	Hundreds Count Display F	58L, 22L	57R				
58L	Units Count Display F	57L, 21L	58R				
59L	Hundreds Count Display E	60L, 24L	59R				
60L	Units Count Display E	59L, 64L	60R	Common			61R, 25R
61L	Enable Display D	40R	61R	Common			60R
62L	Tens Count Display D	56L	62R	+5V INPUT			63R, 27R
63L	Hundreds Count Display C	64L, 28L	63R	+5V INPUT			62R
64L	Units Count Display C	63L, 60L	64R	Units Count Display H	19L		
65L	Hundreds Count Display B	56L	65R	Enable Display H			CE
66L	Units Count Display B	18L	66R	Hundreds Count Display G			32R, 67R
67L	Hundreds Count Display A	68L, 32L	67R	Tens Count Display G			66R, 68R
68L	Units Count Display A	67L	68R	Units Count Display G			67R, 69R
69L			69R	Enable Display G			
70L			70R				
Connector:			Connector:				
1			1				
2			2				
3			3				
4			4				
5			5				
6			6				
7			7				
8			8				
9			9				
10			10				
11			11				
12			12				
13			13				
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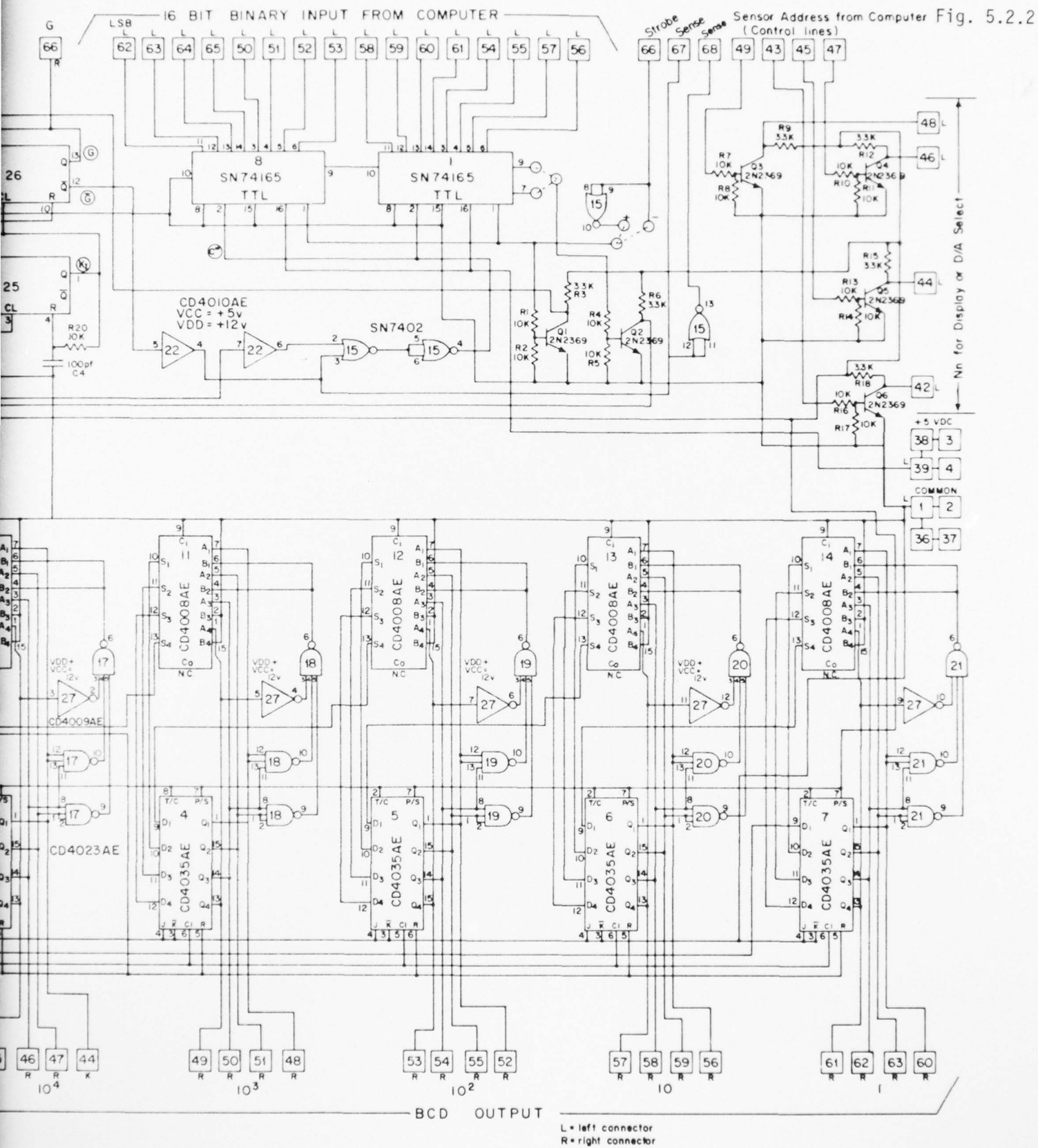
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Part Number: P/N 016-PC-02-0

Date:

2





CTD DECK UNIT MK III  
NUMBER CONVERTER

2

(E)

IC32 CD4011

IC26 CD4013

IC19 CD4023

IC12 CD4008

IC5 CD4035

(A)

C1 100pf (s.m.)

(B)

IC31 CD4013

IC25 CD4013

IC18 CD4023

IC11 CD4008

IC4 CD4035

P1 5K

R22 15K

R20 10K

C4 100pf (s.m.)

IC30 CD4001

IC24 CD4013

IC17 CD4023

IC10 CD4008

IC3 CD4035

R23 2.2K

R21 10K

C2 100pf (s.m.)

IC29 CD4013

IC23 CD4011

IC16 CD4017

IC9 CD4019

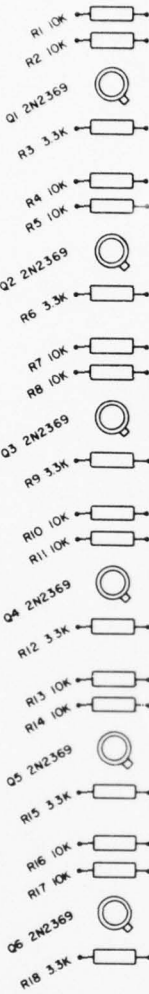
IC2 CD4019

IC22 CD4050

IC15 SN7402

IC8 SN74165

IC1 SN74165

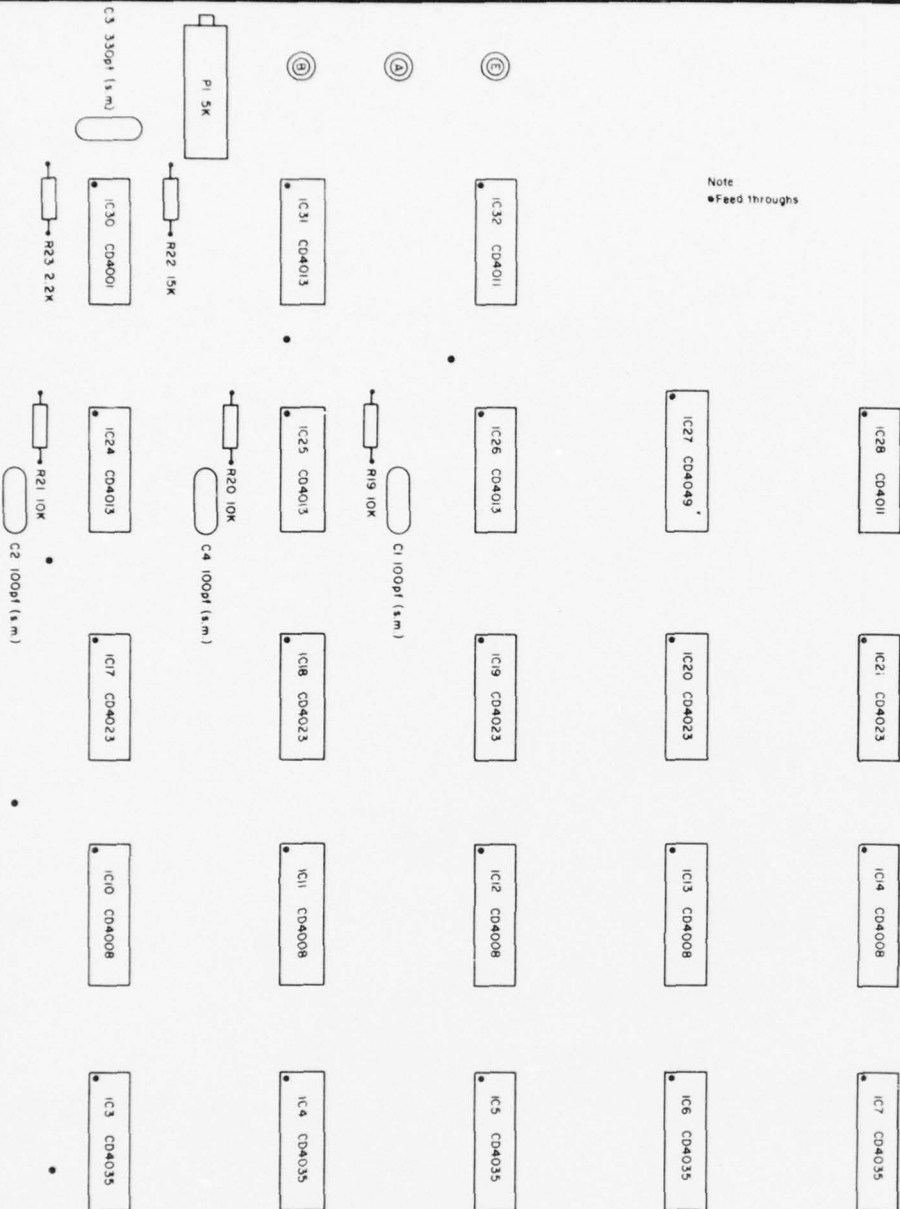


P/N 015-PC-02-1

CTD Deck Unit MK III

Fig. 5.2.2(2)

Note  
• Feed throughs







AD-A052 054

WOODS HOLE OCEANOGRAPHIC INSTITUTION MASS

F/G 8/10

W.H.O.I./BROWN CONDUCTIVITY, TEMPERATURE, AND DEPTH MICROPROFIL--ETC(U)

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N00014-66-C-0241

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3 OF 3

AD  
A052 054



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DATE  
FILMED  
5-78  
DDC

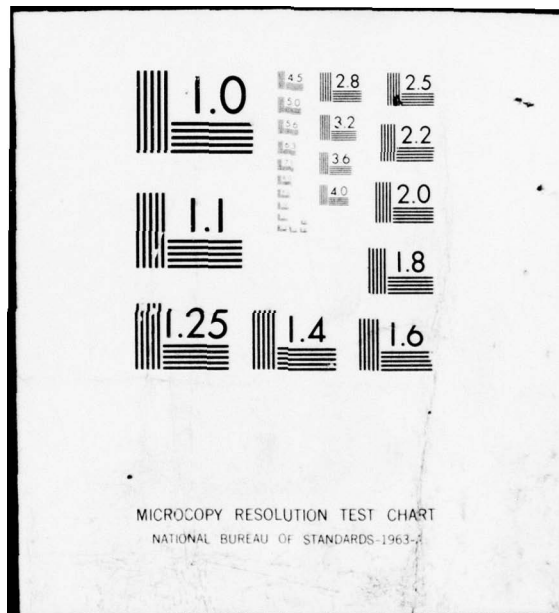


Fig. 5.2.2(3)

Pin Num.		Function		Demod. J7 and J8						Pin Num.		Function		Demod. J7 and J8											
				Num. Conv. J3 and J4		D/A J5 and J6		Display J1 and J2		Comp. I/O (J11)		Internal I/O J12				Num. Conv. J3 and J4		D/A J5 and J6		Display J1 and J2		Comp. I/O (J11)		Internal I/O J12	
1L	Common to Buss	2L, 36L										1R													
2L	Common to Buss	1L										2R													
3L	+5V Input from Buss	38L, 4L										3R													
4L	+5V Input from Buss	3L										4R													
5L	+12V Input from Buss	40L, 6L										5R													
6L	+12V Input from Buss	5L										6R													
7L												7R													
8L												8R													
9L												9R													
10L												10R													
11L												11R													
12L												12R													
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30L												30R													
31L												31R													
32L												32R													
33L												33R													
34L												34R													
35L												35R													
36L	Common to Buss	1L, 37L										36R	E8, Enable 8, OUT												
37L	Common to Buss	36L										37R	E9, Enable 9, OUT												
38L	+5V Input from Buss	3L, 39L										38R	E14, Enable 14, OUT												
39L	+5V Input from Buss	38L										39R	E15, Enable 15, OUT												
40L	+12V Input from Buss	5L, 41L										40R	E16, Enable 16, OUT												
41L	+12V Input from Buss	40L										41R	E17, Enable 17, OUT												
42L	Sensor Add. 0 Output (CMOS)											42R	BCD Output 10 <sup>5</sup> (1)												
43L	Sensor Add. 0 Input (TTL)											43R	N.C. Shift Clock OUT	40R											
44L	Sensor Add. 1 Output (CMOS)											44R	BCD Output 10 <sup>4</sup> (1)												
45L	Sensor Add. 1 Input (TTL)											45R	BCD Output 10 <sup>4</sup> (8)												
46L	Sensor Add. 2 Output (CMOS)											46R	BCD Output 10 <sup>4</sup> (4)												
47L	Sensor Add. 2 Input (TTL)											47R	BCD Output 10 <sup>3</sup> (2)												
48L	Sensor Add. 3 Output (CMOS)											48R	BCD Output 10 <sup>3</sup> (1)												
49L	Sensor Add. 3 Input (TTL)											49R	BCD Output 10 <sup>3</sup> (8)												
50L	5th Bit // Input											50R	BCD Output 10 <sup>3</sup> (4)												
51L	6th Bit // Input											51R	BCD Output 10 <sup>3</sup> (2)												
52L	7th Bit // Input											52R	BCD Output 10 <sup>2</sup> (1)												
53L	8th Bit // Input											53R	BCD Output 10 <sup>2</sup> (8)												

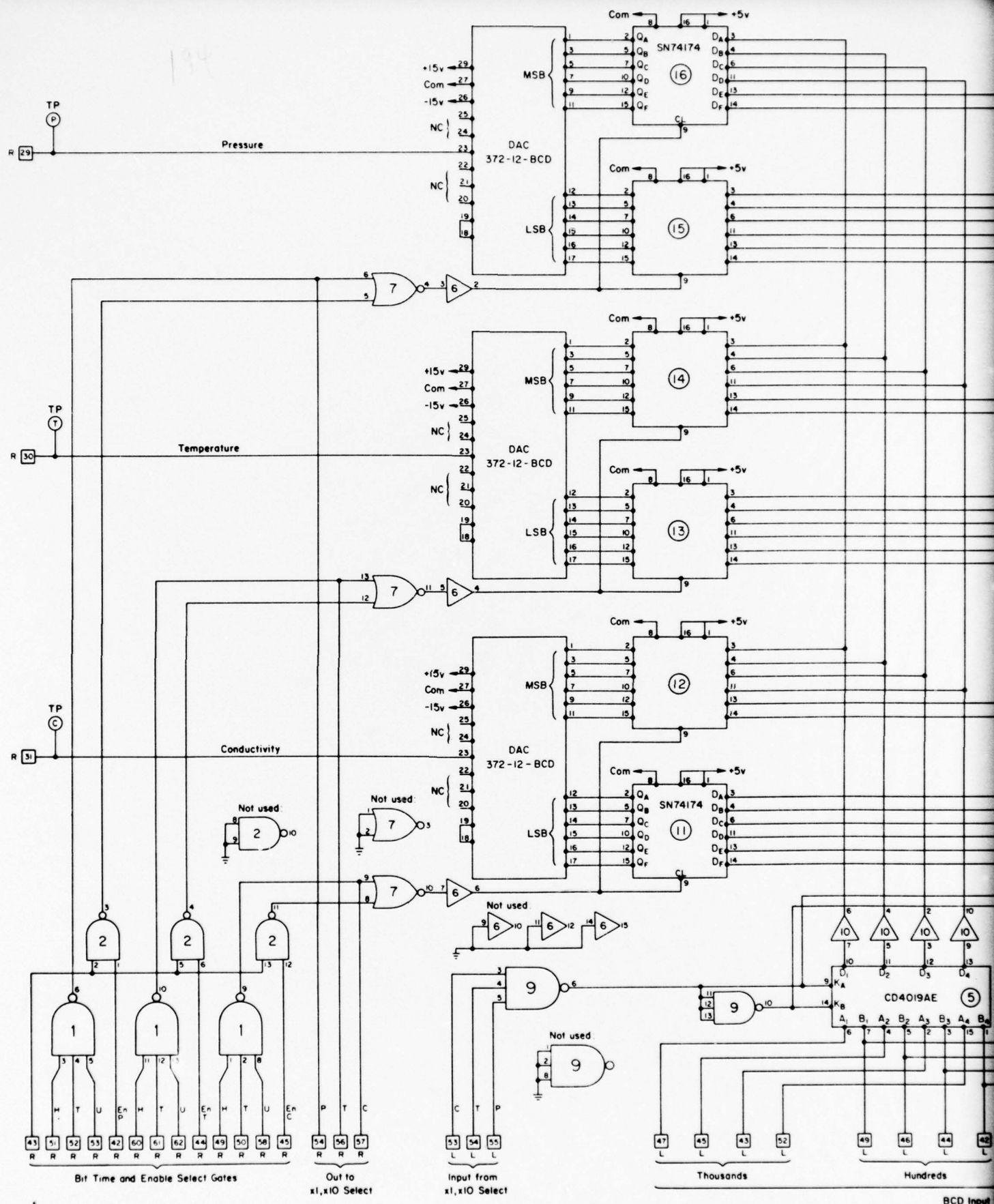
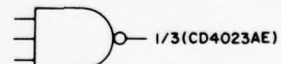
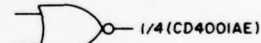
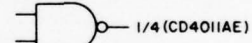
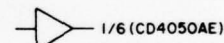
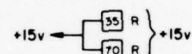
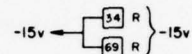
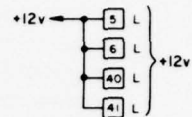
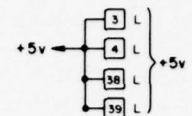
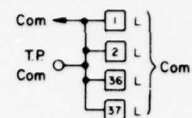
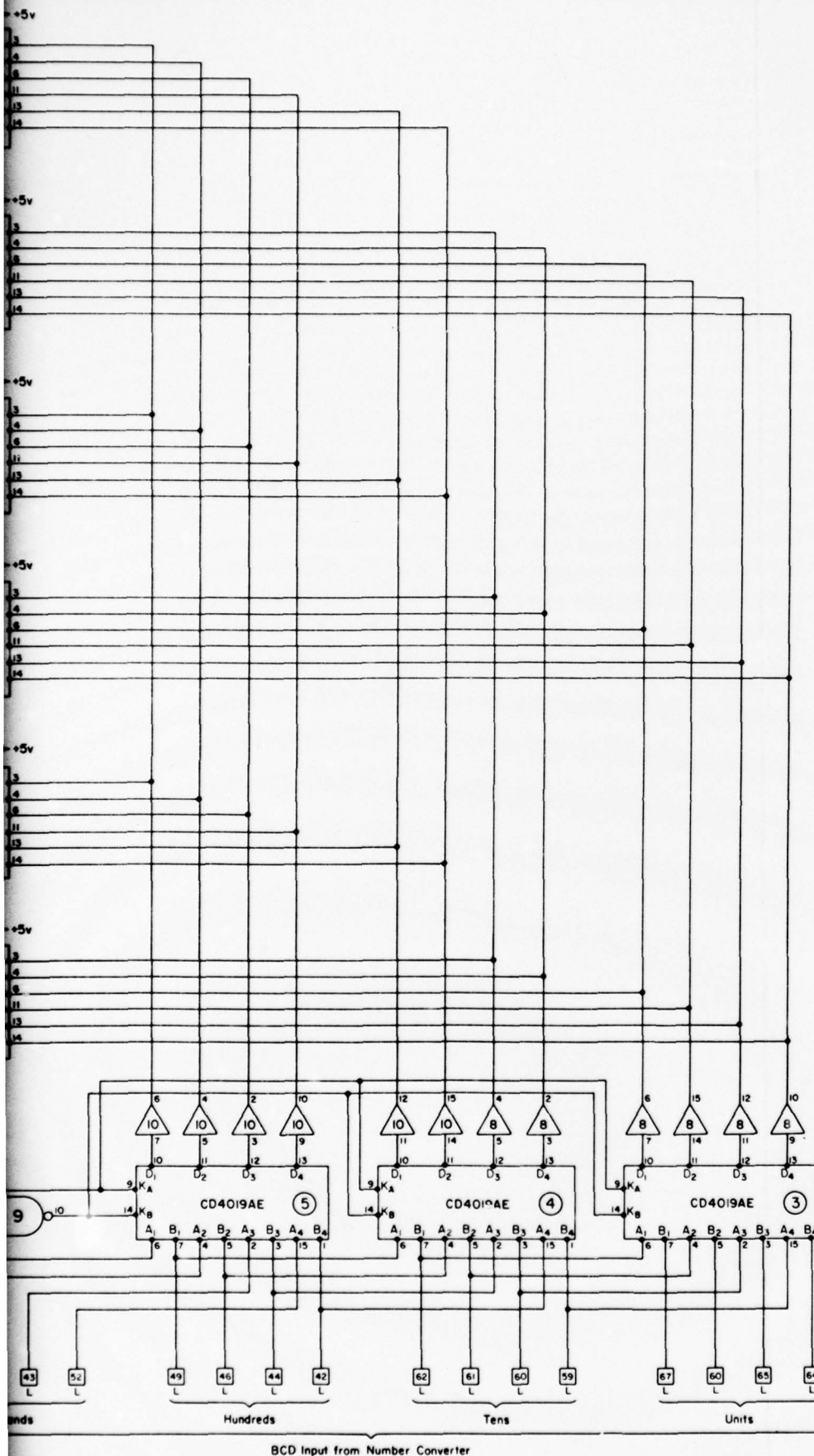




Fig. 5.2.3

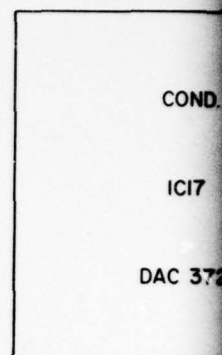
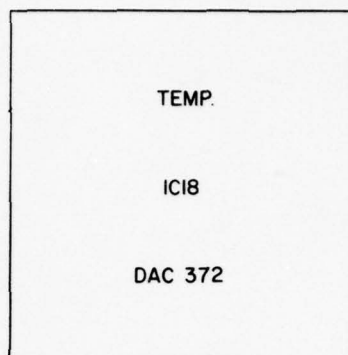
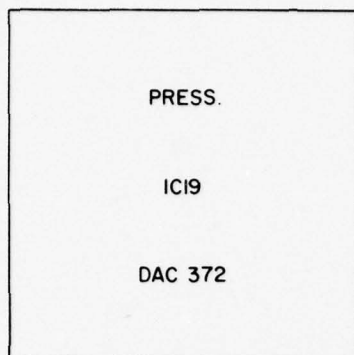
145



CTD DECK UNIT MK III  
D/A CONVERTER

2

196



ICI6 SN74174

ICI5 SN74174

ICI4 SN74174

ICI3 SN74174

ICI2 SN74174

ICI0 CD4050

ICI9 CD4023

ICI8 CD4050

ICI7 CD4001

ICI5 CD4019

ICI4 CD4019

ICI3 CD4019

ICI2 CD4011

CTD Deck Unit MK III

Fig. 5.2.3(2)

197

T

C

Note:  
•Feed throughs

TEMP.

IC18

DAC 372

COND.

IC17

DAC 372

IC14 SN74174

IC13 SN74174

IC12 SN74174

IC11 SN74174

IC8 CD4050

IC7 CD4001

IC6 CD4050

IC3 CD4019

IC2 CD4011

IC1 CD4023

CTD Deck Unit MK III

D/A CONVERTER

2

Pin Num.	Function	Demod. J7 and J8	Num. Conv. J3 and J4	D/A J5 and J6	Display J1 and J2	Comp. I/O (J11)	Internal I/O J12	Pin Num.	Function	Demod. J7 and J8	Num. Conv. J3 and J4	D/A J5 and J6	Display J1 and J2	Comp. I/O (J11)	Internal I/O J12	CF
1L	Common from Buss			2L, 36L				1R								
2L	Common from Buss			1L			AY, BA	2R								
3L	+5V Input from Buss			38L, 4L				3R								
4L	+5V Input from Buss			3L				4R								
5L	+12V Input from Buss			40L, 6L				5R								
6L	+12V Input from Buss			5L				6R								
7L								7R								
8L								8R								
9L								9R								
10L								10R								
11L								11R								
12L								12R								
13L								13R								
14L								14R								
15L								15R								
16L								16R								
17L								17R								
18L								18R								
19L								19R								
20L								20R								
21L								21R								
22L								22R								
23L								23R								
24L								24R								
25L								25R								
26L								26R								
27L								27R								
28L								28R								
29L								29R	Press D/A Output							AV
30L								30R	Temp D/A Output							AW
31L								31R	Cond D/A Output							AZ
32L								32R								
33L								33R								
34L								34R	-15V Input from Buss						69R	
35L								35R	+15V Input from Buss						70R	
36L	Common from Buss			1L, 37L				36R								
37L	Common from Buss			36L			BB	37R								
38L	+5V Input from Buss			3L, 39L				38R								
39L	+5V Input from Buss			38L				39R								
40L	+12V Input from Buss			5L, 41L				40R								
41L	+12V Input from Buss			40L				41R								
42L	BCD Input 10 <sup>2</sup> (1)							42R	Enable Press.							



Fig. 5.2.3(3)

[illegible]

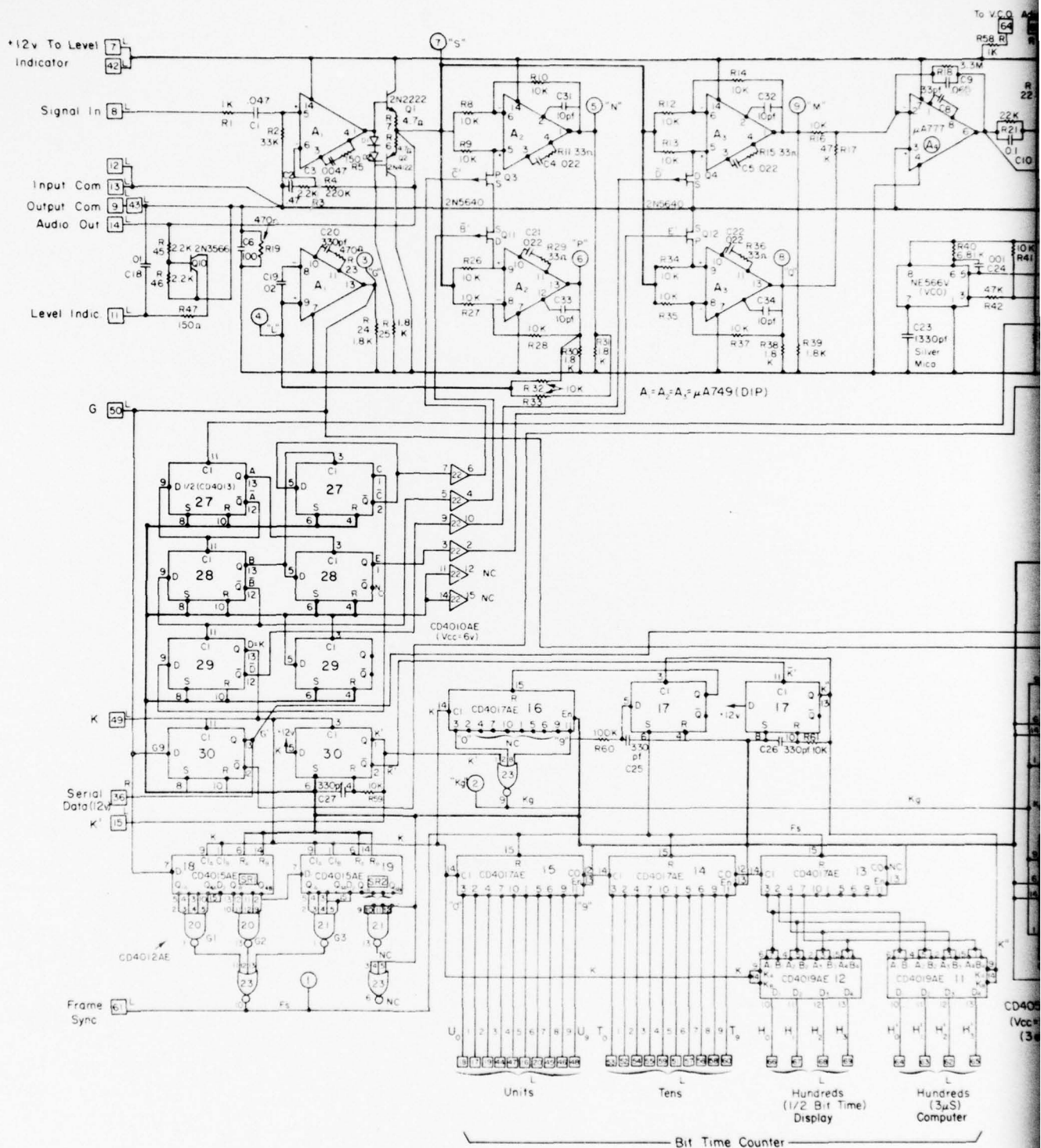
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Part Number: P/N O/T-PC-02-0

Date:

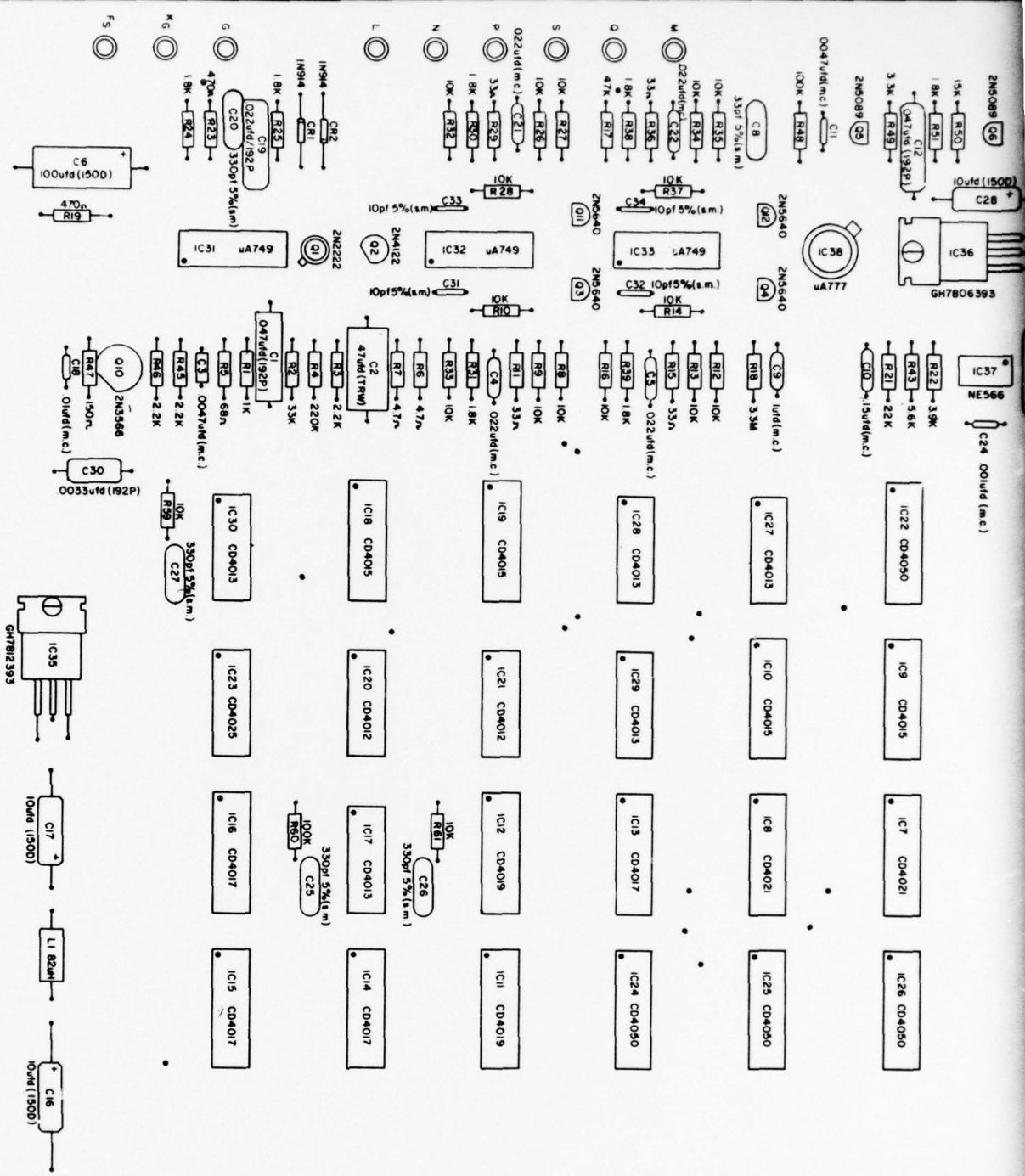
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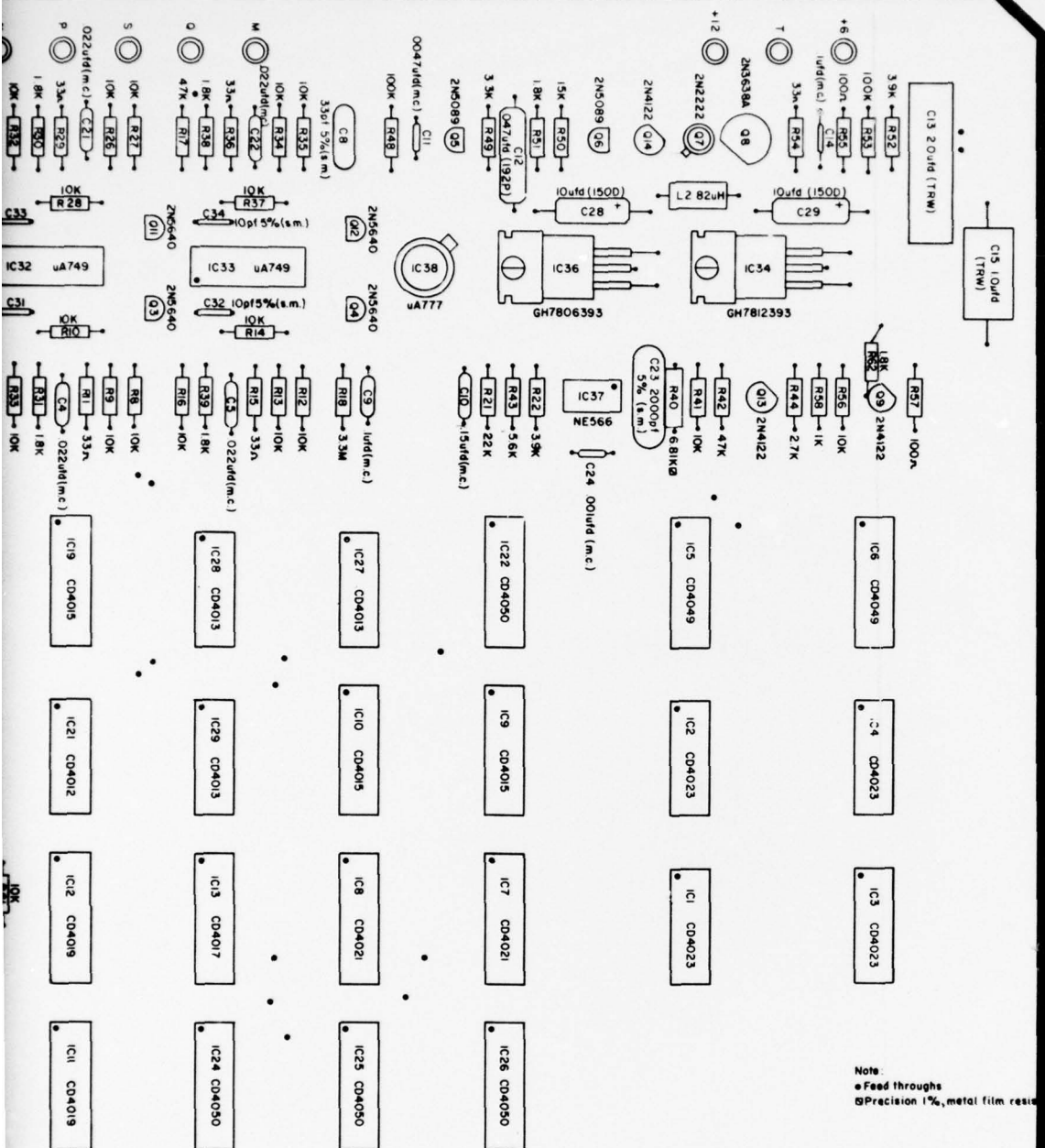
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P/N 014-PC-02-1

CTD Deck Unit MK III

Fig. 5.2.4(2)



CTD Deck Unit MK III

DEMODULATOR

2



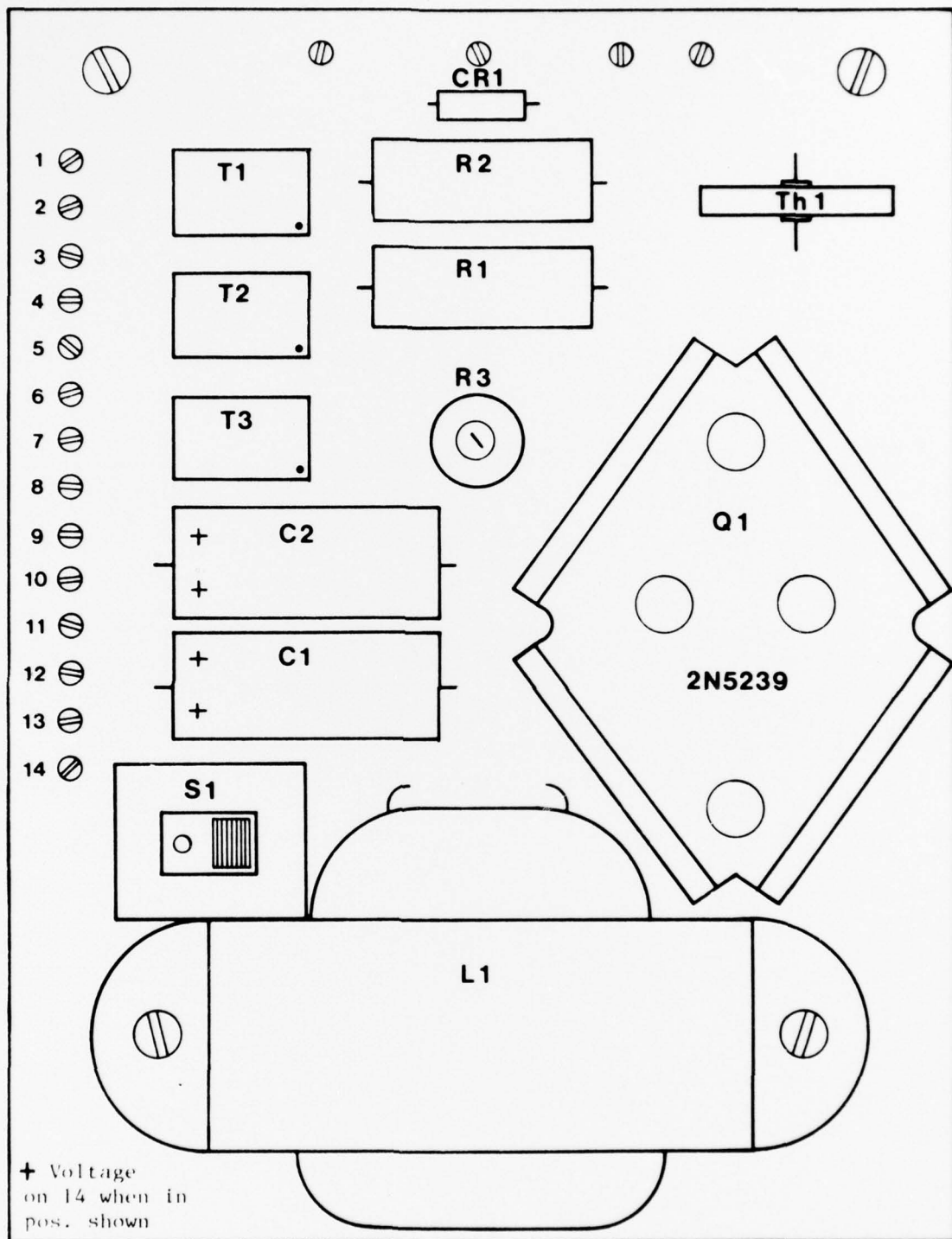
Pin Num.	Function	Demod. J7 and J8	D/A Conv. J3 and J4	Display J1 and J2	Comp. I/O (J11)	Internal I/O J12	Pin Num.	Function	Demod. J7 and J8	D/A Conv. J3 and J4	Display J1 and J2	Comp. I/O (J11)	Internal I/O J12
1L	Common to Buss	2L, 36L					1R	7th Bit // OUT					W
2L	Common to Buss	1L					2R	6th Bit // OUT					Y
3L	+5V Input from Buss	38L, 4L					3R	Temperature Interrupt					AS
4L	+5V Input from Buss	3L					4R	Frame Sync Interrupt					AM
5L	+12V Output to Buss	40L, 6L					5R	Pressure Interrupt					AP
6L	+12V Output to Buss	5L					6R	Units Count 6, Cond.	20L				
7L	Level Indicator, Anode	42L					7R	Tens Count 7, Cond.	56L				
8L	Signal Input						8R	Units Count 7, Sign Bits	45L				
9L	OUTPUT COMMON	43L					9R	Tens Count 8, Sign Bits	58L				
10L	- N/C -						10R	Hund Count Ho, Sign Bits	15R				
11L	Level Indicator Cathode						11R	Units Count 0, F.S.	18L				
12L	Input Common #II						12R	Tens Count 1, F.S.	52L				
13L	Input Common # I						13R	Units Count 2, Pressure	19L				
14L	Audio Out						14R	Tens Count 3, Pressure	55L				
15L	Serial Data Clock K <sup>1</sup>	67R <sup>1</sup>					15R	Hund Count Ho, Pressure	10R, 41R				
16L	Bit Time Count Units 5						16R	Spare Interrupt					BB
17L	Bit Time Count Units 1						17R	Spare Interrupt					AZ
18L	Bit Time Count Units 0	11R					18R	Spare Interrupt					BA
19L	Bit Time Count Units 2	13R					19R						
20L	Bit Time Count Units 6	6R					20R						
21L							21R						
22L	11th Bit // OUT						22R						
23L	12th Bit // OUT						23R						
24L	16th MSB // OUT						24R						
25L	Serial Data Out (MSB lead)	65R					25R						
26L	10th Bit // OUT						26R						
27L	15th Bit // OUT						27R						
28L	14th Bit // OUT						28R						
29L	13th Bit // OUT						29R	-N/C-					
30L	1st L.S.B. // OUT						30R	Phase Adj LED					AE
31L	8th Bit // OUT						31R	Phase Adj LED					AF
32L	2nd Bit // OUT						32R	-N/C-					
33L	3rd Bit // OUT						33R	-N/C-					
34L	4th Bit // OUT						34R	-N/C-					
35L	5th Bit // OUT						35R	+15V Input from Buss	70R				
36L	Common to Buss	1L, 37L					36R	Serial Data Out (12V)					
37L	Common to Buss	36L, 43R					37R	TTY Clock Out 5V Level					T
38L	+5V Input from Buss	31, 39L					38R	9th Bit // OUT					
39L	+5V Input from Buss	38L					39R	Number Conv P/S Control	68R				
40L	+12V Output to Buss	5L, 41L					40R	Number Conv. Shift Clock	43R				
41L	+12V Output to Buss	40L					41R	Hund Count Ho, Temp	15R, 44R				
42L	Level Indicator Anode	7L					42R	Tens Count 5, Temp	51L				
43L	Output Common	9L					43R	Units Count 4, Temp	47L				



Fig. 5.2.4(3)

19L	20L	21L	22L	23L	24L	25L	26L	27L	28L	29L	30L	31L	32L	33L	34L	35L	36L	37L	38L	39L	40L	41L	42L	43L	44L	45L	46L	47L	48L	49L	50L	51L	52L	53L	54L	55L	56L	57L	58L	59L	60L	61L	62L	63L	64L	65L	66L	67L	68L	69L	70L	71L	72L	73L	74L	75L	76L	77L	78L	79L	80L	81L	82L	83L	84L	85L	86L	87L	88L	89L	90L	91L	92L	93L	94L	95L	96L	97L	98L	99L	100L	101L	102L	103L	104L	105L	106L	107L	108L	109L	110L	111L	112L	113L	114L	115L	116L	117L	118L	119L	120L	121L	122L	123L	124L	125L	126L	127L	128L	129L	130L	131L	132L	133L	134L	135L	136L	137L	138L	139L	140L	141L	142L	143L	144L	145L	146L	147L	148L	149L	150L	151L	152L	153L	154L	155L	156L	157L	158L	159L	160L	161L	162L	163L	164L	165L	166L	167L	168L	169L	170L	171L	172L	173L	174L	175L	176L	177L	178L	179L	180L	181L	182L	183L	184L	185L	186L	187L	188L	189L	190L	191L	192L	193L	194L	195L	196L	197L	198L	199L	200L	201L	202L	203L	204L	205L	206L	207L	208L	209L	210L	211L	212L	213L	214L	215L	216L	217L	218L	219L	220L	221L	222L	223L	224L	225L	226L	227L	228L	229L	230L	231L	232L	233L	234L	235L	236L	237L	238L	239L	240L	241L	242L	243L	244L	245L	246L	247L	248L	249L	250L	251L	252L	253L	254L	255L	256L	257L	258L	259L	260L	261L	262L	263L	264L	265L	266L	267L	268L	269L	270L	271L	272L	273L	274L	275L	276L	277L	278L	279L	280L	281L	282L	283L	284L	285L	286L	287L	288L	289L	290L	291L	292L	293L	294L	295L	296L	297L	298L	299L	300L	301L	302L	303L	304L	305L	306L	307L	308L	309L	310L	311L	312L	313L	314L	315L	316L	317L	318L	319L	320L	321L	322L	323L	324L	325L	326L	327L	328L	329L	330L	331L	332L	333L	334L	335L	336L	337L	338L	339L	340L	341L	342L	343L	344L	345L	346L	347L	348L	349L	350L	351L	352L	353L	354L	355L	356L	357L	358L	359L	360L	361L	362L	363L	364L	365L	366L	367L	368L	369L	370L	371L	372L	373L	374L	375L	376L	377L	378L	379L	380L	381L	382L	383L	384L	385L	386L	387L	388L	389L	390L	391L	392L	393L	394L	395L	396L	397L	398L	399L	400L	401L	402L	403L	404L	405L	406L	407L	408L	409L	410L	411L	412L	413L	414L	415L	416L	417L	418L	419L	420L	421L	422L	423L	424L	425L	426L	427L	428L	429L	430L	431L	432L	433L	434L	435L	436L	437L	438L	439L	440L	441L	442L	443L	444L	445L	446L	447L	448L	449L	450L	451L	452L	453L	454L	455L	456L	457L	458L	459L	460L	461L	462L	463L	464L	465L	466L	467L	468L	469L	470L	471L	472L	473L	474L	475L	476L	477L	478L	479L	480L	481L	482L	483L	484L	485L	486L	487L	488L	489L	490L	491L	492L	493L	494L	495L	496L	497L	498L	499L	500L	501L	502L	503L	504L	505L	506L	507L	508L	509L	510L	511L	512L	513L	514L	515L	516L	517L	518L	519L	520L	521L	522L	523L	524L	525L	526L	527L	528L	529L	530L	531L	532L	533L	534L	535L	536L	537L	538L	539L	540L	541L	542L	543L	544L	545L	546L	547L	548L	549L	550L	551L	552L	553L	554L	555L	556L	557L	558L	559L	560L	561L	562L	563L	564L	565L	566L	567L	568L	569L	570L	571L	572L	573L	574L	575L	576L	577L	578L	579L	580L	581L	582L	583L	584L	585L	586L	587L	588L	589L	590L	591L	592L	593L	594L	595L	596L	597L	598L	599L	600L	601L	602L	603L	604L	605L	606L	607L	608L	609L	610L	611L	612L	613L	614L	615L	616L	617L	618L	619L	620L	621L	622L	623L	624L	625L	626L	627L	628L	629L	630L	631L	632L	633L	634L	635L	636L	637L	638L	639L	640L	641L	642L	643L	644L	645L	646L	647L	648L	649L	650L	651L	652L	653L	654L	655L	656L	657L	658L	659L	660L	661L	662L	663L	664L	665L	666L	667L	668L	669L	670L	671L	672L	673L	674L	675L	676L	677L	678L	679L	680L	681L	682L	683L	684L	685L	686L	687L	688L	689L	690L	691L	692L	693L	694L	695L	696L	697L	698L	699L	700L	701L	702L	703L	704L	705L	706L	707L	708L	709L	710L	711L	712L	713L	714L	715L	716L	717L	718L	719L	720L	721L	722L	723L	724L	725L	726L	727L	728L	729L	730L	731L	732L	733L	734L	735L	736L	737L	738L	739L	740L	741L	742L	743L	744L	745L	746L	747L	748L	749L	750L	751L	752L	753L	754L	755L	756L	757L	758L	759L	760L	761L	762L	763L	764L	765L	766L	767L	768L	769L	770L	771L	772L	773L	774L	775L	776L	777L	778L	779L	780L	781L	782L	783L	784L	785L	786L	787L	788L	789L	790L	791L	792L	793L	794L	795L	796L	797L	798L	799L	800L	801L	802L	803L	804L	805L	806L	807L	808L	809L	810L	811L	812L	813L	814L	815L	816L	817L	818L	819L	820L	821L	822L	823L	824L	825L	826L	827L	828L	829L	830L	831L	832L	833L	834L	835L	836L	837L	838L	839L	840L	841L	842L	843L	844L	845L	846L	847L	848L	849L	850L	851L	852L	853L	854L	855L	856L	857L	858L	859L	860L	861L	862L	863L	864L	865L	866L	867L	868L	869L	870L	871L	872L	873L	874L	875L	876L	877L	878L	879L	880L	881L	882L	883L	884L	885L	886L	887L	888L	889L	890L	891L	892L	893L	894L	895L	896L	897L	898L	899L	900L	901L	902L	903L	904L	905L	906L	907L	908L	909L	910L	911L	912L	913L	914L	915L	916L	917L	918L	919L	920L	921L	922L	923L	924L	925L	926L	927L	928L	929L	930L	931L	932L	933L	934L	935L	936L	937L	938L	939L	940L	941L	942L	943L	944L	945L	946L	947L	948L	949L	950L	951L	952L	953L	954L	955L	956L	957L	958L	959L	960L	961L	962L	963L	964L	965L	966L	967L	968L	969L	970L	971L	972L	973L	974L	975L	976L	977L	978L	979L	980L	981L	982L	983L	984L	985L	986L	987L	988L	989L	990L	991L	992L	993L	994L	995L	996L	997L	998L	999L	1000L	1001L	1002L	1003L	1004L	1005L	1006L	1007L	1008L	1009L	1010L	1011L	1012L	1013L	1014L	1015L	1016L	1017L	1018L	1019L	1020L	1021L	1022L	1023L	1024L	1025L	1026L	1027L	1028L	10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Fig. 5.2.6(2)



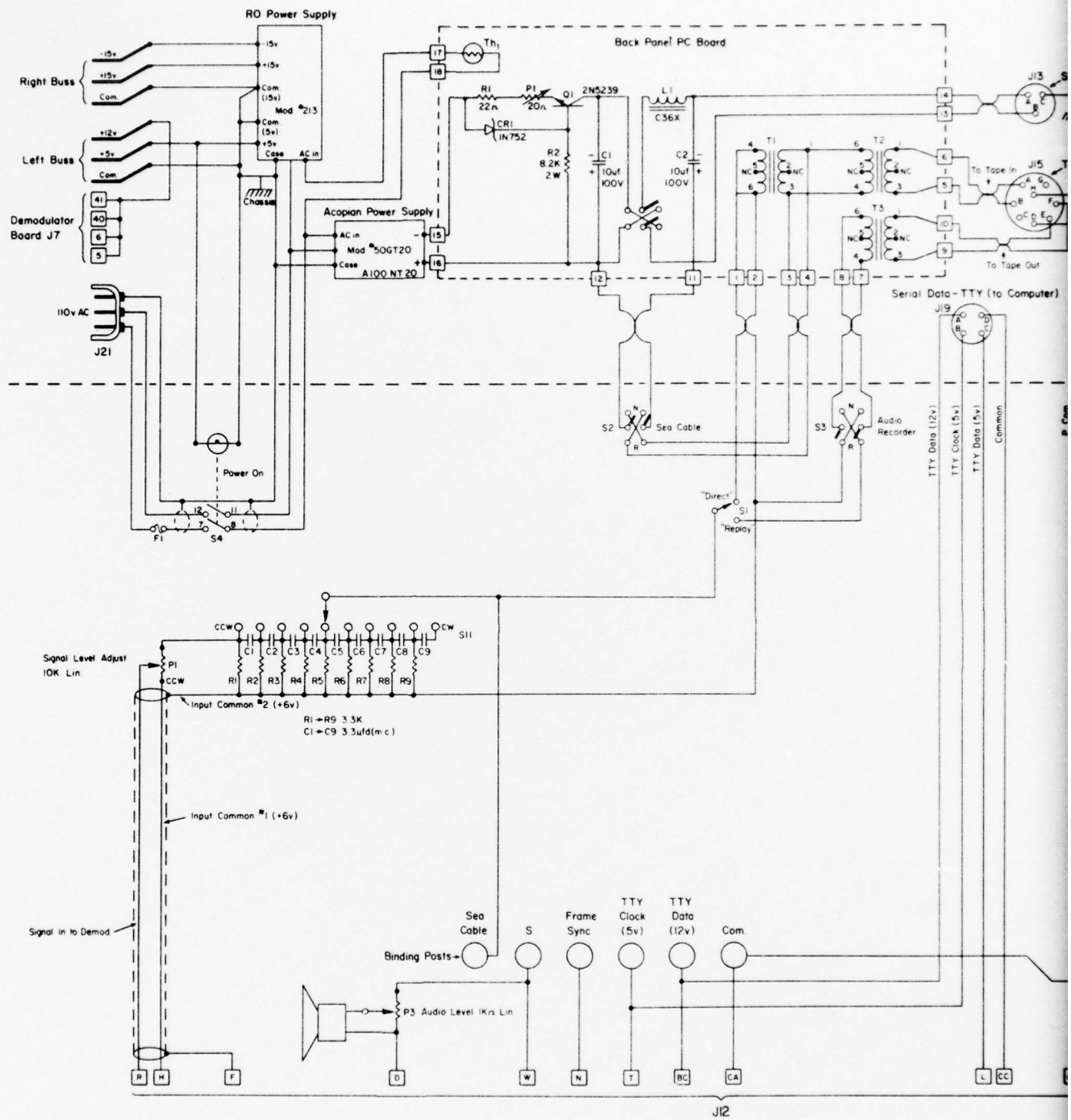
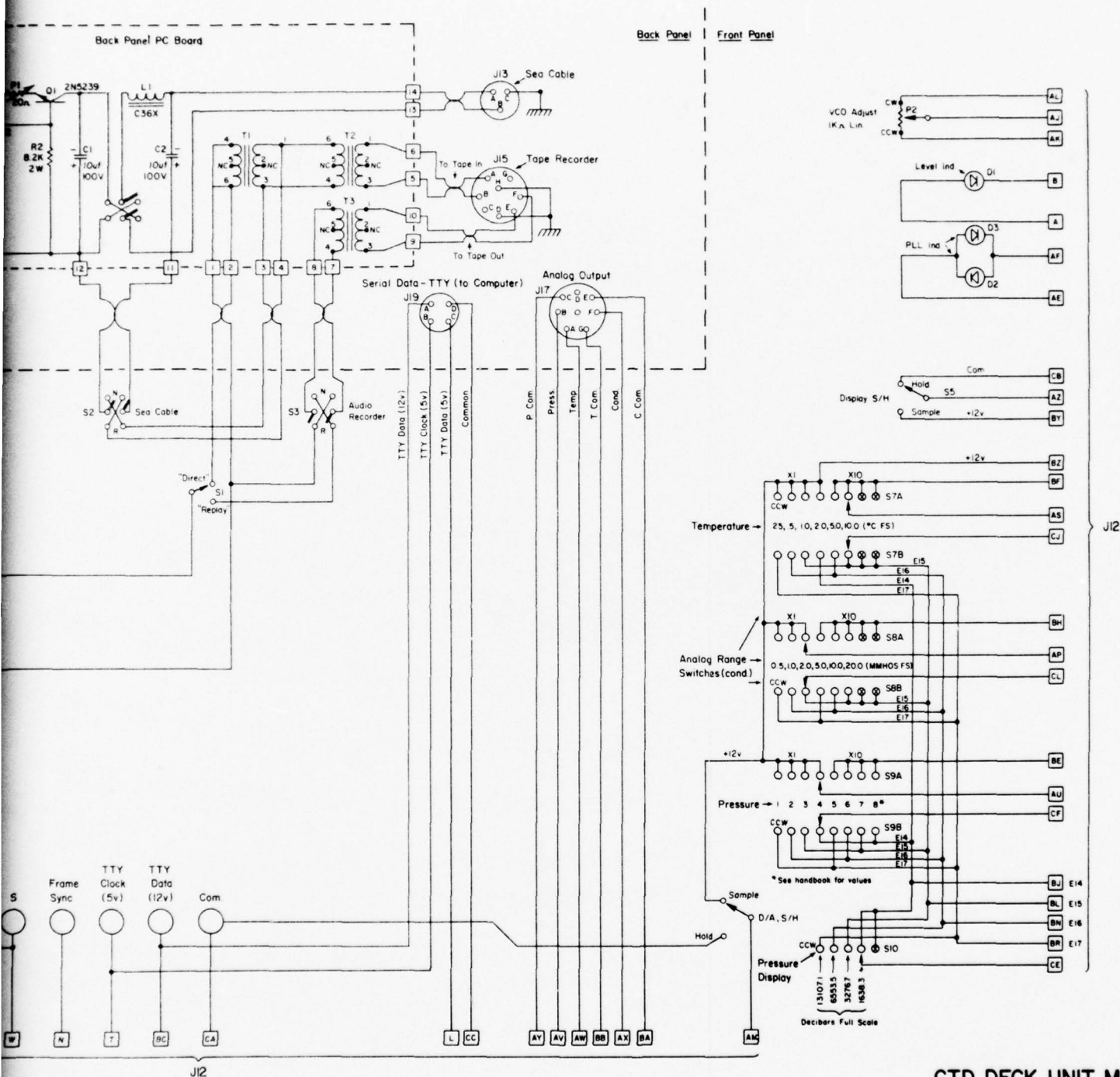


Fig. 5.2.7



CTD DECK UNIT MK III  
FRONT/BACK PANEL

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[illegible]



210

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Part Number: J12

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Fig. 5.2.7(3)

Y	6th Bit	// OUT	2R		X,AB	CY	Common	// IN	63L	CM,DA
Z	Common									
AA	5th Bit	// OUT	35L							
AB	Common									
AC	4th Bit	// OUT	34L		Z.AD		1st L.S.B.	// IN	62L	
AD	Common									
AE	3rd Bit	// OUT	33L		AB.AF					
AF	Common				AD.AI					
AH	2nd Bit	// OUT	32L							
AJ	Common				AF.AL					
AK	1st L.S.B.	// OUT	30L		AJ,					
AL	Common									
AM	Frame Sync Interrupt		4R							
AN	Common				AR,Bugs					
AP	Pressure Interrupt		5R							
AR	Common				AN.AT					
AS	Temp. Interrupt		3R							
AT	Common				AR.AV					
AU	Cond. Interrupt		50R							
AV	Common				AT.AZ					
AW	Sign Bits Interrupt		51R							
AX	Common				AV.BP					
AY	Spare Interrupt		49R							
AZ	Spare Interrupt		17R							
BA	Spare Interrupt		18R							
BB	Spare Interrupt		16R							
BC	Spare Interrupt		61R							
BD	Spare Interrupt		62R							
BE	Spare Interrupt		60R							
BF	Sensor Address Line		47L							
BH	Sensor Address Line		45L							
BJ	Sensor Address Line		43L							
BK	Sensor Address Line		49L							
BL	SENSE		67L							
BM	SENSE		68L							
BN	STROBE		66L							
BP	Common				AZ,BR					
BR	Common				BU,Bugs					
BS	Common									
BT	16th Bit	// IN	56L							
BU	Common									
BV	15th Bit	// IN	57L		BS,BW					
BW	Common				BU,BY					
BX	14th Bit	// IN	55L							
BY	Common				BW,CA					
BZ	13th Bit	// IN	54L							

Name of Connector: COMPUTER I/O

Part Number: J11

Date:

2

Connector: J 11

11 11



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## PARTS LISTS

<u>Underwater Unit</u>	<u>Part Number</u>	<u>Page</u>
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Fast Response Temp. Interface	003-PC-01-1	6.1.3
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Power Supply (U.W.U)	008-PC-01-0	6.1.6
AC Comparator	005-PC-01-1	6.1.7
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Chassis Mounted Circuits		6.2.7

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PRESSURE INTERFACE  
(UWU)  
Circuit Board 001-PC-01-1

6.1.1

Capacitors

C3	33	pf	5%	Silver Mica
C4	2000	pf	5%	Silver Mica
C6	10	ufd	10%	Sprague 150D 20v
C7	100	ufd	10%	Sprague 150D 20v
C8	8200	pf	5%	Silver Mica
C9	8200	pf	5%	Silver Mica
C10	T.B.D.		5%	Silver Mica
C11	T.B.D.		5%	Silver Mica

Connector

Elco            7022-035-000-001

Diodes

CR1	1N 914
CR2	1N 914
CR3	1N 914
CR4	1N 914
CR5	1N 914
CR6	1N 914

Inductors

L1    30mH    Triad    EM-030-A

Integrated Circuits

1C1    CD4011AE    Quad NAND Gates

Potentiometers

P1	1	kilohm	Bourns 3009Y
P2	10	kilohm	Bourns 3009Y
P3	20	kilohm	Bourns 3009Y
P4	1	kilohm	Bourns 3009Y
P5	100	ohm	Bourns 3009Y

Resistors

R1	2.21	kilohm	RN60C metal film	1%
R2	2.21	kilohm	RN60C metal film	1%
R3	33	ohm	RN60C metal film	1%
R4	T.B.D.		RN60C metal film	1%
R5	T.B.D.		RN60C metal film	1%
R6	3.32	megohm	RN60C metal film	1%
R7	T.B.D.			
R8	T.B.D.			
R9	33.2	kilohm	RN60C metal film	1%
R10	20	kilohm	RN60C metal film	1%
R11	49.9	kilohm	RN60C metal film	1%
R12	5.62	kilohm	RN60C metal film	1%
R13	47.5	kilohm	RN60C metal film	1%
R14	1	kilohm	RN60C metal film	1%
R15	221	ohm	RN60C metal film	1%
R16	499	ohm	RN60C metal film	1%
R17	221	ohm	RN60C metal film	1%
R18	1	megohm	1/2 watt carbon	5%
R19	1	megohm	1/4 watt carbon	5%
R20	200	ohm	Vishay 0.1%	
R21	T.B.D.			
R22	T.B.D.			

Sockets

1    Augat 514-AG-10D

Transformers

T1	001-T1-01-0	NBIS
T2	001-T2-01-0	NBIS
T3	001-T3-01-0	NBIS

Transistors

Q1	2N 4250
Q2	2N 5089
Q3	2N 4250
Q4	2N 5638
Q5	2N 5089
Q6	2N 5638



TEMPERATURE INTERFACE  
(UWU)  
Circuit Board 002-PC-01-1

6.1.2

Capacitors

C1	33	pf	5%	Silver Mica
C2	10	ufd	10%	Sprague 150D 20v
C3	100	ufd	10%	Sprague 150D 20v
C4	8200	pf	5%	Silver Mica
C4A	T.B.D.			
C5	8200	pf	5%	Silver Mica
C5A	T.B.D.			

Connector

Elco 7022-035-000-001

Diodes

CR1	1N 914
CR2	1N 914
CR3	1N 914
CR4	1N 914
CR5	1N 914
CR6	1N 914

Hardware

2	#4/40 x 5/8 Nylon Screws
2	#4 Nuts

Inductors

L1 30mH Triad EM-030-A

Integrated Circuits

1C1 CD4011AD Dual input Quad NAND

Potentiometers

P1	5	kilohm	Bourns 3009Y
P2	5	kilohm	Bourns 3009Y
P3	2	kilohm	Bourns 3009Y

Resistors

R1	20	kilohm	RN60C metal film 1%
R2	2	kilohm	RN60C metal film 1%
R3	200	kilohm	RN60C metal film 1%
R4	49.9	kilohm	RN60C metal film 1%
R5	5.62	kilohm	RN60C metal film 1%
R6	47.5	kilohm	RN60C metal film 1%
R7	1	kilohm	RN60C metal film 1%
R8	499	ohm	RN60C metal film 1%
R9	392	ohm	RN60C metal film 1%
R10	392	ohm	RN60C metal film 1%
R11	1	megohm	1/4 watt carbon 5%
R12	44.84	ohm	Vishay 0.1%
R13	300	ohm	Vishay 0.1%
R14	4.99	kilohm	RN60C metal film 1%
R15	1	megohm	1/4 watt carbon 5%
R16	33.2	kilohm	RN60C metal film 1%

Sockets

1 Augat 514-AG-10D

Transformers

T2	002-T2-01-0	NBIS
T3	002-T3-01-0	NBIS

Transistors

Q1	2N 4250
Q2	2N 5089
Q3	2N 4250
Q4	2N 5638
Q5	2N 5089
Q6	2N 5638

NOTE:

Fishay Resistor  $R_F$  is situated in the Sensor Housing.

$$R_F = 10 (R_{01} + R_{02}) (\pm 0.1\%)$$

$R_{01}$  + resistance of thermometer element  
1 at 0°C

$R_{02}$  = resistance of thermometer element  
2 at 0°C

FAST RESPONSE SENSOR  
(UWU)  
Circuit Board 003-PC-01-1

6.1.3

Capacitors

C1	50	pf	5%	Silver Mica
C2	1.0	ufd	10%	TRW 50v
C3	10	ufd	10%	Sprague 150D 20v
C4	10	pf	5%	Silver Mica
C5	1.0	ufd	10%	TRW 50v
C6	8200	pf	5%	Silver Mica
C7	0.1	ufd	10%	TRW 50v
C8	0.1	ufd	10%	TRW 50v
C9	.0033	ufd	10%	Sprague 192P 80v
C10	0.1	ufd	10%	TRW 50v
C11	30	pf	5%	Silver Mica
C12	1.8	ufd	10%	TRW 50v
C13	0.1	ufd	10%	TRW 50v
C14	330	pf	5%	Silver Mica
C15	100	ufd	10%	Sprague 150D 10v

Resistors (con't)

R4	10	kilohm
R5	470	ohm
R6	100	kilohm
R7	220	ohm
R8	3.3	kilohm
R9	270	kilohm
R10	270	kilohm
R11	10	kilohm
R12	100	kilohm
R13	100	kilohm
R14	4.7	ohm
R15	10	kilohm
R16	1	kilohm
R17	1	kilohm
R18	10	ohm
R18A	T.B.D.	
R19	180	ohm
R19A	T.B.D.	
R20	1	kilohm
R21	10	ohm

Connector

Elco 7022-035-000-001

Diodes

CR1	1N 914
CR2	1N 914

Sockets

3	Augat #514-AG-10D
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Inductors

L1	003-L1-01-0 NBIS
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Terminal Post

1	Cambion #160-1043-03-01
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Integrated Circuits

1C1	MEM780P Gen. Inst. Quad MOSFET
1C2	uA749DC Fairchild Dual Op. Amp.
1C3	MEM780P Gen. Inst. Quad MOSFET
1C4	LM208AD Nat. Semi. Op. Amp.

Transformers

T1	003-T1-01-0 NBIS
T2	003-T2-01-0 NBIS

Potentiometers

P1	10	kilohm	Bourns 3009Y
P2	10	kilohm	Bourns 3009Y

Resistors

$\frac{1}{4}$  watt carbon 5% (unless noted)

R1	1.91	kilohm	RN60C metal film 1%
R2	100	kilohm	
R3	22	kilohm	

CONDUCTIVITY INTERFACE  
(UWU)  
Circuit Board 004-PC-01-2

6.1.4

Capacitors

C1	10	ufd	10% Sprague 150D 20v
C2	100	ufd	10% Sprague 150D 20v
C3	390	pf	5% Silver Mica
C4	8200	pf	5% Silver Mica
C4A	T.B.D.		
C5	8200	pf	5% Silver Mica
C5A	T.B.D.		
C6	10	ufd	10% Sprague 150D 20v
C7	8200	pf	5% Silver Mica
C7A	T.B.D.		
C8	8200	pf	5% Silver Mica
C8A	T.B.D.		
C9	100	ufd	10% Sprague 150D 20v
C10	.0018	ufd	10% Sprague 192P

Connector

Elco 7022-035-000-001

Diodes

CR1	1N 914
CR2	1N 914
CR3	1N 914
CR4	1N 914
CR5	1N 914
CR6	1N 914

Hardware

2	#4/40 x 5/8 Nylon Screws
2	#4 Nuts

Inductors

L1	30 mH	Triad EM-030-A
L2	30 mH	Traid EM-030-A

Potentiometers

P1	5	kilohm Bourns 3009Y
P2	1	kilohm Bourns 3262P

Resistors

RN60C metal film (unless noted) 1%

R1	49.9	kilohm
R2	49.9	kilohm
R3	4.99	kilohm
R4	1	kilohm
R5	392	ohm
R6	392	ohm
R7	1	kilohm
R8	47.5	kilohm
R9	49.9	kilohm
R10	40	kilohm RN55C
R11	10.0	kilohm RN55C
R12	1	kilohm
R13	33.2	kilohm
R14	5.62	kilohm
R15	499	ohm
R16	1	megohm
R17	4.9	kilohm Vishay S102 .01%
R18	33.2	kilohm

Sockets

1	Augat #616-CG-1
1	Augat #516-AG-D

Transformers

T1	004-T1-01-0 NBIS
T2	004-T2-01-0 NBIS
T3	004-T3-01-0 NBIS
T4	004-T4-01-0 NBIS

Transistors

Q1	2N 4122
Q2	2N 5089
Q3	2N 4250
Q4	2N 4250
Q5	2N 5638
Q6	2N 5089
Q7	2N 4122
Q8	2N 5089

OXYGEN BOARDCircuit Board 020-PC-01-0Capacitors

C1	.33	ufd	10% Miniature Ceramic
C2	.01	ufd	10% Miniature Ceramic
C3	10	ufd	10% Sprague 150D 20v
C4	.047	ufd	10% Miniature Ceramic
C5	470	pf	5% Silver Mica
C6	.022	ufd	192P Sprague
C7	200	pf	5% Silver Mica
C8	200	pf	5% Silver Mica
C9	200	pf	5% Silver Mica
C10	200	pf	5% Silver Mica

Connectors

1	Elco #7022-35-000-001
3	Augat #508-AG-1D
4	Augat #514-AG-10D
7	Augat #516-AG-10D

Diodes

D1	1N 914
D2	1N 914
D3	1N 914
D4	1N 914
D5	LVA 43A Zener

Integrated Circuits

IC1	uA 776TC
IC2	LF 355H
IC3	uA 776TC
IC4	CD 4066 AE
IC5	CD 4013 AE
IC6	MC 14572 CP
IC7	CD 4021 AE
IC8	CD 4021 AE
IC9	CD 4040 AE
IC10	CD 4024 AE
IC11	CD 4013 AE
IC12	CD 4015 AE
IC13	CD 4021 AE
IC14	CD 4029 AE

Potentiometers

P1	100	kilohms	Bourns 3009Y
P2	50	kilohms	Bourns 3009Y
P3	100	kilohms	Bourns 3009Y
P4	20	kilohms	Bourns 3009Y

Regulators

Z1	AD 580
----	--------

Resistors

R1	10 kilohms $\frac{1}{4}$ w carbon, 5%
R2	68.1 kilohms RN60C Metal Film
R3	22.1 kilohms RN60C Metal Film
R4	22 megohms $\frac{1}{4}$ w carbon, 5%
R5	1.2 megohms RN60C Metal Film
R6	100 kilohms RN60C Metal Film
R7	499 kilohms RN60C Metal Film
R8	22 megohms $\frac{1}{4}$ w carbon, 5%
R9	392 kilohms RN60C Metal Film
R10	47.5 kilohms RN60C Metal Film
R11	33 kilohms $\frac{1}{4}$ w carbon, 5%
R12	33 kilohms $\frac{1}{4}$ w carbon, 5%
R13	220 kilohms $\frac{1}{4}$ w carbon, 5%
R14	33 kilohms $\frac{1}{4}$ w carbon, 5%
R15	22 kilohms $\frac{1}{4}$ w carbon, 5%
R16	220 kilohms $\frac{1}{4}$ w carbon, 5%

Transistors

Q1	2N 4401
Q2	2N 4401

Transformers

T1	Triad, Sp-67
----	--------------

POWER SUPPLY  
(UWU)  
Circuit Board 008-PC-01-0

Capacitors

C1	100	pf	5% Silver Mica
C2	1000	ufd	Sprague 39D 10v
C3	10	ufd	Sprague 150D 50v
C4	.1	ufd	10% TRW 50v
C5	100	ufd	Sprague 150D 20v
C6	1	ufd	10% TRW 50v
C7	2500	ufd	Sprague 39D 15v
C8	.0018	ufd	10% Sprague 192P 200v

Connector

Elco	7022-035-000-001
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Diodes

CR1	1N458A
CR2	1N914
CR3	1N914
CR4	1N914
CR5	1N941 (Zener)

Hardware

2	Screws/Pan Head	2/56 x 1/2
2	Hex nuts	#2
2	Inter. Tooth	#2

Integrated Circuits

1C1	Au723	Fairchild Op. Amp.
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Potentiometers

R6	500	ohm	Bourns 3009Y
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Resistors

1/4 watt carbon, 5%

R1	27	ohm
R2	1.5	kilohm

Resistors (con't)

R3	10	kilohm
R4	100	kilohm
R5	470	ohm
R7	2.7	kilohm
R8	560	ohm
R9	15	ohm
R10	560	ohm
R11	4.7	ohm
R12	560	ohm
R13	1	kilohm
R14	4.7	kilohm
R15	220	ohm
R16	470	ohm
R17	470	ohm
R18	470	ohm
R19	10	kilohm

Sockets

1	Augat	#514-AG-10D
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Transistors

Q1	2N3638A
Q2	2N3566
Q3	2N4122
Q4	2N3566
Q5	2N4912
Q6	2N4122
Q7	2N3566



A.C. COMPARATOR AND AUTOMATIC QUADRATURE BALANCE  
(UWU)

6.1.7

Circuit Board 005-PC-01-1

Capacitors					Terminal Post				
C1	1000	pf	2%	Silver Mica	4	Cambion #160-1043-03-01			
C2	5	pf	5%	Silver Mica					
C3	.01	ufd	10%	Sprague 192P					
C4	.033	ufd	10%	Sprague 192P		Transformers			
C5	.001	ufd	10%	Sprague 192P		200v			
C6	.01	ufd	10%	Sprague 192P	T1	005-T1-01-0	NBIS		
C7	330	pf	5%	Silver Mica	T2	005-T2-01-0	NBIS		
C8	100	ufd	10%	Sprague 150D		20v			
C9	.018	ufd	10%	Sprague 192P		80v			
C10	.0039	ufd	10%	Sprague 192P		80v			
C11	10	pf	5%	Silver Mica		Resistors			
C12	390	pf	5%	Silver Mica					
Connector					R1	10	kilohm	1/2 watt carbon	5%
Elco	7022-035-000-001				R2	47	ohm	1/2 watt carbon	5%
					R3	10	kilohm	1/2 watt carbon	5%
					R4	10	kilohm	1/2 watt carbon	5%
					R5	33	kilohm	1/2 watt carbon	5%
					R6	330	ohm	1/2 watt carbon	5%
					R7	3.3	kilohm	1/2 watt carbon	5%
					R8	150	kilohm	1/2 watt carbon	5%
					R9	1	kilohm	1/2 watt carbon	5%
					R10	10	kilohm	RN60C metal film	1%
					R11	10	kilohm	RN60C metal film	1%
					R12	10	kilohm	RN60C metal film	1%
					R13	3.3	kilohm	1/2 watt carbon	5%
					R14	15	ohm	1/2 watt carbon	5%
					R15	1	kilohm	1/2 watt carbon	5%
					R16	18	kilohm	1/2 watt carbon	5%
					R17	33	ohm	1/2 watt carbon	5%
					R18	1	kilohm	1/2 watt carbon	5%
					R19	33.2	kilohm	RN60C metal film	1%
					R20	22	kilohm	1/2 watt carbon	5%
					R21	3.3	kilohm	1/2 watt carbon	5%
					R22	4.7	kilohm	1/2 watt carbon	5%
					R23	33.2	kilohm	RN60C metal film	1%
					R24	33.2	kilohm	RN60C metal film	1%
					R25	33.2	kilohm	RN60C metal film	1%
					R26	10	kilohm	RN60C metal film	1%
					R27	10	kilohm	RN60C metal film	1%
					R28	10	kilohm	RN60C metal film	1%
					R29	3.3	kilohm	1/2 watt carbon	5%
					R30	15	ohm	1/2 watt carbon	5%
					R31	1	kilohm	1/2 watt carbon	5%
					R32	33.2	kilohm	RN60C metal film	1%
					R33	33.2	kilohm	RN60C metal film	1%
					R34	33.2	kilohm	RN60C metal film	1%
					R35	33.2	kilohm	RN60C metal film	1%
					R36	10	kilohm	RN60C metal film	1%
					R37	220	ohm	1/2 watt carbon	5%
					R38	1	megohm	1/2 watt carbon	5%
					R39	15	kilohm	1/2 watt carbon	5%
					R40	18	kilohm	1/2 watt carbon	5%
Diodes									
CRL	1N 914								
CR2	1N 914								
CR3	1N 914								
CR4	1N 914								
CR5	1N 914								
CR6	1N 914								
Integrated Circuits									
1C1	749DC	Fairchild Dual Op. Amp.							
1C2	749DC	Fairchild Dual Op. Amp.							
1C3	776TC	Fairchild Dual Op. Amp.							
1C4	777TC	Fairchild Dual Op. Amp.							
1C5	796HC	Fairchild Dual Op. Amp.							
1C6	MEM780P	Gen. Inst. Quad Mosfet							
Potentiometers									
P1	100	kilohm	Bourns	3009Y					
P2	10	kilohm	Bourns	3009Y					
P3	100	kilohm	Bourns	3009Y					
Sockets									
3	Augat #514-AG-10D								
2	Augat #508-AG-1-D								

A.C. COMPARATOR AND AUTOMATIC QUADRATURE BALANCE (con't)Resistors (con't)

R41	10	megohm, $\frac{1}{2}$ watt carbon, 5%
R42	470	ohm, $\frac{1}{2}$ watt carbon, 5%
R43	470	ohm, $\frac{1}{2}$ watt carbon, 5%
R44	15	kilohm, $\frac{1}{2}$ watt carbon, 5%
R45	1	kilohm, $\frac{1}{2}$ watt carbon, 5%
R46	820	kilohm, $\frac{1}{2}$ watt carbon, 5%

D/A CONVERTER  
(UWU)  
Circuit Board 006-PC-01-1

6.1.8

<u>Connector</u>			<u>Transistors (con't)</u>	
Elco	7022-035-000-001		Q16	2N 5638
			Q17	2N 5638
			Q18	2N 5638
			Q19	2N 5638
	<u>Integrated Circuits</u>		Q20	2N 5638
			Q21	2N 5638
1C1	CD4049AE	Hex Inverting Buffer	Q22	2N 5638
1C2	CD4049AE	Hex Inverting Buffer	Q23	2N 5638
1C3	CD4049AE	Hex Inverting Buffer	Q24	2N 5638
			Q25	2N 5638
			Q26	2N 5638
			Q27	2N 5638
			Q28	2N 5638
	<u>Resistors</u>		Q29	2N 5638
			Q30	2N 5638
R1	33	ohm, 1/4 watt carbon, 5%	Q31	2N 5638
R2	33	ohm, 1/4 watt carbon, 5%	Q32	2N 5638

<u>Sockets</u>	
3	Augat #516-AG-10D

<u>Transformers</u>	
T1	006-T1-01-0
T2	006-T2-01-0
T3	006-T3-01-0

<u>Transistors</u>	
Q1	2N 5638
Q2	2N 5638
Q3	2N 5638
Q4	2N 5638
Q5	2N 5638
Q6	2N 5638
Q7	2N 5638
Q8	2N 5638
Q9	2N 5638
Q10	2N 5638
Q11	2N 5638
Q12	2N 5638
Q13	2N 5638
Q14	2N 5638
Q15	2N 5638

DIGITIZER LOGIC AND QUADRATURE MEMORY  
(UWU)

6.1.9

Circuit Board 007-PC-01-1

Connector

Elco 7022-035-000-001

Diodes

CR1 1N914)  
CR2 1N914) Optional Use  
CR3 1N914)  
CR4 1N914)

Integrated Circuits

1C1 MC14549CP Successive approximation Register  
1C2 CD4021AE Shift Register  
1C3 MC14549CP Successive approximation Register  
1C4 CD4021AE Shift Register  
1C5 CD4013AE D type Flip-Flip (dual)  
1C6 CD4013AE D type Flip-Flop (dual)  
1C7 MEM780P Quad MOSFET (optional use)

Sockets

4 Augat #514-AG-10D  
4 Augat #516-AG-10D

Terminal Post

1 Cambion #160-1043-03-01

# MEMORY AND MULTIPLEXER

6.1.10

(UWU)

## Circuit Board 010-PC-01-1

### Capacitors

C1	220	pf	5%	Silver Mica
C2	330	pf	5%	Silver Mica
C3	330	pf	5%	Silver Mica
C4	.001	ufd	10%	Miniature Ceramic
C5	330	pf	5%	Silver Mica
C7	220	pf	5%	Silver Mica
C8	.082	ufd	10%	Miniature Ceramic
C9	.001	ufd	10%	Miniature Ceramic

### Resistors

$\frac{1}{4}$  watt carbon 5%

R1	10	kilohm
R2	10	kilohm
R3	10	kilohm
R4	10	kilohm
R5	10	kilohm
R7	10	kilohm
R8	68	kilohm
R9	10	kilohm

### Connector

Elco 7022-035-000-001

### Sockets

4	Augat #514-AG-10D
8	Augat #516-AG-10D
2	Augat #524-AG-10D

### Diodes

CR1	1N 914
CR2	1N 914

### Integrated Circuits

1C1	CD4039AE	Random Access Memory
1C2	CD4039AE	Random Access Memory
1C3	CD4021AE	Shift Register
1C4	CD4021AE	Shift Register
1C5	CD4021AE	Shift Register
1C6	CD4021AE	Shift Register
1C7	CD4021AE	Shift Register (Optional)
1C8	CD4021AE	Shift Register (Optional)
1C9	CD4019AE	AND/OR Select Gates
1C10	CD4017AE	Counter
1C11	CD4013AE	Flip-Flop
1C12	CD4013AE	Flip-Flop
1C13	CD4013AE	Flip-Flop
1C14	CD4013AE	Flip-Flop



MARK III and MARK IIb CTD ADAPTIVE SAMPLING BOARD  
 (UWU)  
NBIS Assembly Number C10009

Capacitors

C1 .1 ufd 10% minature ceramic  
 C2 .01 ufd 10% minature ceramic

Circuit Board

30006-

Resistors

R1	3.3	kilohms	1/4 watt carbon	5%
R2	33	kilohms	1/4 watt carbon	5%
R3	33	kilohms	1/4 watt carbon	5%
R4	10	kilohms	1/4 watt carbon	5%
R5	3.3	kilohms	1/4 watt carbon	5%
R6	33	kilohms	1/4 watt carbon	5%
R7	22	kilohms	1/4 watt carbon	5%
R8	33	kilohms	1/4 watt carbon	5%

Connector

Elco 7022

Transistors

Q1	2N 4124
Q2	2N 4126
Q3	2N 4126
Q4	2N 4124
Q5	2N 4124

Diodes

CR1 1N 914

Integrated Circuits

IC1	CD4017AE	Counter
IC2	CD4013AE	Flip-Flop
IC3	CD4013AE	Flip-Flop
IC4	CD4071BE	Quad OR
IC5	CD4013AE	Flip-Flop
IC6	CD4013AE	Flip-Flop
IC7	CD4021AE	Shift Register
IC8	CD4081BE	Quad AND
IC9	CD4017AE	Counter

TTY-FSK  
(UWU)  
Circuit Board 014-PC-01-0

Capacitors

C1	220	pf	5%	Silver Mica
C2	.082	ufd	10%	Miniature Ceramic
C3	1	ufd	10%	TRW 50v
C4	.15	ufd	10%	Miniature Ceramic
C5	1	ufd	10%	TRW 50v
C6	.33	ufd	10%	Miniature Ceramic
C7	100	ufd	10%	Sprague 150D 10v
C8	470	pf	5%	Silver Mica

Resistors (con't)

R12	33	kilohm
R13	33	kilohm
R14	33	kilohm
R15	33	kilohm
R16	33	kilohm
R17	33	kilohm
R18	33	kilohm

Connectors

1	Elco	#7022-35-000-001
9	Augat	#514-AG-10D
6	Augat	#516-AG-10D

Switches

1	CTS	#206-8
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Integrated Circuits

IC1	CD4017AE	Counter
IC2	CD4013AE	Flip-Flop
IC3	CD4013AE	Flip-Flop
IC4	CD4066AE	Quad Bilateral Switch
IC5	CD4015AE	Shift Register
IC6	CD4001AE	Quad NOR Gates
IC7	CD4049AE	Hex Buffer
IC8	CD4021AE	Shift Register
IC9	CD4013AE	Flip-Flop
IC10	CD4017AE	Counter
IC11	CD4068AE	Input NAND Gates
IC12	CD4013AE	Flip-Flop
IC13	CD4025AE	
IC14	CD4024AE	Counter

Transformers

1	014-T1-01-0	NBIS
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Transistors

Q1	AD	811
Q2	2N	4401

Resistors

$\frac{1}{4}$  watt carbon 5% (unless noted)

R1	10	kilohm
R2	18.2	kilohm RN60C Metal Film
R3	18.2	kilohm RN60C Metal Film
R4	18.2	kilohm RN60C Metal Film
R5	18.2	kilohm RN60C Metal Film
R6	2.2	kilohm
R7	3.3	kilohm
R8	1.8	kilohm
R9	82	ohm
R10	12	kilohm
R11	12	kilohm

**SIGNAL GENERATOR**  
**CIRCUIT BOARD 30001**

Capacitors

C1	220	pf	5% Silver Mica
C2	62	pf	5% Silver Mica
C3	TBD		
C4	5000	pf	5% Silver Mica
C5	.47	ufd	TRW
C6	TBD		
C7	.1	ufd	TRW
C8	.0033	ufd	192P, Sprague
C9	.022	ufd	192P, Sprague
C10	.1	ufd	TRW
C11	.022	ufd	192P, Sprague
C12	10	ufd	10% Sprague 150D, 20v
C13	10	pf	5% Silver Mica
C14	10	pf	5% Silver Mica

Resistors (con't)

R6	3.3	kilohm
R7	33	kilohm
R8	33	kilohm
R9	3.3	kilohm
R10	10	kilohm
R11	27	kilohm
R12	27	kilohm
R13	10	kilohm
R14	470	kilohm
R15	33	ohm
R16	3.3	kilohm
R17	10	kilohm
R18	10	kilohm
R19	33	ohm
R20	3.3	kilohm

Connectors

3	Augat #514-AG-10D
2	Augat #516-AG-10D
1	Elco #7022-035-000-001

Terminal Post

4	Cambion #140-1785-02-01-00
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Transformers

	<u>Crystals</u>	T1	Sig. Gen. #013-T1-01-3
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1	640 KHZ
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Inductors

L1	Sig. Gen. L1
L2	82uf, WEE 82

Transistors

Q1	2N 5089
Q2	2N 4122
Q3	2N 3566
Q4	2N 4401

Integrated Circuits

IC1	CD 4017 AE
IC2	CD 4040 AE
IC3	CD 4024 AE
IC4	CD 4013 AE
IC5	Ua 749

Resistors

	$\frac{1}{2}$ watt carbon, 5%
R1	1.5 megohm
R2	47 ohm
R3	3.9 kilohm
R4	33 kilohm
R5	100 kilohm

SENSOR HEAD ASSEMBLY

1 BULKHEAD SEAL BLOCK, NBIS #005-SS-01-0  
 1 SENSOR CLAMP, NBIS #006-SS-01-0  
 1 SENSOR SEAL BLOCK, NBIS #007-SS-01-0  
 1 SENSOR MOUNTING BLOCK, NBIS #008-SS-01-0  
 1 SENSOR GUARD, NBIS #009-SS-01-0  
 1 SENSOR HEAD BASE, NBIS #010-SS-01-0  
 1 SENSOR BASE, NBIS #011-SS-01-0  
 1 SENSOR BASE COVER, NBIS #012-SS-01-0  
 1 \* OXYGEN ADAPTOR, NBIS #013-SS-01-0  
  
 1 CONDUCTIVITY PLUG ASSEMBLY, NBIS #003-CP-01-0  
 1 THERMISTOR PLUG ASSEMBLY, NBIS #004-CP-01-0  
  
 1 CONDUCTIVITY CELL ASSEMBLY, NBIS #001-CC-01-0  
 1 THERMISTOR ASSEMBLY, NBIS #002-TC-01-0  
  
 1 TRANSFORMER, NBIS #002-T1-01-0  
 1 CIRCUIT BOARD, NBIS #019-PC-01-0  
  
 1 THERMOMETER, ROSEMONT #171BJ  
 18 CAMBION TERMINAL POST, #140-1785-02-01-00  
 16 HERMETIC SEAL CORP., SEALS #1045-954  
 12' COONER WIRE, #NMV 2/28-736 SJ, Double  
 4' COONER WIRE, #NMV 1/28-736 SJ, Single  
 32" COONER WIRE, #NUF 32-740  
 2 "O" RINGS, #ARP 568-032  
 1 "O" RINGS, #ARP 568-303  
 1 "O" RINGS, #ARP 568-024  
 2 "O" RINGS, #ARP 568-010  
 4 SCREWS, 4/40 x  $\frac{1}{2}$ , Filister socket, S/S  
 2 SCREWS, 10/32 x 3/8, Panhead, S/S  
 2 INTERNAL TOOTH LOCKWASHERS, #10  
 3 SCREWS,  $\frac{1}{4}$  x 28 x 2, Cap, S/S  
 1 SOCKET WRENCH (3/32 Hex Key)

\* OPTIONAL NOTE: If #013-SS-01-0 is used, #012-SS-01-0 is not required.

## T.B.D. VISHAY RESISTORS:

HP 202      1.8534 kilohms)  
              1.8542 kilohms) .01%  
              1.8526 kilohms)

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UNDERWATER UNIT ELECTRONICS CHASSIS

End Plates B10031	2 each
Right Card Guide B10032	1 each
Left Card Guide B10033	1 each
Card Guide B10034	1 each
Connector #00-7008-035-163-001	13 each
Screws #4/40 x 5/8 Pan Head	26 each
Nuts #4	26 each
Internal Tooth Lockwashers #4	26 each
Screws #6/32 x 3/8 Flat Head	8 each
Screws #6/32 x 3/8 Pan Head	8 each
Internal Tooth Lockwashers #6	8 each
Ground Lug #6	1 each
Connector #XSG-2-IDC-2	1 each
Connector #PT-06A-8-4P(SR)	1 each
Diode #1N2936	1 each
Bottom End Cap B10030	1 each
Top Cap B10029	1 each
Pressure Case B10028-G1	1 each
Rochester Connector #XSG-2BCL	1 each
V-Band Clamps 420-3-712	2 each
Guard Cage B10044	1 each
Rochester Connector #RMG-2-FS	1 each
Rochester Connector #G-FLS-P	1 each
Sea Data Extender Card #DA21	1 each
Crate	1 each
Hex Wrench 3/32	1 each



DECK UNIT  
DISPLAY CARD  
Circuit Board 016-PC-02-1

Hardware

2 Ejectors w/pins  
12 Cambion Terminal Post #160-1043-03-01  
18 Display #HP-5082-7302 (\*40)  
2 Display #HP-5082-7304 (\*4)

Resistors (con't)

\*R17 150 ohm  
\*R18 150 ohm

Integrated Circuits

1C1 CD4050AE Hex Buffer  
1C2 CD4050AE Hex Buffer  
1C3 CD4050AE Hex Buffer  
1C4 CD4050AE Hex Buffer  
1C5 CD4019AE Quad AND/OR Select Gate  
1C6 CD4050AE Hex Buffer  
1C7 CD4050AE Hex Buffer  
1C8 CD4050AE Hex Buffer  
1C9 CD4050AE Hex Buffer  
1C10 CD4012AE Dual 4 Input NAND Gate  
1C11 CD4012AE Dual 4 Input NAND Gate  
1C12 CD4012AE Dual 4 Input NAND Gate  
1C13 CD4050AE Hex Buffer  
1C14 CD4050AE Hex Buffer  
1C15 SN74174N Hex Latch  
1C16 CD4012AE Dual 4 Input NAND Gate  
1C17 CD4012AE Dual 4 Input NAND Gate  
1C18 SN74174N Hex Latch  
1C19 CD4012AE Dual 4 Input NAND Gate

Sockets

6 Jermyn #A23-2023 (\*8)  
3 Jermyn #A23-2030 (\*4)  
6 Augat #514-AG-10D  
13 Augat #516-AG-10D

Resistors

$\frac{1}{4}$  watt carbon, 5%

\*R1 330 ohm  
\*R2 330 ohm  
R3 330 ohm  
R4 330 ohm  
\*R5 330 ohm  
\*R6 330 ohm  
R7 330 ohm  
R8 330 ohm  
\*R9 330 ohm  
\*R10 330 ohm  
\*R11 330 ohm  
\*R12 330 ohm  
\*R13 150 ohm  
R14 150 ohm  
R15 150 ohm  
R16 150 ohm

NOTE: \* OPTIONAL USE

DECK UNIT  
NUMBER CONVERTER  
Circuit Board 015-PC-02-0

Capacitors

C1	100	pf	5%	Silver Mica
C2	100	pf	5%	Silver Mica
C3	330	pf	5%	Silver Mica
C4	100	pf	5%	Silver Mica

Potentiometers

P21	5 Kilohm	Bourns	3009Y
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Resistors

$\frac{1}{4}$  watt carbon, 5%

Hardware

2	Ejectors w/pins
4	Cambion Terminal Post #140-1785-02-01

R1	10	kilohm
R2	10	kilohm
R3	3.3	kilohm
R4	10	kilohm
R5	10	kilohm
R6	3.3	kilohm
R7	10	kilohm
R8	10	kilohm
R9	3.3	kilohm
R10	10	kilohm
R11	10	kilohm
R12	3.3	kilohm
R13	10	kilohm
R14	10	kilohm
R15	3.3	kilohm
R16	10	kilohm
R17	10	kilohm
R18	3.3	kilohm
R19	10	kilohm
R20	10	kilohm
R21	10	kilohm
R22	15	kilohm
R23	2.2	kilohm

Integrated Circuits

1C1	SN74165	Shift Register
1C2	CD4919AE	Quad AND/OR Select Gates
1C3	CD4035AE	4 Stage Shift Register
1C4	CD4035AE	4 Stage Shift Register
1C5	CD4035AE	4 Stage Shift Register
1C6	CD4035AE	4 Stage Shift Register
1C7	CD4035AE	4 Stage Shift Register
1C8	SN74165	Shift Register
1C9	CD4019AE	Quad AND/OR Select Gates
1C10	CD4008AE	4 Bit Full Adder
1C11	CD4008AE	4 Bit Full Adder
1C12	CD4008AE	4 Bit Full Adder
1C13	CD4008AE	4 Bit Full Adder
1C14	CD4008AE	4 Bit Full Adder
1C15	SN7402	Quad 2 Input NOR Gates
1C16	CD4017AE	Decade Counter
1C17	CD4023AE	Triple 3 Input NAND Gates
1C18	CD4023AE	Triple 3 Input NAND Gates
1C19	CD4023AE	Triple 3 Input NAND Gates
1C20	CD4023AE	Triple 3 Input NAND Gates
1C21	CD4023AE	Triple 3 Input NAND Gates
1C22	CD4050AE	Hex Buffer
1C23	CD4011AE	Quad 2 Input NAND Gates
1C24	CD4013AE	Dual D type Flip-Flop
1C25	CD4013AE	Dual D type Flip-Flop
1C26	CD4013AE	Dual D type Flip-Flop
1C27	CD4049AE	Inverting Hex Buffer
1C28	CD4011AE	Quad 2 Input NAND Gates
1C29	CD4013AE	Dual D type Flip-Flop
1C30	CD4001AE	Quad 2 Input NOR Gates
1C31	CD4013AE	Dual D type Flip-Flop
1C32	CD4011AE	Quad 2 Input NAND Gates

Sockets

15	Augat #514-AG-10D
17	Augat #516-AG-10D

Transistors

Q1	2N 2369
Q2	2N 2369
Q3	2N 2369
Q4	2N 2369
Q5	2N 2369
Q6	2N 2369

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DECK UNIT  
D/A CONVERTER  
Circuit Board 017-PC-02-1

Hardware

2 Ejectors w/pins  
4 Cambion Terminal Post #160-1043-03-01

Integrated Circuits

1C1	CD4023AE	TRI 3 Input NOR Gates
1C2	CD4011AE	Quad 2 Input NAND Gates
1C3	CD4019AE	Quad AND/OR Select Gates
1C4	CD4019AE	Quad AND/OR Select Gates
1C5	CD4019AE	Quad AND/OR Select Gates
1C6	CD4050AE	Hex Non-Inverting Buffer
1C7	CD4001AE	Quad 2 Input NOR Gates
1C8	CD4050AE	Hex Non-Inverting Buffer
1C9	CD4023AE	TRI 3 Input NOR Gates
1C10	CD4050AE	Hex Buffer
1C11	SN74174AE	Hex D type Flip-Flop
1C12	SN74174AE	Hex D type Flip-Flop
1C13	SN74174AE	Hex D type Flip-Flop
1C14	SN74174AE	Hex D type Flip-Flop
1C15	SN74174AE	Hex D type Flip-Flop
1C16	SN74174AE	Hex D type Flip-Flop
1C17	DAC-372	Hybrid Systems D/A Converter
1C18	DAC-372	Hybrid Systems D/A Converter
1C19	DAC-372	Hybrid Systems D/A Converter

Sockets

4 Augat #514-AG-10D  
12 Augat #516-AG-10D

DECK UNIT DEMODULATORCircuit Board 014-PC-02-1Capacitors

C1	.047	ufd	10%	Sprague 192P 80v
C2	.47	ufd	10%	TRW 50v
C3	.0047	ufd	10%	Miniature Ceramic
C4	.022	ufd	10%	Miniature Ceramic
C5	.022	ufd	10%	Miniature Ceramic
C6	100	ufd	10%	Sprague 150D 20v
C8	33	pf	5%	Silver Mica
*C9	.1	ufd	10%	Miniature Ceramic
*C10	.15	ufd	10%	Miniature Ceramic
C11	.0047	ufd	10%	Miniature Ceramic
C12	.047	ufd	10%	Sprague 192P 80v
C13	2.0	ufd	10%	TRW 50v
C14	.1	ufd	10%	Miniature Ceramic
C15	1.0	ufd	10%	TRW 50v
C16	10	ufd	10%	Sprague 150D 20v
C17	10	ufd	10%	Sprague 150D 20v
C18	101	ufd	10%	Miniature Ceramic
C19	.022	ufd	10%	Sprague 192P 80v
C20	330	pf	5%	Silver Mica
C21	.022	ufd	10%	Miniature Ceramic
C22	.022	ufd	10%	Miniature Ceramic
*C23	2000	pf	5%	Silver Mica
C24	.001	ufd	10%	Miniature Ceramic
C25	330	pf	5%	Silver Mica
C26	330	pf	5%	Silver Mica
C27	330	pf	5%	Silver Mica
C28	10	ufd	10%	Sprague 150D 20v
C29	10	ufd	10%	Sprague 150D 20v
C30	.0033	ufd	10%	Sprague 192P 200v
C31	10	pf	5%	Silver Mica
C32	10	pf	5%	Silver Mica
C33	10	pf	5%	Silver Mica
C34	10	pf	5%	Silver Mica

\* 5KHz operation only:

C9 = .068 ufd 10% Miniature Ceramic  
 C10 = .1 ufd 10% Miniature Ceramic  
 C23 = 1330 pf 5% Silver Mica

Diodes

CR1	1N 914
CR2	1N 914

Inductors

L1	82 uh Nytronics Wee Ductors
L2	82 uh Nytronics Wee Ductors

Integrated Circuits

1C1	CD4023	Triple 3 Input NAND Gates
1C2	CD4023	Triple 3 Input NAND Gates
1C3	CD4023	Triple 3 Input NAND Gates
1C4	CD4023	Triple 3 Input NAND Gates
1C5	CD4049	Inverting Hex Buffer
1C6	CD4049	Inverting Hex Buffer
1C7	CD4021	Shift Register
1C8	CD4021	Shift Register
1C9	CD4015	Shift Register
1C10	CD4015	Shift Register
1C11	CD4019	Quad AND/OR Select Gates
1C12	CD4019	Quad AND/OR Select Gates
1C13	CD4017	Decade Counter
1C14	CD4017	Decade Counter
1C15	CD4017	Decade Counter
1C16	CD4017	Decade Counter
1C17	CD4013	Dual "D" type Flip-Flop
1C18	CD4015	Shift Register
1C19	CD4015	Shift Register
1C20	CD4012	Dual 4 Input NAND Gates
1C21	CD4012	Dual 4 Input NAND Gates
1C22	CD4050	Non-Inverting Hex Buffer
1C23	CD4025	Triple Input NOR Gates
1C24	CD4050	Non-Inverting Hex Buffer
1C25	CD4050	Non-Inverting Hex Buffer
1C26	CD4050	Non-Inverting Hex Buffer
1C27	CD4013	Dual "D" type Flip-Flop
1C28	CD4013	Dual "D" type Flip-Flop
1C29	CD4013	Dual "D" type Flip-Flop
1C30	CD4013	Dual "D" type Flip-Flop
1C31	uA749	Dual Operational Amplifier
1C32	uA749	Dual Operational Amplifier
1C33	uA749	Dual Operational Amplifier
1C34	7812	Regulator (12v)
1C35	7812	Regulator (12v)
1C36	7806	Regulator (6v)
1C37	NE566	Oscillator
1C38	uA777HC	Operational Amplifier

DECK UNIT DEMODULATORResistors $\frac{1}{4}$  watt carbon 5% (unless noted)

R1	1	kilohm
R2	33	kilohm
R3	2.2	kilohm
R4	220	kilohm
R5	68	ohm
R6	4.7	ohm
R7	4.7	ohm
R8	10	kilohm
R9	10	kilohm
R10	10	kilohm
R11	33	ohm
R12	10	kilohm
R13	10	kilohm
R14	10	kilohm
R15	33	ohm
R16	10	kilohm
R17	47	kilohm
R18	3.3	megohm
R19	470	ohm
R21	22	kilohm
R22	3.9	kilohm
R23	470	ohm
R24	1.8	kilohm
R25	1.8	kilohm
R26	10	kilohm
R27	10	kilohm
R28	10	kilohm
R29	33	ohm
R30	1.8	kilohm
R31	1.8	kilohm
R32	10	kilohm
R33	10	kilohm
R34	10	kilohm
R35	10	kilohm
R36	33	ohm
R37	10	kilohm
R38	1.8	kilohm
R39	1.8	kilohm
R40	6.81	kilohm
R41	10	kilohm
R42	47	kilohm
R43	5.6	kilohm
R44	2.7	kilohm
R45	2.2	kilohm

RN60C Metal Film 1%

Resistors (con't)

R46	2.2	kilohm
R47	150	ohm
R48	100	kilohm
R49	3.3	kilohm
R50	15	kilohm
R51	1.8	kilohm
R52	3.9	kilohm
R53	100	kilohm
R54	33	ohm
R55	100	ohm
R56	10	kilohm
R57	100	ohm
R58	1	kilohm
R59	10	kilohm
R60	100	kilohm
R61	10	kilohm
R62	1.8	kilohm

Sockets

12	Augat #514-AG-10D
18	Augat #516-AG-10D
1	Augat #508-AG-1-D

Terminal Post

12	Cambion #160-1043-03-01
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Transistors

Q1	2N 2222
Q2	2N 4122
Q3	2N 5640
Q4	2N 5640
Q5	2N 5089
Q6	2N 5089
Q7	2N 2222
Q8	2N 3638a
Q9	2N 4122
Q10	2N 3566
Q11	2N 5640
Q12	2N 5640
Q13	2N 4122
Q14	2N 4122



DECK UNIT DEMODULATORHARDWARE

3 2/56 x 1/4 Panhead Screws, SS  
3 #2 Nuts, SS  
3 #2 Flatwashers, SS  
3 #2 Internal Tooth Lockwashers, SS  
2 Ejectors w/pins

## DECK UNIT

## POWER SUPPLY

Circuit Board P/N 30028

Capacitors

C1 10 ufd Sprague 100v  
 C2 10 ufd Sprague 100v

Chokes

L1 .5H Triad #C-26-X

Diodes

CR1 1N752A

Hardware

2 #6 Hex Nuts  
 2 6/32 x 1/2 Pan Head Screws  
 2 #2153 Fiber Washers  
 2 #6 Internal Tooth Washers  
 4 #8 Star Lock Washers  
 2 #8 Flat Washers  
 4 8/32 x 1/4 Hex Standoffs, Threaded  
 2 #6 Flat Washers  
 4 8/32 x 3/8 Pan Head Screws

Resistors

R1 22 ohm 2 watt carbon 5%  
 R2 8.2 Kilohm 2 watt carbon 5%

Terminal Post

18 Cambion 140-1785-02-01-00

Thermistor

TH1 Fenwall #MB 13-L1

Transformers

T1 Triad #SP67  
 T2 Triad #SP29  
 T3 Triad #SP29

Transistors

Q1 2N5239 RCA

Potentiometer

P1 20 ohm #3339-P-1-200  
 Bourns

Switches

S1 #MSS-204NG-1 Alco

Heat Sink Hardware

1 43-03-2, Thermalloy  
 Insulator  
 1 6016-B, Thermalloy

DECK UNIT CHASSIS PARTS LISTMAIN CHASSIS

Front Panel #010-AL-02-0 1 each  
 Back Panel #011-AL-02-0 1 each  
 Chassis Rails #012-AL-02-0 4 each  
 Main Chassis #013-AL-02-0 1 each  
 Top Cover #015-AL-02-0 1 each  
 Bottom Cover #015-AL-02-0 1 each  
 Side Covers #014-AL-02-0 2 each  
 Output Connector Bracketts #016-AL-02-0 26 each  
 Screws #4/40 x 3/8, panhead 26 each  
 Nuts #4 38 each  
 Internal Lock Washers #4 38 each  
 Screws #4/40 x  $\frac{1}{2}$ , panhead 16 each  
 Filister head #4/40 x  $\frac{1}{2}$  1 each  
 Screws #6/32 x 3/8, panhead 12 each  
 Nuts #6 12 each  
 Internal Lockwashers #6 12 each  
 Screws #8/32 x 3/8, panhead 8 each  
 Nuts #8 4 each  
 Internal Lockwashers #8 8 each  
 Screws #10/32 x 3/8, panhead 36 each  
 Internal Lockwashers #10 36 each  
 Screws #10/32 x  $\frac{1}{2}$ , panhead 2 each  
 Screws # $\frac{3}{4}$  x 28, flathead 4 each  
 Bezel #018-AL-02-0 1 each  
 Binding Post #111-0103-001 6 each  
 Capacitors, Mini, .33ufd 9 each  
 Handle Set #H- $\Phi$ 13B 1 each  
 LED's #H-5082-4403 3 each  
 Plexi-Clips #017-AL-02-0 4 each  
 Plexi-Lens #010-PG-02-0 1 each  
 Potentiometers #RV4-NAYSD102A, 1k 1 each  
 " #3862C-282-102A, 1k 1 each  
 " #3862C-282-103C, 10k 1 each  
 Knob #RB67-1SB-DCM,  $\frac{1}{4}$ " 1 each  
 " #RB67-1SB-DCM, 1/8" 7 each  
 Resistors 1/8 watt carbon, 3.3k 9 each  
 Mini Lamp #377 1 each  
 Mini Speaker #011-EL-02-0 1 each  
 Speaker Brackett #019-AL-02-0 1 each  
 Switch #JBT 1-2-3 3 each  
 " #JBT 2-2-3 2 each  
 Switch #PS-105 1 each  
 " #PS-107 1 each  
 " #9A45218N 3 each  
 " #PL106705 1 each  
 Mini Transformer #012-EL-02-0 1 each

DECK UNIT CHASSIS PARTS LISTCHASSIS AND BACK PANEL

Guidespacers #T101 .200	4 each
" #T101 .250	20 each
" #T101 .500	12 each
" #T101 1.000	12 each
Guides #T101 301.60	8 each
Rails #T902 800	2 each
Connectors #8016-090-217-804	2 each
" #PT02a-12-8-s	2 each
" #PT02a-8-3-p	1 each
" #PT02a-8-4-s	1 each
Power Buss #	1 each
Power Supply #018-PC-02-0	1 each
" #B50FT20	1 each
" #213	1 each
Fuse Holder #HKP	1 each
Fuse #2A	1 each
Connectors #706-7015-01	8 each
	1 each
Connectors #8016-090-206-707	1 each

ACCESSORIES

Connector #PT06a-8-3s (sr)	1 each
" #PT06a-8-4p (sr)	1 each
" #PT06a-12-8p (sr)	2 each
" 8016-090-296-707	1 each
Line Cord #17462s	1 each
Packing Crate	1 each
Packing	1 each
Operations Manual	1 each

## APPENDICES

10 KH tuned feedback amplifier	7.1
Servo balanced thermistor bridge	7.2
A successive approximation method	7.3
Salinity Computation	7.4
Phase locked loop & synchronous detector	7.5



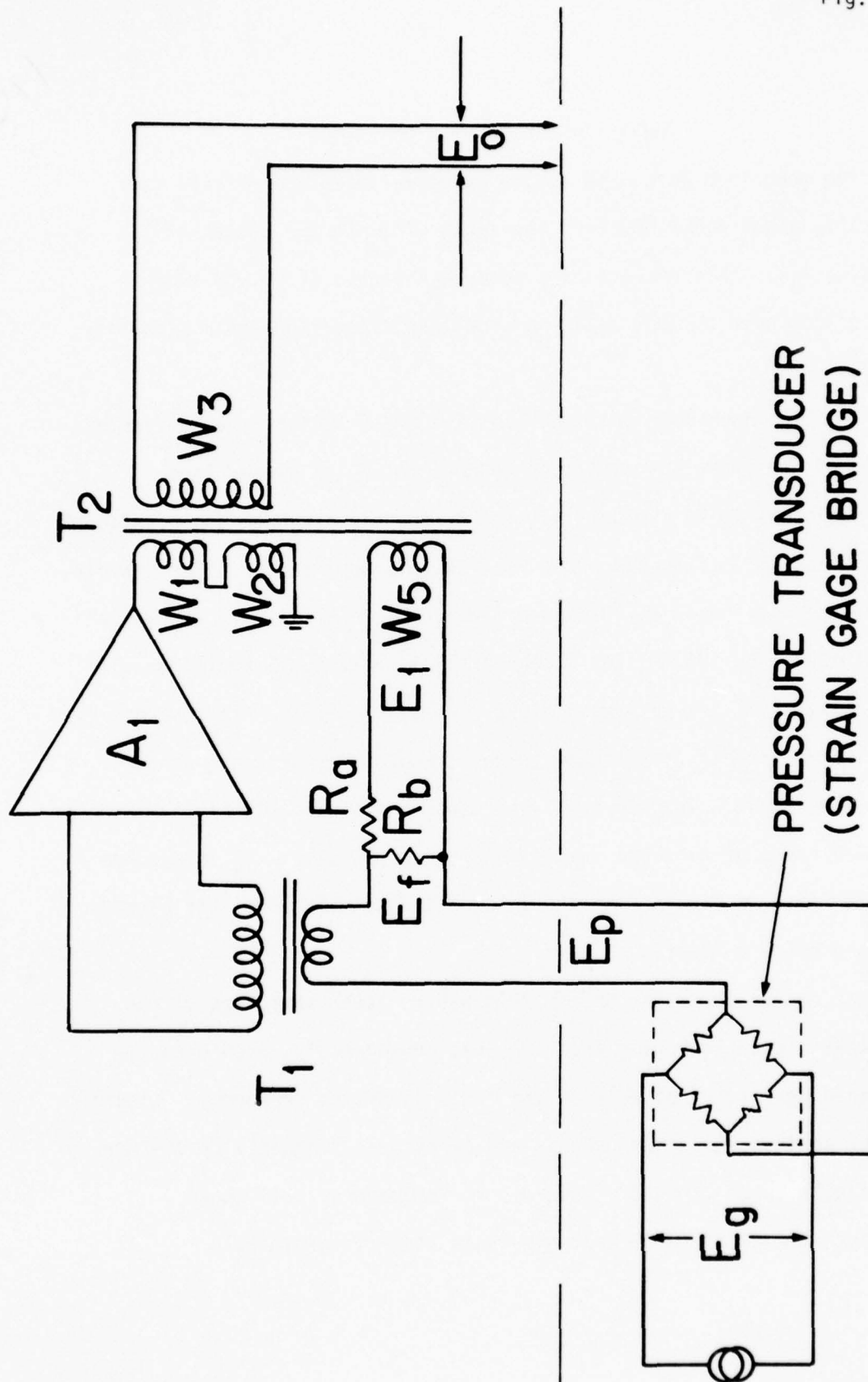
## 10kHz TUNED FEED-BACK AMPLIFIER

The open loop gain used in the pressure interface circuit is typically about 3,000,000 from the input of  $T_1$  to the output of  $T_2$  (winding  $W_3$ ). This results in a feed-back factor of 30,000 (for closed loop gain of 100) ensuring excellent closed loop gain stability at 10kHz.

The high open-loop gain and high feed-back factor require careful design of the phase and amplitude response of  $A_1$  if closed loop oscillation is to be avoided. It can be readily shown that conventional operational amplifiers cannot be used in this application. For example, if the open-loop gain at 10kHz was 3,000,000 the unity gain frequency would have to be 300 MHz for a conventional operational amplifier with 6 db/octave roll off (assuming close loop gain - 100). Clearly this is totally impractical, particularly when transformers are used at the input and output. Transformer  $T_1$  is used to optimize signal to noise and as a means of avoiding common mode noise problems.  $T_2$  is a tuned transformer (see Figure 7.1) and is used to optimize power efficiency and to provide a floating output.

The design approach used in this system takes advantage of the fact that closed loop gain accuracy and, consequently, high open-loop gain were required only at the fixed operating frequency. Clearly one can achieve very high gain at any particular frequency by the use of a single tuned circuit. However, at frequencies well above resonance the gain ( $A$ ) of a single tuned stage is given by

Fig. 7.1



$$A = \frac{F_r A_r}{QF}$$

where  $A_r$  = gain at resonance

$F_r$  = resonant frequency

$Q$  = quality factor of tuned circuit

$F$  = frequency

For a feed back factor of 30,000 at resonance, the frequency ( $F_1$ ) at which the feed-back factor reduces to unity, is calculated as follows:

$$\frac{A_r}{A} = 30,000$$

$$= \frac{QF_1}{F_r}$$

$$\text{therefore } F_1 = \frac{30,000 F_r}{Q}$$

A typical value for  $Q$  is 50 therefore,  $F_1 = 6 \text{ MHz}$

Since the tuned circuit has a phase shift approaching  $90^\circ$  at frequencies well above or below resonance (see Figure 7.1(2), the untuned stages, including input and output transformers, must have a total phase shift less than  $90^\circ$  for frequencies up to  $6 \text{ MHz}$  if the amplifier is to be unconditionally stable under closed loop conditions; a difficult situation. If one were to cascade two tuned stages of the type shown in Figure 7.1(2), the phase shift would

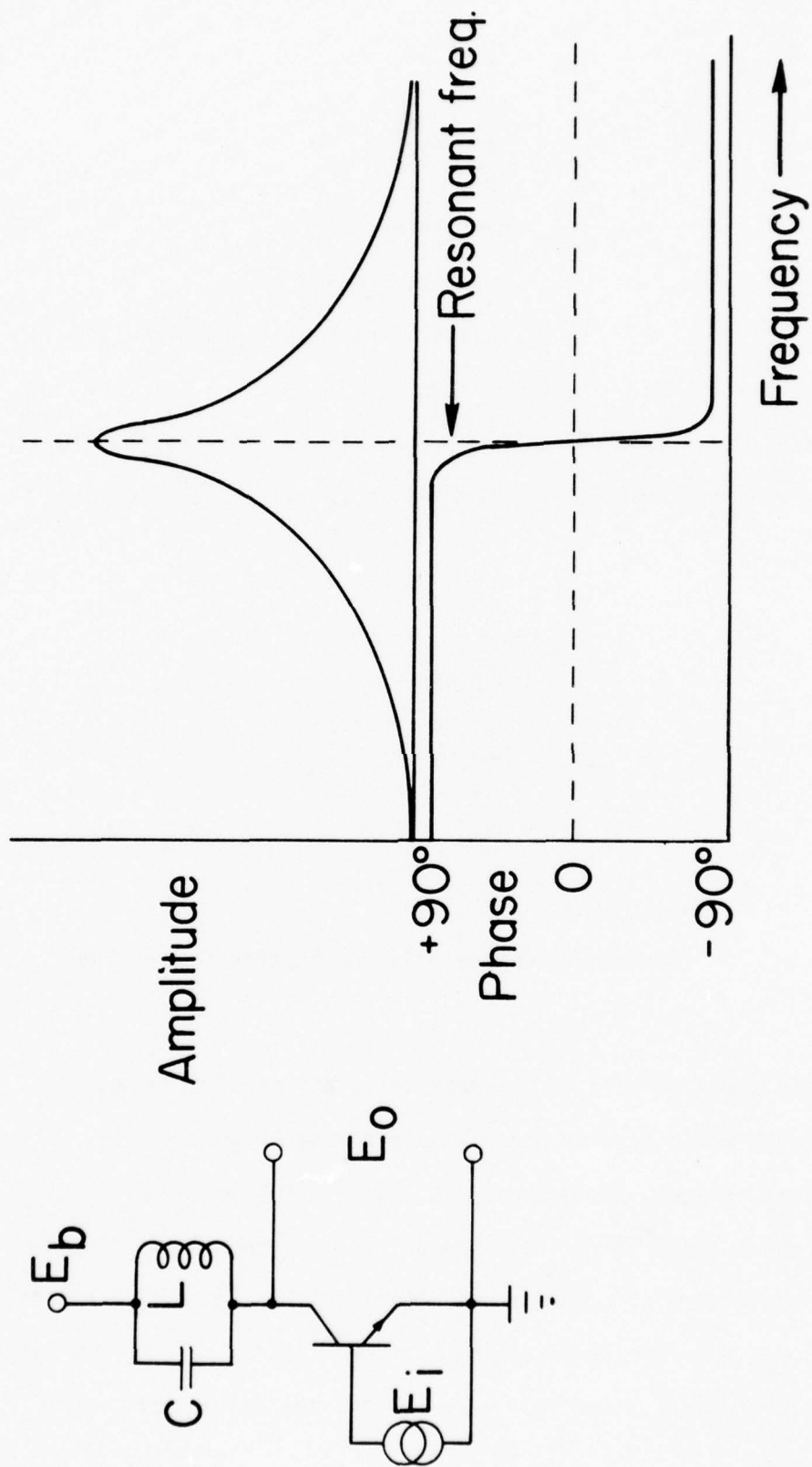


Fig. 7.1(2)

rapidly approach  $180^\circ$  above and below resonance and would almost certainly be more difficult to stabilize under closed loop conditions than the single tuned stage circuit discussed above. However, a very simple modification to the circuit of Figure 7.1(2) readily permits the use of two tuned stages and is shown in figure 7.1(3) along with the amplitude and phase response. At resonance the impedance of the tuned circuit (L, C) is very high compared with R, consequently, R has negligible effects. However, at frequencies remote from resonance, L or C tends to be a short circuit leaving R as the dominant element. This has the advantage of very high gain at resonance and zero phase shift at very high or very low frequencies, thus permitting the use of an amplifier with two tuned stages.

Figure 7.1(4) shows a conceptual schematic of the feed-back amplifier without an input transformer. Fig. 7.1(5) lists the computed amplitude and phase response of this amplifier for both open-loop and closed-loop conditions with the following circuit values:

$$g_{m1} = g_{m2} = 25\text{mA/Volt}$$

$$R_1 = 1,000 \text{ ohms}$$

$$C_1 = C_2 = .01 \text{ microfarads}$$

$$L_1 = L_2 = .0253303 \text{ henries}$$

$$R_2 = R_3 = 80,000 \text{ ohms}$$

$$N_1 = N_2 = 100 \ N_3$$

$$\text{i.e. } N_3 = \frac{N_1}{100}$$

$$\text{therefore, feed-back voltage } (E_f) = \frac{E_o}{100}$$



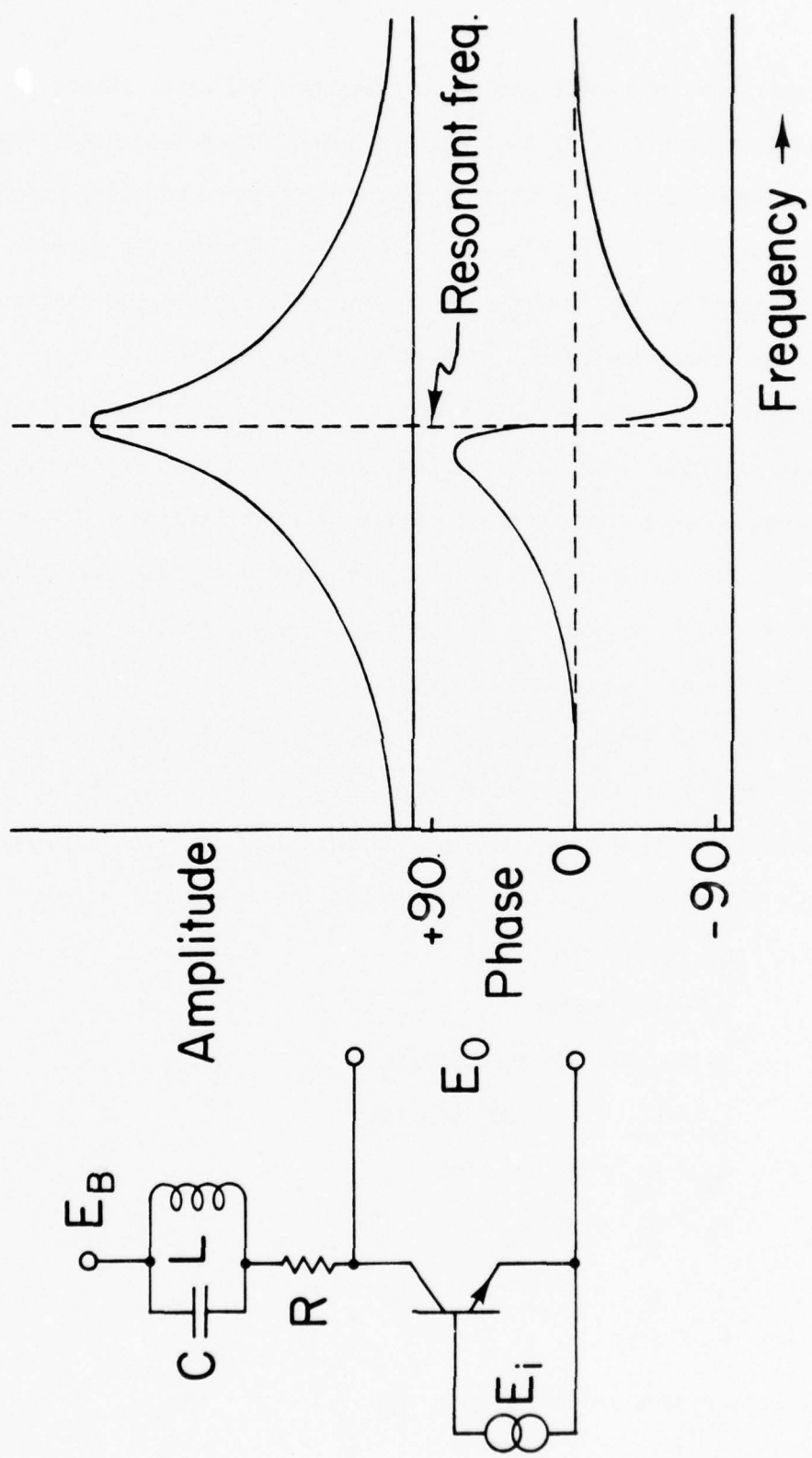


Fig. 7.1(3)

An examination of Fig. 7.1(5) shows that for a closed loop gain of 100 at 10 kHz operation is quite stable with a 1 db peak at 3,500 and 28,000 Hz. Also, at extreme frequencies, i.e., 100 Hz and 1 MHz, the phase shift is almost down to  $90^\circ$  from a maximum of about  $162^\circ$ . The frequencies at which the open-loop gain is 100 are about 1,000 and 100,000 Hz, and the phase shifts are about  $+99^\circ$  and  $-99^\circ$  respectively. This means that if a transformer is placed at the input and is inside the loop, its phase shift must be small at 10 kHz and less than  $\pm 81^\circ$  at 1,000 and 100,000 Hz. These are readily met permitting the use of transformers within the loop for the purpose of providing optimum signal to noise ratios and floating inputs.

The basic design shown in Figure 7.1(4) was used in the interface circuits for temperature, conductivity, and pressure.

Fig. 7.1(4)

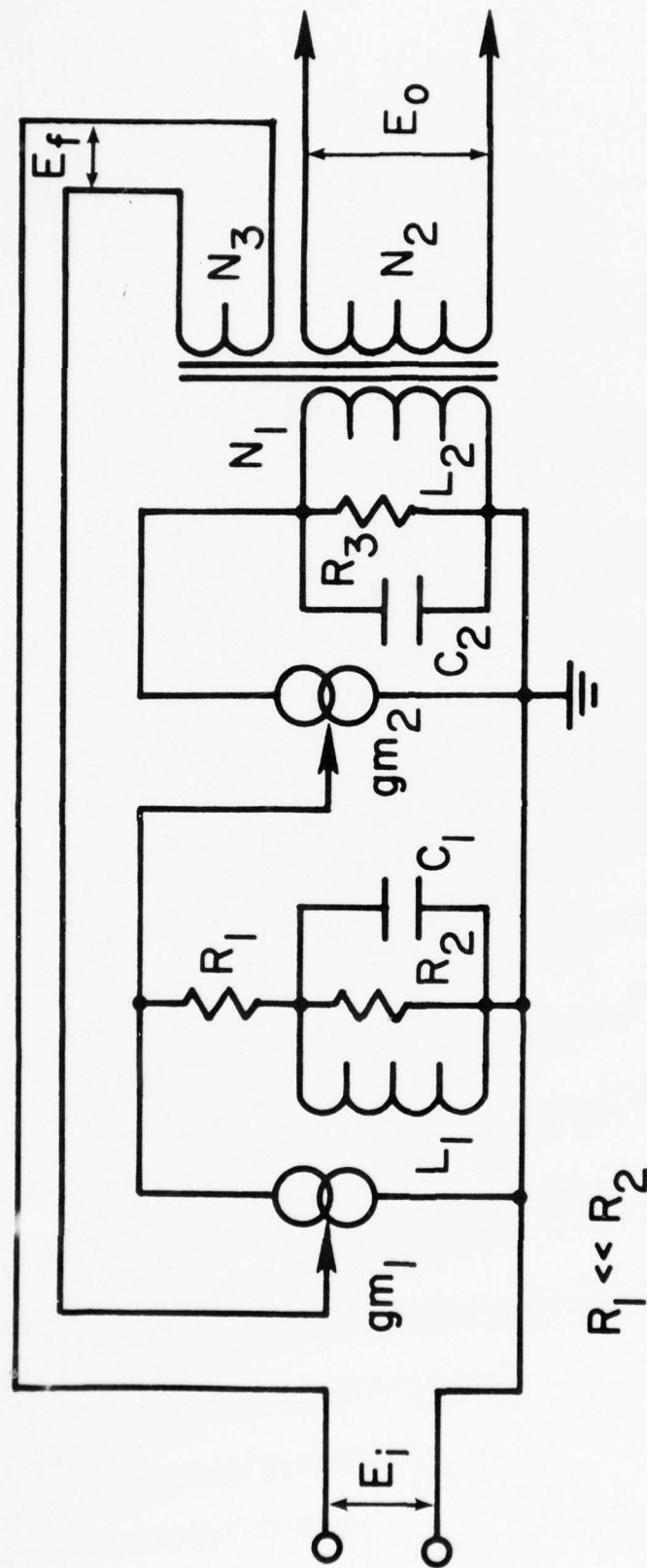


Fig. 7.1(5)

OPEN LOOP PARAMETERS			CLOSED LOOP PARAMETERS	
Frequency (Hz)	Gain (db)	Phase (Deg)	Gain	Phase (Deg)
100	20.0	90.9	9.91595	85.21
200	26.0	91.8	19.6479	80.476
500	34.0	94.5	46.2133	67.071
1000	40.2	99.0	77.6821	48.909
2000	46.8	108.1	103.959	26.878
3000	51.4	117.2	110.024	15.276
3500	53.5	121.8	110.34	11.467
4000	55.5	126.4	109.818	8.513
5000	59.8	135.5	107.59	4.442
6000	64.6	144.4	104.986	2.076
8000	78.3	159.3	101.153	0.249
9000	91.1	161.8	100.265	.050
9500	103.3	154.4	100.061	.017
9800	118.0	126.1	100.007	.006
9840	121.0	115.5	100.004	.005
9880	124.3	100.2	100.001	.003
9920	127.8	77.3	99.9991	.002
9960	130.8	43.6	99.9979	.001
10000	132.1	0.0	99.9975	.000
10040	130.9	-43.5	99.9979	-.001
10080	127.8	-76.8	99.9991	-.002
10120	124.4	-99.5	100.001	-.003
10160	121.2	-114.7	100.004	-.005
10200	118.2	-125.3	100.007	-.006
10500	104.2	-153.5	100.055	-.016
11000	92.8	-161.3	100.217	-.042
12000	81.7	-161.0	100.781	-0.154
16000	65.9	-146.5	104.375	-1.676
20000	59.8	-135.5	107.59	-4.442
30000	52.8	-120.3	110.351	-12.629
60000	45.0	-105.1	98.728	-32.611
100000	40.2	-99.0	77.6821	-48.909
300000	30.4	-93.0	32.0513	-74.335
1000000	20.0	-90.9	9.91595	-85.21

## SERVO BALANCED THERMISTOR BRIDGE

A simplified schematic of the servo balanced thermistor bridge is shown in figure 7.2. The bridge consists of the miniature high speed thermistor  $R_T$  (Fenwal Electronics - GC32SM2), a fixed resistor  $R_F$  and two windings ( $W_2$  and  $W_3$ ) on transformer  $T_1$ . The value of  $R_F$  is chosen so that the bridge output voltage ( $E_t$ ) has minimum non-linearity over the range of 0 to 30°C. The input to the first amplifier  $A_1$  is equal to the difference between  $E_t$  and the output ( $E_m$ ) from the multiplier  $M_1$ .

The two inputs to  $M_1$  are -

- i) a 10 KHz sine wave signal from  $W_4$  on  $T_1$
- ii) a DC signal ( $E_c$ ) from the output of the integrator ( $A_2$ , R and C).

The input to the integrator is the output of a second multiplier  $M_2$  (a phase sensitive detector). The reference signal to the multiplier is a 10 KHz square wave in phase with the oscillator signal  $E_g$  driving the thermistor bridge and multiplier  $M_1$ . The relationships are as follows:

$$\begin{aligned} \text{Output voltage } E_o &= e_o \sin \omega t \\ &= E_1 A_1 = e_1 A_1 \sin \omega t \dots \dots \dots (1) \end{aligned}$$

$$\begin{aligned} \text{where } E_1 &= E_t - E_m \\ &= (e_t - e_m) \sin \omega t \end{aligned}$$

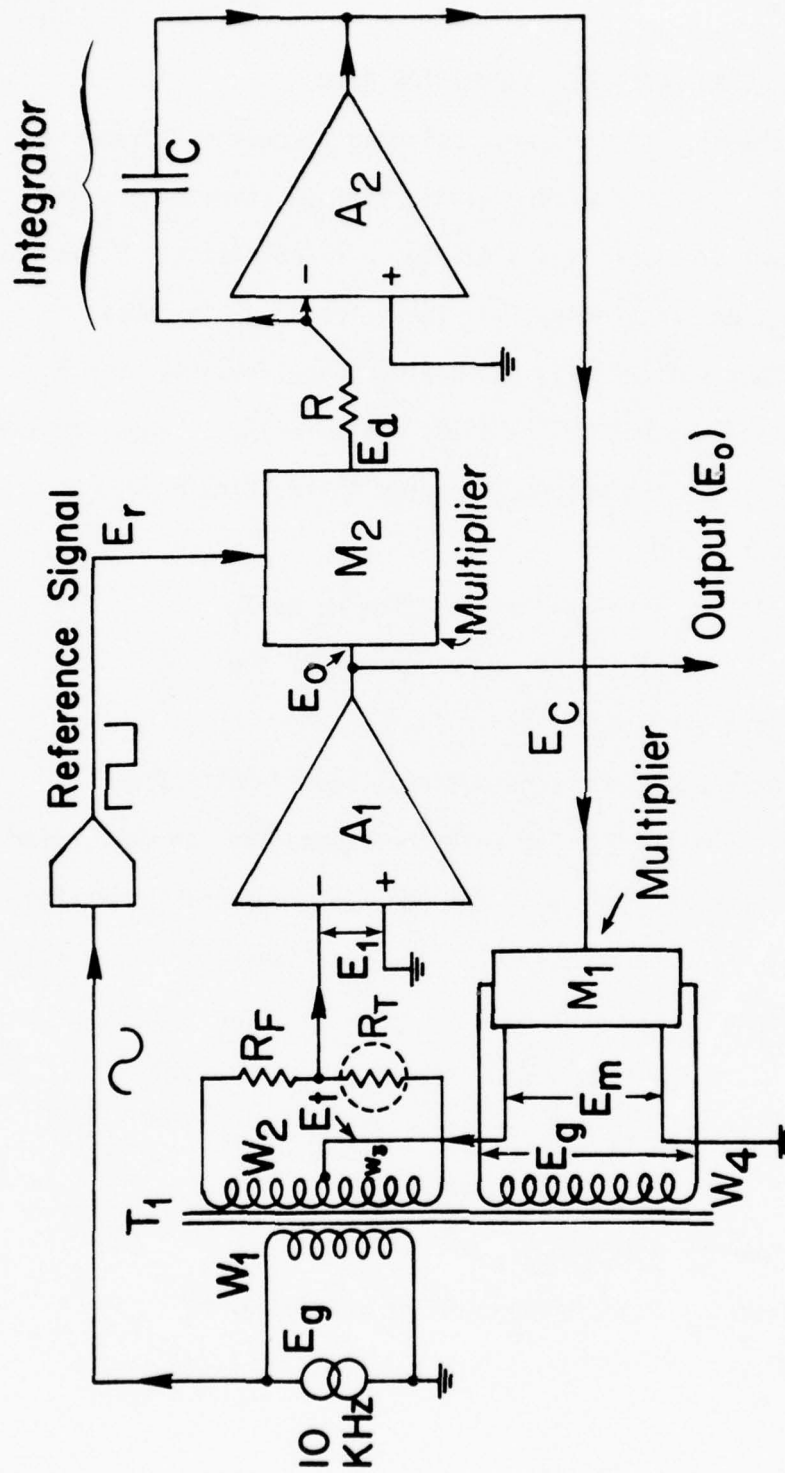
$$\text{now } E_m = K_1 E_c E_g$$

$$\text{where } K_1 = \text{scale constant of multiplier } M_1$$

$$\text{therefore } E_o = A_1 (E_t - K_1 E_c E_g) \dots \dots \dots (2)$$



Fig. 7.2



$R_T$  = Fast Response Thermistor

The output of the integrator  $E_c$  is given by

$$E_c = \frac{1}{RC} \int E_d dt$$

now  $E_d = K_2 E_0 E_r$

where  $K_2$  = scale constant of multiplier  $M_2$

Since  $E_r$  is a constant amplitude square wave in phase with  $E_i$

we can express  $E_r$  as a Fourier series as follows:

$$E_r = \frac{4}{\pi} e_r (\sin \omega t + \frac{1}{3} \sin 3\omega t + \dots + \frac{1}{n} \sin n\omega t + \dots)$$

.. (n = odd integer)

and  $e_r$  = peak amplitude of square wave

$$\begin{aligned} \text{therefore } E_d &= \frac{4}{\pi} e_r K_2 e_0 (\sin \omega t + \frac{1}{3} \sin 3\omega t + \dots \text{ etc.}) \\ &= K_3 e_0 (\sin^2 \omega t + \frac{1}{3} \sin \omega t \sin 3\omega t + \dots \text{ etc.}) \end{aligned}$$

$$\text{where } K_3 = \frac{4}{\pi} K_2 E_r = \text{constant}$$

Since  $\omega \gg \frac{1}{RC}$  only zero frequency components of  $E_d$  will cause a significant output ( $E_c$ ) from the integrator

since  $\sin^2 \omega t = \frac{1}{2} (1 - \cos 2\omega t)$  the only zero frequency component of  $E_d$  is given by

$$E_d = \frac{1}{2} K_3 E_0$$

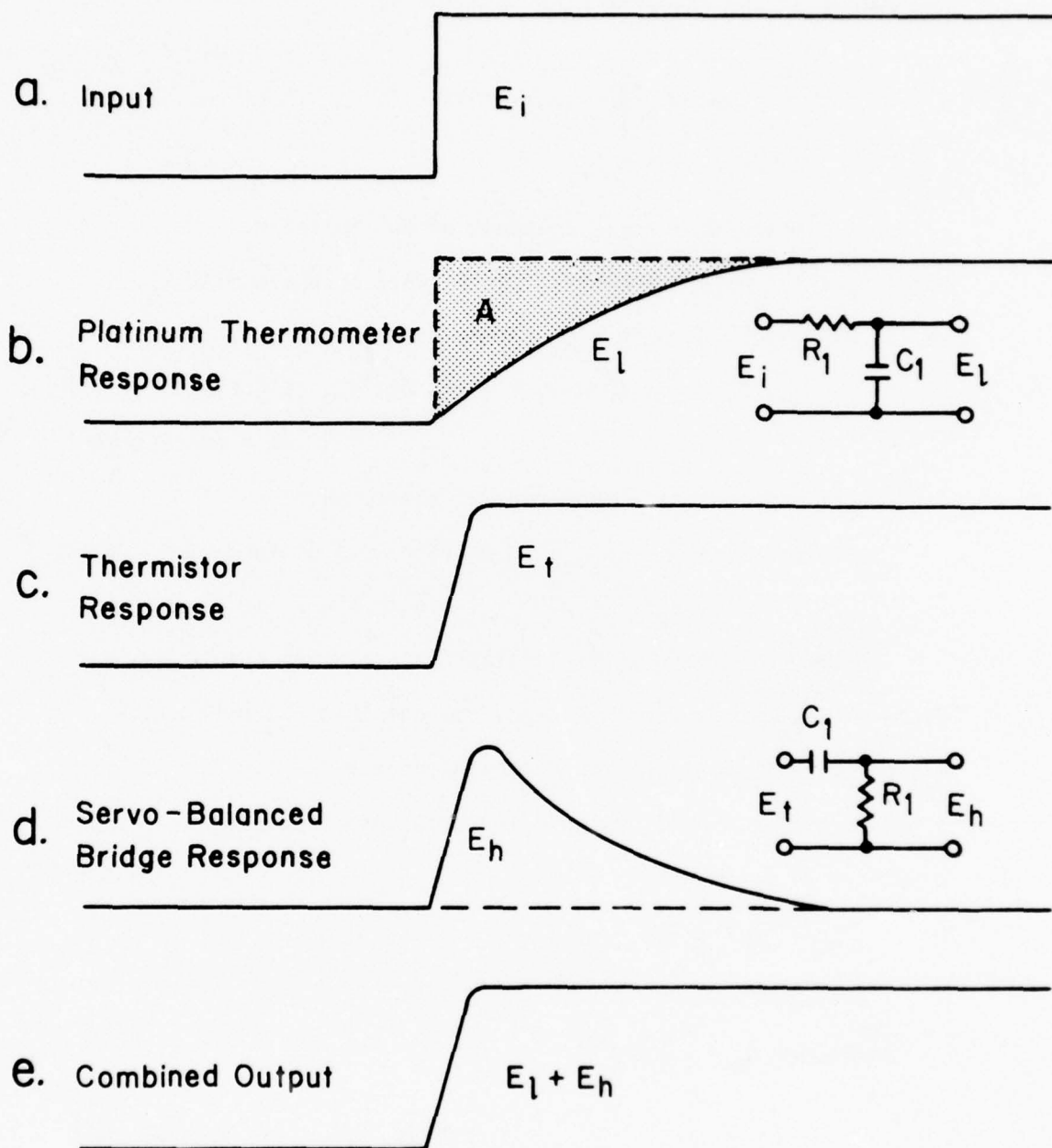
$$\text{therefore } E_c = \frac{K_3}{2RC} \int E_0 dt$$

$$\text{substituting in (2) } E_0 = A_1 (E_t - \frac{K_1 E_g K_3}{2RC} \int E_0 dt)$$

$$= A_1 E_t - \frac{K}{RC} \int E_0 dt \dots \dots \quad (3)$$

$$\text{where } K = A_1 K_1 K_3 E_g = \text{constant.}$$

Fig. 7.2(2)



The simple high pass filter in Fig 7.2(2) has the following response

$$E_h = E_i - \frac{1}{R_1 C_1} \int E_h dt$$

if we make  $E_i = A_1 E_t$

and  $R_1 C_1 = \frac{RC}{K}$

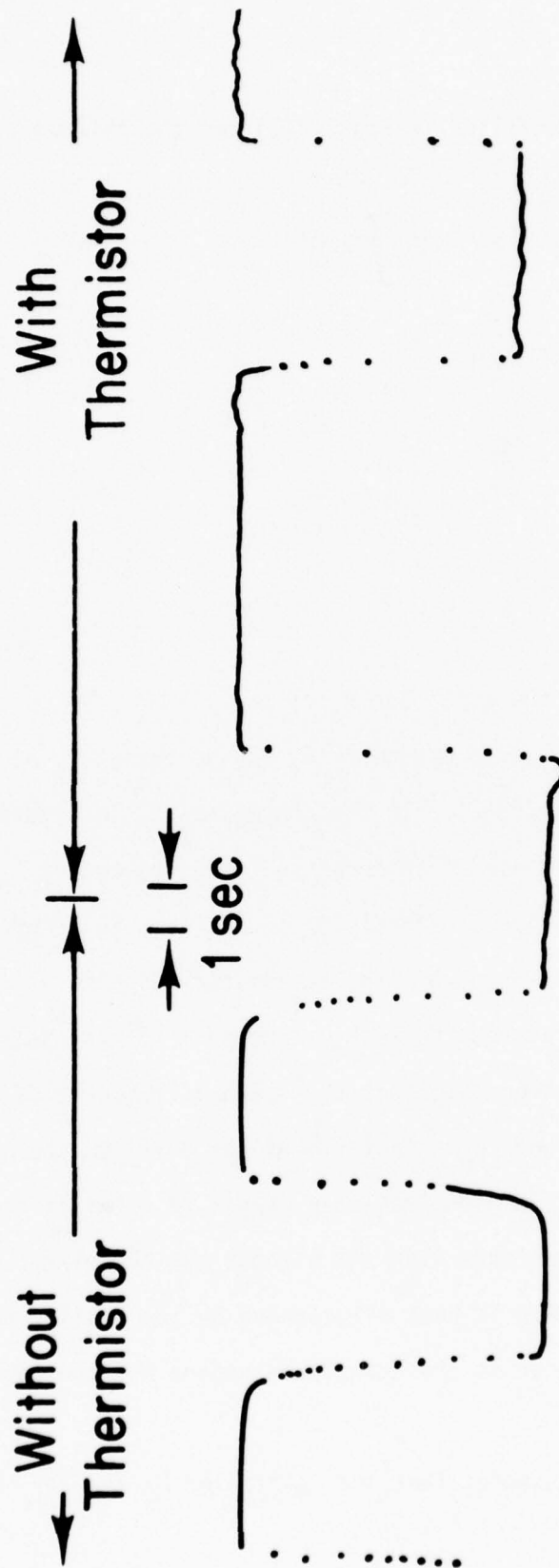
then  $E_h = E_o$

This means that the amplitude  $e_o$  of the 10 KHz sine wave output  $E_o$  has the same response to a change in  $E_t$  as the output  $E_h$  of the high pass filter shown in 7.2(2). If the thermistor  $R_T$  in Figure 7.2 had an instantaneous response to temperature, then the output  $E_o$  would provide exactly the correct signal to correct the lag error in the platinum thermometer. However, the thermistor response is not instantaneous. Therefore, the combined response of the platinum thermometer and the thermistor has the speed of response of the thermistor and the long term stability of the platinum thermometer.

The response to a temperature step change is shown in Figure 7.2(3); the figure shows data taken with and without the thermistor. The improvement in response is best illustrated by the smaller number of data points which occur in the transition region for the combined measurement.

This discussion assumes that the multiplier  $M_2$  and the integrator

Fig. 7.2(3)





are ideal devices, and that  $E_d$  is zero when  $E_o$  is zero and the integrator offset voltage is zero. Adequate performance in the integrator is achieved using a state of the art integrated circuit operational amplifier, such as a National Semiconductor LM208A. The multiplier  $M_2$  is implemented using a switching type synchronous detector. The output ( $E_o$ ) of  $A_1$  is applied to the primary of a transformer with a center-tapped secondary, the center tap being grounded. FET's connected to each side of the secondary are synchronously turn "on" and "off" by  $E_r$  and its complement, resulting in full wave synchronous detection with excellent quadrature rejection and essentially zero dc output when  $E_o$  is zero.

The time constant of the loop is given by

$$t = \frac{T}{A_o}$$

where  $T = RC$  (Ref. Figure 7.2(2))

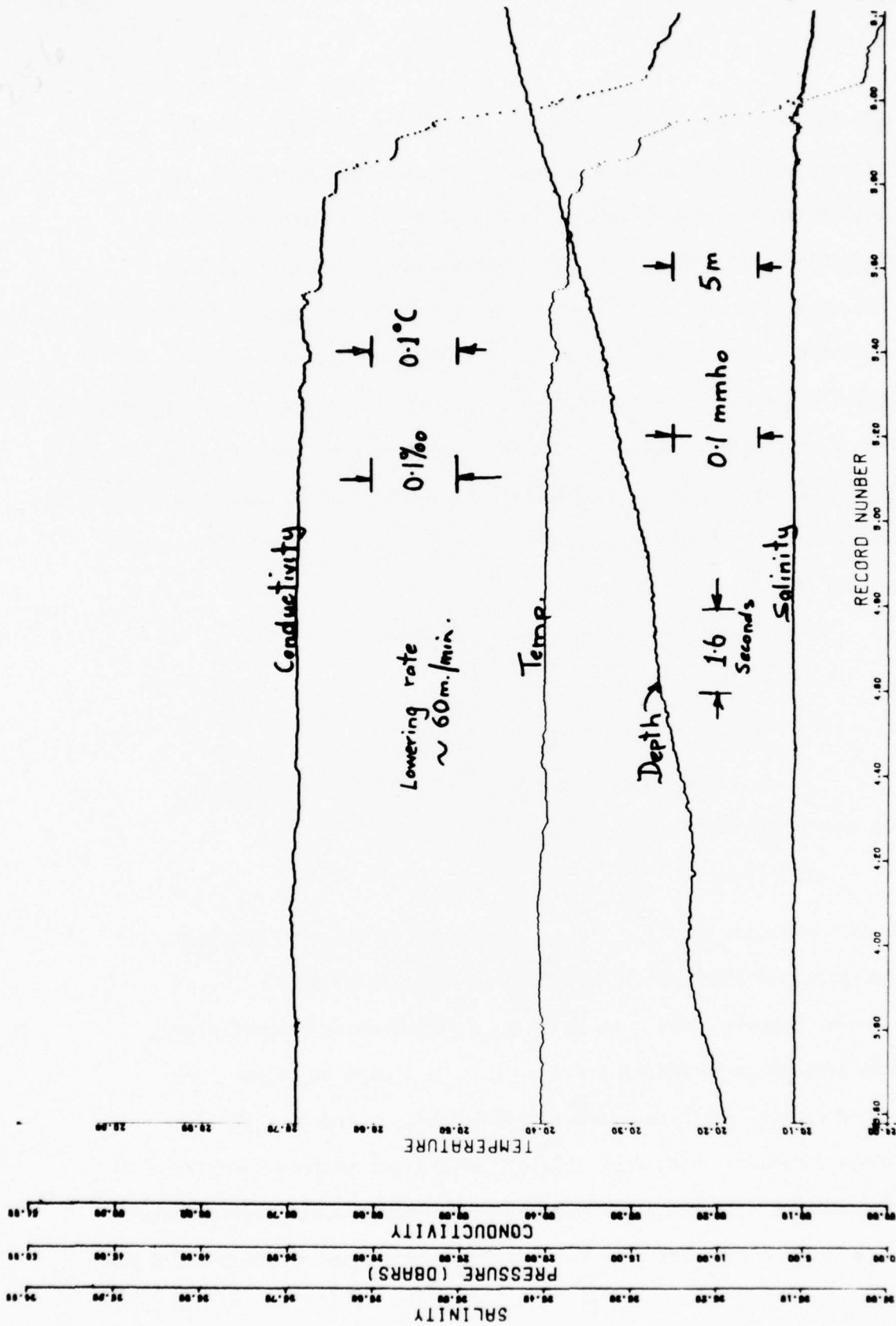
and  $A_o$  = open-loop gain measured from the output of the integrator to the output of  $M_2$

$$\text{therefore } t = \frac{RC}{A_o}$$

Then servo time constant ( $t$ ) is made equal to the time constant of the platinum thermometer by adjusting the gain of  $A_1$ .

The overall effectiveness of this technique is demonstrated by the data shown in Figure 7.2(4). This is a plot of temperature, conductivity, depth and computed salinity as a function of time (record number) going from a fairly well mixed surface layer into the thermocline. In the high gradient region individual readings taken 30 milliseconds apart show maximum rates of change of about  $0.6^\circ\text{C}$  per

Fig. 7.2(4)



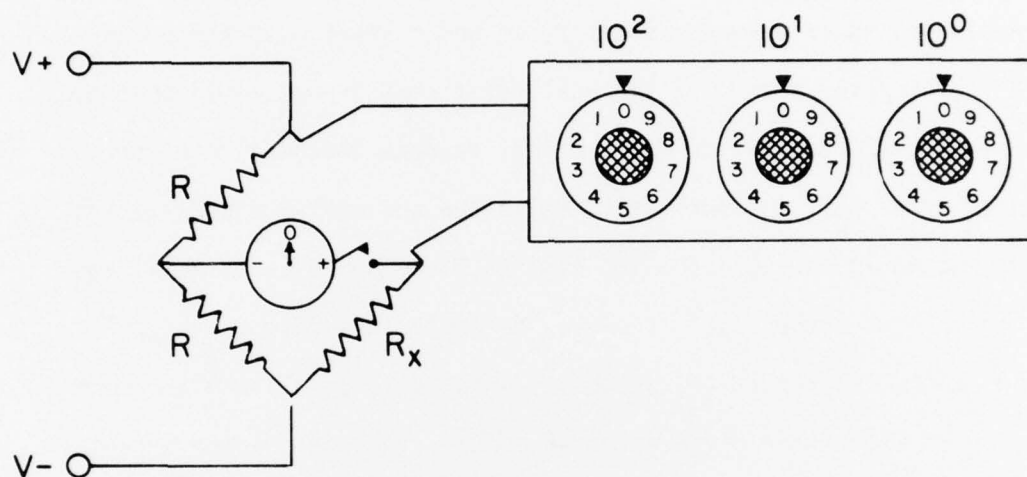
second with corresponding salinity "spikes" less than 0.01 ppt. This clearly shows the match between the response time of the conductivity sensor and the combined response of the thermistor and platinum thermometer.

## A SUCCESSIVE APPROXIMATION METHOD

This is a very common method for comparing a switch selectable value with an unknown value. If we had a wheatstone bridge with a decade resistor and an unknown resistor, we would start with the decade box at zero, zero, zero. If the null meter read "+" we would continue, if, however, it read "-" we would either reverse the null meter or the drive (to make the sign correct). Using the successive approximation method, we would now turn the  $10^2$  dial to 9 and decrease it until the null meter read either null or plus. We could then move to the  $10^1$  and  $10^0$  knobs and repeat the process. This would permit a 0.1% determination of Rx. If the differences were small, we would spend a longer time arriving at a decision than if they were large, similarly after a very large error signal we would allow the null meter time to settle before pressing the sample switch again (in the CTD the adaptive sampling board determines the sample time and recovery time necessary for proper operation, and the comparator replaces the null meter.)

The digitizer logic board may be considered as seventeen D type flip-flops. All of their D inputs are connected in common (to the comparator output). The stages are sequentially clocked and the 'clock' of each stage is connected to the 'set' of the next stage.  $Q_0$  is connected to a switch capable of reversing the polarity of the sensor output whilst each of the other 16 Q outputs is connected to single pole change-over switch on the digital to analog converter board. Each of these switches controls a voltage equivalent to its weight in the binary

Fig. 7.3





code, i.e. Switch 1 only turned on causes the D/A output to be equal to half full scale  $(\frac{2^{15}}{2^{16} - 1}) \times FS = \frac{1}{2}FS$

Switch 16 only turned on causes the D/A output to be equal to one least significant bit  $(\frac{2^0}{2^{16} - 1}) \times FS = \frac{1}{65,535} FS$

while switch 1 and switch 16 both turned on causes a D/A output equal to the algebraic sum of the above

$$= \frac{FS}{2} + \frac{FS}{65,535}$$

## SALINITY COMPUTATION

Because absolute conductivity is difficult to measure most investigators have worked with conductivity ratio using standard sea water as a reference. Consequently, the salinity computation goes as follows:

$$G = G_1 \left( 1 - \alpha(T-15) + \frac{1}{3} KP \right)$$

where  $G$  = conductivity corrected for the effect of temperature and pressure on the conductivity cell.

$G_1$  = indicated conductivity

The CTD is calibrated against the 1968 I.P.T.S. and the following equations require that temperature according to the 1948 I.P.T.S. be used. The following equation will implement this conversion.

$$T_{48} = T_{68} + 4.4 \times 10^{-6} T_{68} (100 - T_{68})$$

$\alpha$  = coefficient of linear expansion (of alumina)

$$\alpha = 6.5 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$$

$T$  = temperature (1948 I.P.T.S.)

$K$  = bulk modulus of compressibility (of alumina)

$$K = 1.5 \times 10^{-8} \text{ cm/cm/decibar}$$

$$P = \text{pressure (decibars)}$$

$$R_T = \frac{G}{G_0 p(T) R_p(T, P, S)}$$

where  $R_T$  = ratio of conductivity of sample to conductivity of 35 ppt when both are at temperature  $T$  and pressure  $P$

$$G_0 = \text{conductivity of 35 ppt sea water at } 15^\circ\text{C } (P=0)$$

$p(T)$  = ratio of conductivity of 35 ppt sea water at temperature  $T$  to its conductivity at  $15^\circ\text{C } (P=0)$

Brown in 1966 determined the ratio as follows:

$$p(T) = .676524 + .201317 \times 10^{-1} T + .998866 \times 10^{-4} T^2 \\ - .194260 \times 10^{-6} T^3 - .672491 \times 10^{-8} T^4$$

Bradshaw and Schleicher in 1965 determined the effect of pressure on conductivity as follows:

$$R_p(T, P, S) = 1 + .01(g(T)f(P) + h(P)j(T)) (1 + \ell(T)m(S))$$

$$\text{where } g(T) = 1.5192 - 4.5302 \times 10^{-2} T + 8.3089 \times 10^{-4} T^2 \\ - 7.900 \times 10^{-6} T^3$$

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$$f(P) = 1.04200 \times 10^{-3} P - 3.3913 \times 10^{-8} P^2 + 3.300 \times 10^{-13} P^3$$

$$h(P) = 4 \times 10^{-4} + 2.577 \times 10^{-5} P - 2.492 \times 10^{-9} P^2$$

$$J(T) = 1.00 - 1.535 \times 10^{-1} T + 8.276 \times 10^{-3} T^2 - 1.657 \times 10^{-4} T^3$$

$$k(T) = 6.95 \times 10^{-3} - 7.6 \times 10^{-5} T$$

$$m(S) = 35.000 - S$$

where  $S$  = salinity (ppt)

The salinity dependence of  $R_p$  is quite small so that for continuous profiling the value of  $S$  computed for the previous scan is quite adequate.

$$R = R_T + (1 - R_T) (.0175 R_T - .0045 R_T^2) (1 - .08 T + .00089 T^2)$$

where  $R$  = ratio of conductivity of sample to conductivity of 35 ppt sea water when both are 15°C and atmospheric pressure.

$$\text{lastly } S = .7347 + 32.2807 R + 3.4775 R^2 - .02395 R^3$$

The last two relationships were derived from data published by Brown in 1966.

## PHASE LOCKED LOOP

The principal element of the CTD demodulator is a phase-locked loop which is illustrated in a generalized form in Fig. 7.5. The phase of the frequency,  $f$  of an input signal is compared with the divided output frequency  $f'$  of a Voltage Controlled Oscillator (V.C.O.), producing the dc signal which is the V.C.O. input. The loop "locks" when  $f'$  is  $90^\circ$  phase-shifted with respect to  $f$ . The data transmission clock is generated in the underwater unit and regenerated from the telemetred data by means of a phase lock loop circuit in the deck unit.

## SYNCHRONOUS DETECTOR

The deck unit phase comparator and filter comprise a phase-sensitive detector and an integrator. The phase-sensitive detector is illustrated in Fig. 7.5(2) below. When  $Z$  is high, the detector is a unity gain inverting amplifier; when  $Z$  is low, the detector is a unity gain non-inverting amplifier. The truth table for this device will be:

The wave forms in Figure 7.5(3) illustrate the performance of the detector with three differently phased input signals,  $W_1$  thru  $W_3$ .

If the chopper and unknown signal are in phase, a negative output is produced; if they are in anti-phase, a positive output is produced. Finally if the signals are in quadrature ( $90^\circ$  phase shifted,) then the output will average zero volts d.c.



Fig. 7.5

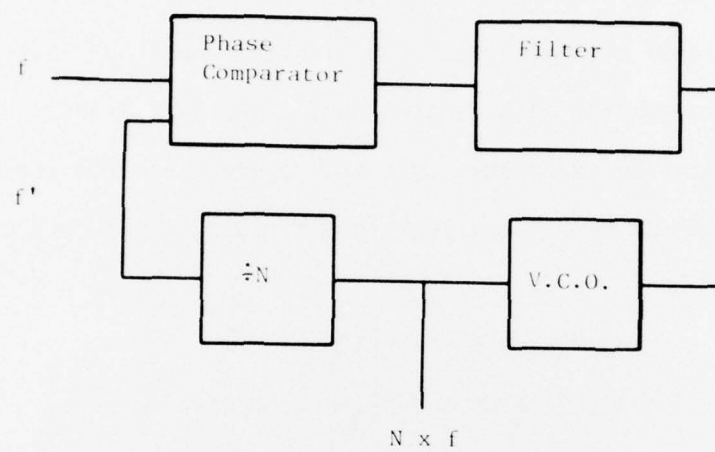


Fig. 7.5(2)

Z	W	X
1	W	$\bar{W}$
0	W	W

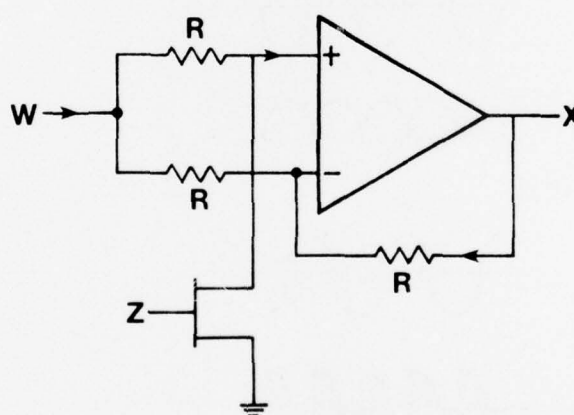
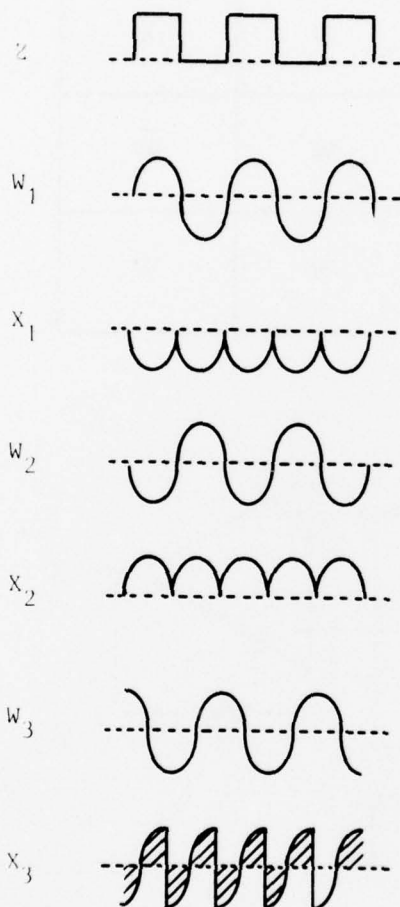


Fig. 7.5(3)



## ACKNOWLEDGEMENTS

The instrument described in this report was developed by Neil Brown, with the invaluable assistance of William McLeod, at the Woods Hole Oceanographic Institution supported by ONR Contract N00014-66-C-0241

The authors wish to thank Jerry Dean for his careful editing of the text and Janice Goodell, Alice Bland, Judy Lumpkin and Janet Moller for preparing the text and figures.

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4. TITLE (and Subtitle) W.H.O.I./BROWN CONDUCTIVITY, TEMPERATURE, AND DEPTH MICROPROFILER.	5. TYPE OF REPORT & PERIOD COVERED Technical Report	
6. AUTHOR N. L. Brown and G. K. Morrison	7. CONTRACT OR GRANT NUMBER(s) N00014-66-C-0241	
9. PERFORMING ORGANIZATION NAME AND ADDRESS Woods Hole Oceanographic Institution Woods Hole, MA 02543	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS NR 083-004	
11. CONTROLLING OFFICE NAME AND ADDRESS NORDA National Space Technology Laboratory Bay St. Louis, MS 39529	12. REPORT DATE Feb 1978	
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)	13. NUMBER OF PAGES 1271 P.	
	15. SECURITY CLASS (of this report) Unclassified	
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) 1. Oceanographic Microprofiler 2. Conductivity, Temperature and Depth Measuring System 3. Microstructure Profiler		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A Conductivity, Temperature and Depth (CTD) profiler has been designed to make precise fine scale measurements of these physical parameters in the ocean. This CTD system consists of a shipboard Data Terminal deck unit and an under-water unit which provides continuous sampling of the three variables as it is lowered into the water. Additional sensors can be added to measure other variables; the most common is dissolved oxygen. (Cont. on back) 387 000		

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→ This report is a detailed description of the CTD System and includes the necessary documentation to operate and maintain the equipment. ↑

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